# TRIBAL INITIAL STUDY / MITIGATED NEGATIVE DECLARATION 

## IONE BAND OF MIWOK INDIANS <br> IONE PLYMOUTH CASINO PROJECT



JANUARY 2024

PREPARED FOR:
Ione Band of Miwok Indians
9252 Bush Street
Plymouth, CA 95669

PREPARED BY:
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(916) 447-3479


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### 1.0 INTRODUCTION

The lone Band of Miwok Indians (Tribe) proposes to develop a casino on trust land (Reduced Project). The Project Site consists of federal trust land within unincorporated Amador County (Figures $\mathbf{1}$ and 2). An Environmental Impact Statement (EIS) was prepared pursuant to the National Environmental Policy Act (NEPA). The Final EIS was published in 2009 and a Record of Decision (ROD) was issued by the Bureau of Indian Affairs (BIA) in May of 2012 that led to the U.S. Department of the Interior acquiring the Project Site into federal trust status. The parcels that comprise the Project Site were placed into Federal Trust in March of 2020 (Amador County, 2020).

The Reduced Project is substantially smaller than Alternative A in the EIS, and includes less than 350 Class III gaming devices. This document assesses potential off-reservation environmental impacts of the Reduced Project.

### 1.1 Regulatory Considerations

The following regulatory resources were considered in the environmental analysis:

- Tribal-State Compact Between the State of California and the Ione Band of Miwok Indians (Compact, 2020).
- Ione Band Environmental Protection Statute, Tribal Council Resolution No. 2023-06 (IBMI, 2023).
- Amador County General Plan (Amador County, 2016).
- Amador County Zoning Code (Amador County, 2023a).

The Tribe entered into a Tribal-State Compact with the State of California (Compact) on August 3, 2020. The Compact became effective upon the publication of notice in the Federal Register on December 11, 2020. Section 11.1 of the Compact states that the Tribe shall not commence construction on a Project (defined as a Gaming Facility) until certain requirements are met, including the evaluation of offreservation environmental impacts. Pursuant to Section 11.2 of the Compact, in April of 2023 the Tribe adopted a Tribal Environmental Protection Ordinance. Compact Sections 11.3 through 11.14 describe the types of studies the Tribe may prepare to document its evaluation of off-reservation environmental impacts. Section 11.5 of the Compact states:
"If the Tribe determines that the Project is not subject to a Categorical Exemption and that the Project may cause a Significant Effect on the Off-Reservation Environment, the Tribe shall prepare an Initial Study. The Tribe shall use the checklist at Appendix B for the Initial Study, and its findings shall be supported by substantial evidence. If, based upon the Initial Study, the Tribe determines that it is appropriate to do so, it may prepare a Negative Declaration or a Mitigated Negative Declaration for the Project."

In accordance with the Compact, the Tribe has made the determination that an Initial Study and a Mitigated Negative Declaration are the appropriate documents in connection with the evaluation of offreservation environmental impacts. The Checklist included in Appendix B of the Compact (Checklist) is presented in Section 3.0 herein.

### 1.2 AgREEMENTS

Mitigation measures to reduce off-reservation impacts to less-than-significant levels are listed in Section
3.0. The Tribe may enter into an intergovernmental agreement (IGA) with the County and/or the City of Plymouth to address significant off-reservation impacts to public services, including law enforcement, fire protection and emergency medical services, or if an IGA is not entered into, the Tribe will enter into an enforceable binding letter agreement with the State of California under which the Tribe shall agree to perform the required mitigation pursuant to section 11.5(c) of the Compact.

### 2.0 PROJECT DESCRIPTION

### 2.1 PROJECT COMPONENTS

The Reduced Project would be constructed within the Tribe's reservation, which is located in Amador County, on the southern border of the City of Plymouth (Figures 1 and 2). The Reduced Project is within the scope of the Gaming Facility identified as the preferred action alternative in the Final EIS ( 75 Fed. Reg 49513, Aug 13, 2010) and approved in the associated Record of Decision (77 Fed. Reg. 31871-31873, May 30, 2012).

The Project Site is located on the east side of State Highway 49/Golden Chain Highway (SR 49), approximately one mile south of the City of Plymouth downtown area. Most of the Project Site is located in unincorporated Amador County. A number of smaller parcels that are located on the western portion of the Project Site are located within the City of Plymouth (Figure 3).

The Reduced Project and associated facilities would be constructed primarily on an approximately 20 -acre undeveloped portion of the Tribe's federal trust land. A Site Plan of the Reduced Project is shown in Figures 3 and 4, and project components are summarized in Table 1. A driveway to the casino would utilize the entrance to the Shenandoah Inn after it is demolished.

The Reduced Project includes the construction of a single-story casino with less than 350 Class III gaming devices. It would also include, a bar, a café, administrative offices, a breakroom, loading dock, warehouse and an outdoor entertainment area. An outdoor entertainment area would be constructed to the north of the main building structure. A wastewater treatment plant (WWTP) would be constructed to process wastewater generated by the casino, restaurants, administrative offices and other facilities. Three irrigation fields totaling approximately 7 acres would dispose of treated effluent. During the first full year of operations, the Reduced Project would employ approximately 240 persons on a full and part-time basis.

Parking lots would consist of approximately 672 parking spaces for the use of casino patrons and employees. The west lot would have 220 spaces, the north lot would have 249 spaces, and the south lot would have 203. Parking lots would include ADA compliant spaces and 48 spaces for valet parking.

## Site Preparation and Construction

The Project Site currently consists mostly of undeveloped open space. Excavation and grading would occur during construction to accommodate the Reduced Project depicted in Figure 4 and as further described in the Preliminary Drainage Analysis attached as Appendix C. The topography of the Project Site ranges from approximately 900 feet to 1,150 feet above mean sea level (amsl). Approximately 9 acres of impervious surfaces would be created on-site (Montrose, 2023).


Figure 1



Stormwater from newly created impervious surfaces would flow into two stormwater facilities. Under Option A, these stormwater improvements would consist of two stormwater ponds, one to the north of the casino structure, and one to the south (see Figure 4). Stormwater conveyance would occur via pipes and culverts. Under Option B, the stormwater pond to the south would be replaced by an underground storage system. Stormwater ponds would be excavated, and earthen berms would not be a significant feature. A more detailed description of the proposed drainage improvements is presented in Appendix C.

During grading, cut and fill would be balanced, with no significant import or export of material. Construction would require heavy equipment such as dozers, graders, tractors, loaders, backhoes, mixers, cranes, forklifts, pavers, and rollers. Construction would adhere to Section 6.4.2 of the Compact, which requires the project to meet or exceed the requirements of the California Building Standards Code, the California Public Safety Code and Title III of the Americans with Disabilities Act of 1990 (Compact, 2020). Project construction is estimated to temporarily employ approximately 300 workers.

TABLE 1: PROJECT COMPONENTS

| Component | Number | Approximate Square <br> Footage |  |
| :--- | :---: | :---: | :---: |
| Casino |  | - |  |
| Gaming Floor |  | 25,205 |  |
| Class III Slot Machines | 10 tables |  |  |
| Table Games |  | 17,617 |  |
| Back of House Service and <br> Support Areas |  | 42,822 |  |
| Subtotal |  | 3,652 |  |
| Food and Beverage |  | 3,259 |  |
| Café |  | 1,611 |  |
| Bar |  | 162 |  |
| Kitchen |  | 8,684 |  |
| Grab and Go |  | 5,568 |  |
| Subtotal |  | 57,074 |  |
| Outdoor Entertainment | Total |  |  |
|  |  |  |  |
| Casino Surface Parking |  | - |  |
| Wastewater Treatment Plant |  |  |  |



## Architecture, Signage, Lighting and Landscaping

The architecture and exterior signage of the building would be compatible with the natural and rural characteristics of the site and vicinity by incorporating native materials and neutral colors. Construction of the Reduced Project would primarily occur during daytime hours. Minor construction lighting could be visible from off-reservation residences during dusk and nighttime hours. Illuminated signs would be designed to blend with the light levels of the building and landscape lighting in both illumination levels and color characteristics. The exterior lighting of the Reduced Project would be integrated into components of the architecture and would be strategically positioned to minimize off-site lighting. The architectural design of the project would be enhanced by landscaping using drought tolerant plants native to the region.

## Access

As described in Appendix E and as illustrated in Figure 4, access to the Project Site would be via Village Drive, which connects to SR 49.

## Water Supply

As described in more detail in the FEIS, the Reduced Project would source water from existing wells. Water quality would be achieved by a multi-staged filtration and treatment process. Total potable water demand for the Reduced Project is estimated at 37,438 (Appendix D), to achieve the estimated 22,463 GPD net water usage by the casino facility. A 90,000-gallon storage tank will be constructed to meet water demands. The storage tank would provide 4 days of water storage to support fire flow demands, if wells or treatment systems were off-line for any reason.

## Wastewater

Wastewater would be treated at an on-site WWTP, located to the east of the casino (Figure 4). The WWTP would be sized to treat the peak flows resulting from the Reduced Project. The anticipated average flow rate is 36,315 GPD, or 13.3 million gallons per year. Treated effluent would be used to irrigate 3 separate fields, with a combined area of approximately 7 acres. The combination of irrigation and evaporation would consume the effluent during most months. Irrigation disposal would be reduced during the rainy season (November to March). During periods of rain, effluent would be temporarily stored in either a 4 million-gallon tank (Option A), or a similar sized storage pond (Option B). Under Option B, the pond would be approximately 5.3 feet deep and the berms surrounding the pond would be up to 7.5 feet tall. A more detailed description of the proposed on-site WWTP and ponds is presented in Appendix D.

## Gas and Electric

Pacific Gas \& Electric (PG\&E) provides electrical power to the majority of Amador County, including the City. PG\&E currently maintains the Oleta substation, a 33-kilovolt facility on the corner of Main Street and Shenandoah Road that serves an area from Plymouth to Sutter Creek. Overhead PG\&E utility lines are located adjacent to the Project Site and on the Project Site to serve the Shenandoah Inn. PG\&E does not provide natural gas in the area. A propane tank will be brought to the site to provide gas.

### 2.2 Changes in the Project

Components of the current project as compared to the EIS alternatives, including Alternative A that was approved in the ROD, are summarized in Table 2. As shown in the table, the Reduced Project is most similar to EIS Alternative C, but is still smaller in scope. EIS Alternative D is not listed in the table, as it is a retail development and thus not comparable to the other casino alternatives.

TABLE 2: REDUCED PROJECT COMPARED TO EIS ALTERNATIVES ${ }^{1}$

| Component | EIS Alternative A - Proposed Casino and Hotel ${ }^{1}$ | EIS Alternative B - Reduced Casino with Hotel ${ }^{1}$ | EIS Alternative C - Reduced Casino ${ }^{1}$ | Reduced Project |
| :---: | :---: | :---: | :---: | :---: |
| Casino Games |  |  |  |  |
| Slot Machines | 2,000 | 1,500 | 1,000 | 349 |
| Table Games | 40 | 30 | 20 | 10 |
| Casino Square Footage |  |  |  |  |
| Gaming Floor | 65,000 | 48,750 | 32,500 | 25,205 |
| Back of House Service and Support Areas | 20,000 | 18,000 | 15,250 | 17,617 |
| Food and Beverage | 20,000 | 20,000 | 18,500 | 8,684 |
| Outdoor Entertainment and Other | 15,000 | 14,000 | 13,000 | 5,568 |
| Total | 120,000 | 100,750 | 79,250 | 57,074 |
| Hotel Rooms | 250 | 250 | 0 | 0 |
| Event, Convention Center sf. | 30,000 | 30,000 | 0 | 0 |
| Parking Spaces |  |  |  |  |
| Car Parking | 2,914 | 2,354 | 1,069 | 672 |
| RV and Bus Parking | 51 spaces | 51 spaces | 51 spaces | 0 |
| Total | 2,965 | 2,405 | 1,120 | 672 |
| Water/Wastewater |  |  |  |  |
| Water Demand | 116,700 GPD $^{2}$ | 104,000 GPD ${ }^{2}$ | 64,900 GPD ${ }^{2}$ | 37,438 GPD $^{3}$ |
| Wastewater Generation | 154,600 GPD | 135,200 GPD | 75,400 GPD | 36,315 GPD $^{3}$ |
| 1. Source: Information for EIS alternatives obtained from Final EIS (BIA, 2009). <br> 2. Net of adjusting for recycled water used to meet non-potable water demands. <br> 3. Source: Appendix D. |  |  |  |  |

## 3．0 ENVIRONMENTAL EFFECTS

### 3.1 DeTERMINATION

Environmental impacts assessed on the following pages have been evaluated using the following rating system：potentially significant impact，less than significant impact with mitigation incorporated，less than significant impact，or no impact．If an impact is determined potentially significant，further environmental review is provided below．For impacts determined less than significant with mitigation incorporated， mitigation measures are recommended where necessary and have been designed consistent with applicable federal，State，and local regulatory requirements．

Environmental issue areas checked below have the potential to be affected by the Reduced Project and may constitute an effect necessitating mitigation or further environmental review．The Reduced Project was determined to have no significant impact on unchecked issue areas，and mitigation or additional environmental review are not warranted．

| $\square$ | Aesthetics |
| :--- | :--- |
| $\square$ | Agricultural and Forest Resources |
| $\searrow$ | Air Quality |
| $\searrow$ | Biological Resources |
| $\square$ | Cultural Resources |
| $\square$ | Geology and Soils |
| $\square$ | Greenhouse Gas Emissions |
| $\square$ | Hazards and Hazardous Materials |
| $\square$ | Water Resources |


|  | Land Use |
| :---: | :---: |
|  | Mineral Resources |
| $\triangle$ | Noise |
|  | Population and Housing |
| 区 | Public Services |
|  | Recreation |
| 】 | Transportation／Traffic |
|  | Utilities and Service Systems |
| 区 | Cumulative Effects |


| $3.2 \quad$ AESTHETICS |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Would the project: |

## Question A

The project location and on-reservation topography are such that construction and operation of the Project would alter the views from off-site vantage points. Machinery and construction activities would be visible to passing motorists on SR 49. Visibility of construction activities from off-site locations would be temporary in nature and would not permanently degrade existing visual characteristics.

The proposed casino is a one-story building with a height of approximately thirty (30) feet. The casino structure would be located where grade is approximately 1,150 feet amsl. The WWTP would be located on the south east portion of the Project Site and would either be marginally visible from SR 49 and public road ways, or not visible at all. Existing grade of the location of the WWTP is approximately 1,000 amsl. Off-site views of the Reduced Project would be partly shielded due to landscaping and local topography.

A viewshed of a northbound motorist on SR 49 is presented in Figure 5. Due to topography, existing landscaping, and the posted speed limit of 50 mph , passing motorists would only have brief views of the Reduced Project from SR 49.

As described in Section 2.1, Project landscaping would incorporate native plants, and the design would utilize neutral colored paints and building materials. Consequently, Reduced Project design would be compatible with the surrounding area.

For the reasons described above, the Reduced Project would have a less-than-significant impact on scenic vistas.

## Question B

No off-reservation scenic resources would be affected by construction activities or operations. No offreservation trees, outcroppings, or historic buildings would be physically altered.


While SR 49 to the west of the Reservation is not a designated state scenic highway, it may be eligible to be classified for some segments (Caltrans, 2023). The closest state scenic highway is approximately eighteen miles to the north. The City of Plymouth has a scenic corridor overlay district that applies to all parcels that are adjacent to or front to or front on SR 49 (City of Plymouth, 2023). This district applies to off-reservation parcels in the vicinity of the Reduced Project, but does not apply to the Project Site. However, the project design would be generally consistent with the scenic corridor guidelines.

For the reasons described above, the Reduced Project would have a less than-significant impact on offreservation scenic resources. Mitigation listed below would further reduce potential impacts.

## Question C

Construction of the Reduced Project would primarily occur during daytime hours. Minor construction lighting could be visible from off-reservation residences during dusk and nighttime hours. Operation of Reduced Project would increase the amount of lighting in the vicinity. However, distance from the Project Site to the reservation boundary, the proposed landscaping, in conjunction with existing screening vegetation and topography would reduce the off-site impacts with regards to lighting. The Reduced Project would not use flashing signs or fluorescent lights. Further, lighting fixtures on the site would generally be downcast to direct lighting away from off-reservation areas. There would be a less than significant impact. Impacts would be further reduced through the implementation of mitigation listed in Section 3.13.

## Mitigation Measures

A. The Tribe shall participate in Caltrans' Adopt-A-Highway Program to provide litter removal on one or more highway segments in the vicinity of the Project Site.

| 3.3 Agriculture and Forest Resources Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{array}{\|c\|} \hline \text { NO } \\ \text { IMPACT } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Involve changes in the existing environment, which, due to their location or nature, could result in conversion of off-reservation farmland to nonagricultural use or conversion of off-reservation forest land to non-forest use? | $\square$ | $\square$ | $\square$ | V |

## Question A

The economic development chapter of the Amador County General Plan outlines policies that emphasize the importance of farmlands for agricultural uses and agri-tourism (Amador County, 2016). Policy E-9.5 and E-9.6 mandate the need for a review of development compatibility with existing new land uses and direct future development away from farmlands of local or statewide importance.

The California Department of Conservation designates land within the vicinity of the Project Site within the classifications of grazing land, urban or build-up land, and other land (California Department of Conservation, 2022). Such land is not considered prime farmland. In addition, no off-reservation land within the vicinity of the Project Site is designated as timberland. With the exception of de minimis land disturbance that could occur from the construction of traffic mitigation measures, the Reduced Project would not cause any land use conversion of off-reservation farmland to non-agricultural use or conversion of off-reservation forest land to non-forest use. There would be no impact.

## Mitigation Measures

None.

| 3.4 AIR QUALITY Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Conflict with or obstruct implementation of the applicable air quality plan? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Violate any air quality standard or contribute to an existing or projected air quality violation? | $\square$ | $\nabla$ | $\square$ | $\square$ |
| c) Result in a cumulatively considerable net increase of any criteria pollutant for which the project region is non-attainment under an applicable federal or state ambient air quality standard (including releasing emissions, which exceed quantitative thresholds for ozone precursors)? | $\square$ | $\square$ | $\square$ | $\square$ |
| d) Expose off-reservation sensitive receptors to substantial pollutant concentrations? | $\square$ | $\square$ | $\square$ | $\square$ |
| e) Create objectionable odors affecting a substantial number of people off-reservation? | $\square$ | $\square$ | $\square$ | $\square$ |

## Questions A-C

The Project Site is located within the Mountain Counties Air Basin (MCAB) which is part of the Amador County Air Pollution Control District (ACAPCD). The Clean Air Act is implemented by the U.S. Environmental Protection Agency (USEPA) and sets ambient air emission limits, referred to as the National Ambient Air Quality Standards (NAAQS), for six criteria air pollutants: particulate matter of aerodynamic radius of 10 microns or less ( $\mathrm{PM}_{10}$ ), particulate matter of aerodynamic radius of 2.5 microns or less ( $\mathrm{PM}_{2.5}$ ), carbon monoxide (CO), nitrogen dioxide (NO2), ground-level ozone (O3), and lead (Pb). The California Air Resources Board (CARB) sets standards for criteria pollutants in California that are more stringent than the NAAQS and include the following additional contaminants: visibility-reducing particles, hydrogen sulfide, sulfates, and vinyl chloride. Table 3 lists California and National Ambient Air Quality Standards (CAAQS/NAAQS) for ozone and particulate matter ( $\mathrm{PM}_{2.5}$ and $\mathrm{PM}_{10}$ ). The MCAB is designated under the NAAQS as marginal nonattainment for 8 -hour ozone (USEPA, 2023). The MCAB is designated under the CAAQS as nonattainment for 1 -hour and 8 -hour ozone (CARB, 2023). The MCAB is in attainment or is unclassified for all other criteria pollutants under the NAAQS and the CAAQS.

TABLE 3: CALIFORNIA AND NATIONAL AMBIENT AIR QUALITY STANDARDS

| Pollutant | Averaging Time | CAAQS | NAAQS |
| :---: | :---: | :---: | :---: |
| Ozone | 8-hour | 0.07 ppm | 0.07 ppm |
|  | 1 hour | 0.09 ppm | - |
| PM 2.5 | 24-hour | - | $35 \mu \mathrm{~g} / \mathrm{m}^{3}$ |
|  | Annual | $12 \mu \mathrm{~g} / \mathrm{m}^{3}$ | $12 \mu \mathrm{~g} / \mathrm{m}^{3}$ |
| PM ${ }_{10}$ | 24-hour | $50 \mu \mathrm{~g} / \mathrm{m}^{3}$ | $150 \mu \mathrm{~g} / \mathrm{m}$ |
|  | Annual | $20 \mu \mathrm{~g} / \mathrm{m}^{3}$ | - |
| Carbon Monoxide (CO) | 1-hour | 20 ppm | 35 ppm |
|  | 8-hour | 9 ppm | 9 ppm |
| Nitrogen Dioxide $\left(\mathrm{NO}_{2}\right)$ | 1-hour | 0.18 ppm | 0.100 ppm |
|  | Annual | 0.030 ppm | 0.053 ppm |
| Sulfur Dioxide ( $\mathrm{SO}_{2}$ ) | 1-hour | 0.25 ppm | 0.075 ppm |
|  | 24-hour | 0.04 ppm | 0.14 ppm |
|  | Annual | NA | 0.03 ppm |
| Sulfates | 24-hour | $25 \mu \mathrm{~g} / \mathrm{m}^{3}$ | NA |
| Lead | 30-day | $1.5 \mu \mathrm{~g} / \mathrm{m}^{3}$ | NA |
|  | Cal. Quarter | NA | $1.5 \mu \mathrm{~g} / \mathrm{m}^{3}$ |
|  | Rolling 3-month average | NA | 0.15 |
| Hydrogen Sulfide | 1-hour | 0.03 ppm | NA |
| Vinyl Chloride ${ }^{\mathrm{K}}$ (chloroethene) | 24-hour | 0.010 ppm | NA |
| Visibility-Reducing Particles | 8-hour | See Note | NA |
| SOURCE: CARB, 2016. <br> Note: Particles in sufficient amount to produce an extinction coefficient of 0.23 per kilometer when the relative humidity is less than 70 percent. This standard is intended to limit the frequency and severity of visibility impairment due to regional haze and is equivalent to a 10 - mile nominal visual range. <br> ppm = parts per million by volume. <br> $\mu \mathrm{g} / \mathrm{m}^{3}=$ micrograms per cubic meter of air. |  |  |  |

Air quality impacts potentially associated with the Reduced Project include those resulting from shortterm construction activities and operation. A significant impact would occur if the Reduced Project would result in emissions of ozone precursors (ROG and NOx) at levels that would conflict with or obstruct an applicable air quality plan, violate an air quality standard, or contribute to an existing or projected air quality violation. To determine the potential for significant off-site air quality impacts, the Reduced Project emissions are compared to the de minimis General Conformity levels set forth in 40 CFR 93.153. ACAPCD does not have any thresholds of significance for air quality. Since ACAPCD does not have specific thresholds of significance, the de minimis General Conformity thresholds will be used to determine if a project would result in emissions that would violate any air quality standard or contribute substantially to an existing or projected air quality violation.

Amador County's General Plan has several policies aimed at maintaining and improving air quality.

Policy C-9.1: Encourage development of commercial or industrial businesses which provide jobs for county residents in order to reduce vehicle miles traveled for residents who must drive elsewhere for employment.
Policy C-9.2: Encourage infill development, and development near existing activity centers in order to encourage walking or bicycle use in running local errands.
Policy C-9.3: Promote the separation of emission sources from sensitive receptors such as schools, day care centers, and health care facilities.
Policy C-9.4: Encourage energy conservation and energy efficient design in new development projects.
Policy C-9.5: Promote recycling of waste materials and the use of recycled materials.
Policy C-9.6: Maintain viable public transportation options in Amador County, and provide transit connections such as park-and-ride services to job centers in nearby counties.
Policy C-9.7: Work with state and federal agencies to seek recognition of air pollutant movement from valley to mountain counties as a contributor to reduced air quality.

The Reduced Project is located near the City of Plymouth and would create new jobs. Thus, the Reduced Project is consistent with the first two policies. The Reduced Project is separated from sensitive receptors and would implement energy conservation and energy efficient design. Therefore, the Reduced Project does not conflict with the Amador County General Plan.

ACAPCD has enacted several rules and regulations to attain and maintain the air quality in its jurisdiction. ACAPCD Rule 218 is regarding fugitive dust emissions. The rule prevents and controls fugitive dust emissions to the atmosphere by using good housekeeping and/or work practices. In order to ensure that fugitive dust emissions from the Reduced Project do not cause substantial pollution off-site consistent with other construction projects in Amador County, Mitigation Measure 3.4-A would be implemented to control fugitive dust emissions.

Construction of the Reduced Project would generate criteria air pollutants from construction equipment (primarily diesel operated), construction worker automobiles (primarily gasoline operated), architectural coatings on buildings and parking lots, and physical land disturbance which generates fugitive dust. Construction emissions are summarized in Table 4, and CalEEMod output files are provided in Appendix A. Default assumptions in CalEEMod were used for construction estimates including construction duration and equipment with construction assumed to start in 2024. As shown in Table 4, project emissions would be far below the thresholds of significance.

TABLE 4: CONSTRUCTION EMISSIONS

| Construction Year |  | Pollutants of Concern |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | NOx | CO | SOx | PM $_{\mathbf{1 0}}$ | PM $_{\mathbf{2 . 5}}$ |  |  |
|  | Tons per Year |  |  |  |  |  |  |  |
| 2024 | 0.25 | 2.98 | 2.44 | 0.01 | 0.46 | 0.23 |  |  |
| 2025 | 0.77 | 0.65 | 0.88 | $<0.005$ | 0.04 | 0.03 |  |  |
| Total Construction Emissions | $\mathbf{1 . 0 2}$ | $\mathbf{3 . 6 3}$ | $\mathbf{3 . 3 2}$ | $\mathbf{0 . 0 1}$ | $\mathbf{0 . 5 0}$ | $\mathbf{0 . 2 6}$ |  |  |
| Maximum Year Construction Emissions | $\mathbf{0 . 7 7}$ | $\mathbf{2 . 9 8}$ | $\mathbf{2 . 4 4}$ | $\mathbf{0 . 0 1}$ | $\mathbf{0 . 4 6}$ | $\mathbf{0 . 2 3}$ |  |  |
|  | de minimis levels | 100 | 100 | $n / a$ | $n / a$ | $n / a$ | $n / a$ |  |
|  | Exceeds Thresholds | No | No | No | No | No | No |  |

## Source: Appendix A.

Operational emissions are summarized in Table 5 and output files are provided in Appendix A. Information on building energy use was estimated for the casino and back offices using data from US Energy Information Administration 2018 Commercial buildings Energy Consumption Survey for Other Public Assembly Buildings which includes casinos (EIA, 2023). Trip information was obtained from the traffic impact study for the Reduced Project. Operation of the Reduced Project would result in direct area and energy emissions as well as indirect mobile emissions. Indirect mobile emissions are associated with vehicle trips to and from the Reduced Project. Direct area and energy emissions would result from such sources as heating, air conditioning, landscape maintenance, kitchen equipment use, and other combustion sources. Table 5 shows that project emissions would be below thresholds of significance. Other fossil fuel sources such as boilers, emergency generators can emit criteria pollutants, including include ROG, NOx, CO, SOx, and particulate matter, however these emissions would be negligible.

TABLE 5: OPERATIONAL EMISSIONS

| Emission Sources | ROG | NOX | CO | SOx | PM ${ }_{10}$ | PM 2.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tons per Year |  |  |  |  |  |
| Area | 0.31 | <0.005 | 0.20 | <0.005 | <0.005 | <0.005 |
| Energy | 0.01 | 0.11 | 0.10 | <0.005 | 0.01 | 0.01 |
| Mobile | 3.56 | 4.74 | 24 | 0.04 | 3.26 | 0.88 |
| Total Emissions | 3.87 | 4.85 | 24.3 | 0.04 | 3.27 | 0.89 |
| de minimis levels | 100 | 100 | $n / a$ | $n / a$ | $n / a$ | $n / a$ |
| Exceeds Thresholds | No | No | No | No | No | No |

Source: Appendix A.

Construction and Operation of the Reduced Project would not result in significant off-reservation effects associated with the regional air quality environment with implementation of Mitigation Measure 3.4-A for fugitive dust control. Therefore, the Reduced Project would not conflict with or obstruct implementation of applicable air quality plans, contribute to existing or projected air quality violations, result in a cumulatively considerable net increase of any criteria air pollutant for which the project region is nonattainment, or expose off-reservation sensitive receptors to substantial pollutant concentrations.

Past, present, and future development projects contribute to a region's air quality on a cumulative basis; thus, air pollution is predominantly considered a cumulative impact. A single project is not usually sufficient in size to result in nonattainment of the NAAQS or CAAQS. Should a project's individual emissions contribute toward the exceedance of such standards, cumulative impacts on air quality would be considered significant. In developing attainment designations for criteria pollutants, the USEPA considers the region's past, present, and future emission levels. The Reduced Project would not result in indirect or cumulative growth impacts, would not cause an exceedance of the thresholds, and would not result in a cumulatively considerable net increase in NOx, ROG, $\mathrm{PM}_{10}$, or $\mathrm{PM}_{2.5}$ to the extent that MCAB would be in nonattainment. There would be a less-than-significant impact.

## Question D

The term "sensitive individuals" refers to those segments of the population most susceptible to poor air quality: children, the elderly, and individuals with pre-existing, serious health problems affected by air quality. Examples of sensitive receptor locations are residences, schools and school yards, parks and playgrounds, daycare centers, nursing homes, and medical facilities. The Project Site is adjacent to SR 49 and vacant land. The closest school that could be considered a sensitive receptor is Plymouth Elementary School located at 18601 Sherwood Street in Plymouth. Residences are located across SR 49 (to the west) approximately 200 feet from the eastern boundary of the site.

The USEPA and CARB classify air pollutants that can be toxic as Hazardous Air Pollutants (HAPs) and Toxic Air Contaminants (TACs), respectively. Diesel exhaust is a complex mixture that includes hundreds of individual constituents and is identified by the State of California as a known carcinogen. Diesel exhaust would be emitted from construction equipment and trucks during operation. Other HAPs and TACs may be present in gasoline exhaust from vehicles, volatile components of wastewater during treatment, combustion of natural gas, and various other chemicals used in paints and consumer products. Due to the variable nature of construction activity, the generation of TAC emissions would be temporary in most cases, especially considering the short amount of time such equipment is typically within an influential distance to expose sensitive receptors to substantial emission concentrations. The majority of operational emissions from vehicles including cars and trucks would occur along roadways and would not be concentrated in any one specific location. Concentrations of mobile-source (including construction equipment) diesel PM emissions are typically reduced by 70 percent at a distance of approximately 500 feet (CARB, 2005). The WWTP is not located near sensitive receptors and any emissions would disperse rapidly in the ambient air. Therefore, the Reduced Project would not expose off-reservation sensitive receptors to substantial air pollution.

## Question E

Construction activities under the Reduced Project would not result in the generation of permanent or long-term objectionable odors. Odors associated with the intermittent operation of diesel-powered equipment might be detected by nearby sensitive receptors, but these odors are expected to be of short duration and are not expected to affect a substantial number of people. Excavated soil or sediment from the Reduced Project's grading activities within the confines of the reservoir may contain organic material that is decaying, which may create an objectionable odor. The intensity of the odor perceived by a receptor depends on the distance of the receptor from the construction activity and the amount and
quality of the exposed soil material. Exposed soil would be quickly reused onsite, covered to control odors, or hauled and disposed of properly offsite.

Wastewater treatment plants can generate substantial odors related to decaying organic matter. The size and type of WWTP, as well as predominant wind directions and terrain impact how odors will disperse from the source. The Reduced Project should implement Mitigation Measure 3.4-B to ensure that odors are controlled with appropriate technology to ensure operation of the facility does not result in significant off-reservation odors. With implementation of Mitigation Measure 3.4-B, the impact of objectionable odors to sensitive individuals is less than significant.

## Mitigation Measures

A. The following construction Mitigation Measure shall be implemented to reduce criteria air pollutant emissions:

- No person may cause, allow or permit fugitive dust emissions without first implementing good housekeeping and/or work practices that reduce and control the emissions to the atmosphere below $20 \%$ opacity or equivalent Ringlemann number, which is a measurement of opacity.
- Good housekeeping and/or work practices include but are not limited to the following:

1. Application of water and/or approved chemicals to control emissions in the demolition of existing buildings or structures, construction operations, solid waste disposal operations, the grading of roads and/or the clearing of land.
2. Application of asphalt, water and/or approved chemicals to road surfaces.
3. Application of water and/or suitable chemicals to material stockpiles and other surfaces that may generate fugitive dust emissions.
4. Maintenance of roadways in a clean condition by washing with water or sweeping promptly.
5. Covering or wetting material stockpiles and open-bodied trucks, trailers, or other vehicles transporting materials that may generate fugitive dust emissions when in motion.
6. Installation and use of paved entry aprons or other effective cleaning techniques to remove dirt accumulating on a vehicle's wheels on haul or access roads to prevent tracking onto paved roadways.
7. Ceasing operations until fugitive emissions can be reduced and controlled.
8. Using vegetation and other barriers to contain and to reduce fugitive emissions. Using vegetation for windbreaks.
9. Instituting good housekeeping practices by regularly removing piles of material that have accumulated in work areas and/or are generated from equipment overflow.
10. Restrict vehicle speeds to 15 miles per hour while driving on unpaved roads in order to minimize fugitive dust emissions.
B. The Reduced Project shall install and operate appropriate technology such as enclosures, aerators, and/or odor scrubbers to ensure that the WWTP does not produce significant offreservation objectional odors. If more than 2 odor complaints are received in any given month, the Tribe shall investigate and implement appropriate additional odor control measures.

| 3.5 BIOLOGICAL RESOURCES |
| :--- | :--- | :--- | :--- | :--- |
| Would the project: |

Off-reservation terrestrial habitat types in the vicinity of the Project Site include developed/disturbed, annual grassland, oak woodland, oak savanna, riparian woodland, and chaparral. Off-reservation aquatic habitat types include ephemeral, and intermittent drainages, seasonal wetlands, and stock ponds. Riparian woodland, aquatic habitats such as wetlands and drainages, and lone chaparral are considered sensitive.

## Question A

A desktop review of biological databases was conducted for the Reduced Project. The Information for Planning and Consultation (IPaC) tool of the U.S. Fish and Wildlife Service was queried for a list of federally listed threatened and endangered species that may occur in the vicinity of the Project Site or may be affected by the Reduced Project (USFWS 2023a; Appendix B). A review was conducted of the occurrence records of state and federal special-status species mapped by California Department of Fish and Wildlife (CDFW) Biogeographic Information and Observation System (BIOS) (CDFW 2023a). The California Natural Diversity Data Base (CNDDB), a database maintained by CDFW (CDFW 2023b; Appendix B), was queried and a list of federally listed special-status species was generated, as was a special status plant species lists from the California Native Plant Society (CNPS 2023) Rare Plant Inventory (RPI). The CNDDB and RBI search
area query was conducted within a radius of nine 7.5' minute USGS topographical quads from the Project Site (Appendix B).

In connection with the preparation of the EIS, biological surveys were conducted within the Project Site and off-reservation where public access was available. No special-status species were observed during surveys. Off-reservation habitats were classified and their condition was then evaluated for their potential to support regionally occurring special-status species. An assessment of off-reservation habitats supported the analysis of potential effects to sensitive biological resources (BIA, 2009). It was found that no habitats suitable for special-status species would be directly impacted.

Construction stormwater pollution run-off has the potential to indirectly impact special-status species from the degradation to water quality of aquatic habitats suitable for regionally occurring special-status species. As discussed in Section 3.1 and Section 3.7, potential impacts to off-reservation water quality standards would not have a substantial adverse impact to special-status species, with the implementation of Mitigation Measure 3.5-E.

Based on a review of surveys conducted in connection with the EIS, a 2023 survey, and a subsequent review of aerial photographs, suitable nesting habitat for birds protected by the Migratory Bird Treaty Act and eagles protected by the Bald and Golden Eagle Protection Act occurs within 500 feet of the Project Site. Construction of the off-site roadway improvements may result in the loss of some existing vegetation that may provide habitat that supports migratory birds, and could result in potentially significant effects. Indirect impacts to nesting migratory birds or eagles may occur from construction activities of the Reduced Project.

With the implementation of Mitigation Measure 3.5-E, potential impacts on nesting migratory birds and eagles from the Reduced Project would be reduced to less than significant.

## Questions B and C

The nearest critical habitat designated by United States Fish and Wildlife Service is located more than 8 miles from the Project Site (USFWS 2023b: Appendix B). The nearest critical aquatic habitat designated by the National Oceanic and Atmospheric Administration (NOAA) Fisheries also known as the National Marine Fisheries Service (NMFS) is located more than 15 miles of the Project Site (NOAA 2023a; Appendix B). The Project Site is within Chinook salmon Essential Fish Habitat (EFH) designated by NOAA (NOAA 2023b; Appendix B). The USFWS National Wetlands Inventory (NWI) (UFWS 2023c; Appendix B) and USGS and aerial photographs (Google Earth, 2023) were referenced to identify known or previously mapped wetlands or other waters of the United States adjacent to the Project Site. NWI aquatic features in the vicinity of the Project Site are shown in Figure 6.

As described in Appendix D, all wastewater generated by the Reduced Project would be treated and disposed of on-reservation. The recycled water generated at the on-site WWTP and used to irrigate landscaped areas of the Project Site would be treated to disinfected tertiary recycled water standards under Title 22 of the California Code of Regulations (CCR). None of this treated water would flow offsite and therefore would not pose an adverse effect on off-reservation wetlands or waters as defined by Section 404 of the Clean Water Act (CWA).

The construction of traffic mitigation measures is the only land disturbance that would occur offreservation. Implementation of proposed traffic mitigation measures will require the installation of a traffic signal on State Route 16 at Latrobe Road, and the widening of the Reduced Project entrance at Village Drive and Golden Chain Highway (SR 49). These locations are predominantly developed with pavement and disturbed and managed shoulder. Beyond the developed and disturbed habitat are highly disturbed annual grassland shoulder, and a roadside ditch. The vegetation on the road shoulder and ditch are regularly mowed and maintained and consists of predominantly non-native ruderal species. The roadside ditch appears to convey flows from a historical water canal system and therefore may be jurisdictional. No modifications to the roadside ditch are anticipated from construction of proposed traffic improvements. Potential environmental impacts related to the construction of traffic improvements, and the related costs, would be reduced to less than significant levels with the implementation of Mitigation Measures 3.5-A through 3.5-D and 3.5-F.

Surface water runoff from the proposed off-reservation improvements has the potential to cause impacts to water quality of sensitive habitats such as wetlands or ephemeral drainages that are downgradient. Soil disturbance from the proposed off-site traffic improvements, and the construction of the Reduced Project could result in stormwater pollution from soil erosion. These potential impacts are analyzed separately in Section 3.7. As discussed therein, potential impacts to water quality would be reduced to less than significant levels, with the implementation of mitigation.

## Question D

The Reduced Project is located outside of the "Essential Connectivity Area," of the California Essential Connectivity Project (CDFW, 2023a). The surrounding area includes SR 49, local roadways, rural and City of Plymouth development, fenced properties, grazing and vineyard operations. These elements all currently limit wildlife movement. Terrestrial wildlife movement likely occurs within the riparian habitat corridors and aquatic species in Dry Creek. However, these habitats are at lower elevations to the south and south east of the Reduced Project and therefore off-reservation interference with nursery sites of migratory fish or wildlife species or the movement through the areas with suitable habitats would be unrelated to the Reduced Project. There would be no impact.

## Question E

The Reduced Project does not change any land use designation within the Project Site, nor would it affect any off-reservation conservation areas listed in any state, regional, or local conservation plan. The Reduced Project would not have any effect on conservation areas designated in the Amador County General Plan (see Amador County, 2016). In addition, no other HCP or NCCP has been approved in the vicinity of the Project Site, such that the Reduced Project could be in conflict with such plan (CDFW, 2023c). There would be no impact.

## Mitigation Measures

A. Construction activities in the vicinity of any off-reservation jurisdictional wetland features shall be conducted during the dry season (April 15 through October 15), to the extent reasonable, to minimize potential erosion.
B. Temporary fencing shall be installed around off-reservation wetland and intermittent drainage features and associated riparian woodland that is outside of the construction area. Fencing shall be located as far as feasible from the edge of wetlands and riparian habitats and installed prior to any construction. The fencing shall remain in place until all construction activities have been completed.
C. Staging areas shall be located away from the areas of off-reservation wetland, intermittent drainage and riparian habitat that are fenced-off. Temporary stockpiling of excavated or imported material shall occur only in approved construction staging areas. Excess excavated soil shall be used on-site or disposed of at a regional landfill or other appropriate facility. Stockpiles that are to remain on the site through the wet season shall be protected to prevent erosion (e.g. tarps, silt fences, straw bales).
D. Best Management Practices (BMPs) shall be employed by the construction contractor to prevent the accidental release of fuel, oil, lubricant, or other hazardous materials associated with construction activities into jurisdictional features. In compliance with the CWA, the Tribe shall apply for coverage under the USEPA's National Pollutant Discharge Elimination System (NPDES) General Construction Permit (GCP). As part of the project's NPDES permit, a contaminant program shall be developed and implemented in the event of release of hazardous materials.
E. Site preparation activities, including tree trimming and removal, should occur outside of the birdnesting season between September 1 and January 31. If tree disturbance or other project-related activities cannot avoid the nesting season (approximately February 1 - August 31), preconstruction surveys using recognized CDFW and USFWS protocols including call count surveys shall be conducted by a qualified biologist within 14-days prior to vegetation removal or ground disturbance activities to determine presence or absence and location of nesting bird species. If active nests are present within 500-feet of construction areas, temporary protective construction exclusion zones shall be established by a qualified biologist in order to avoid direct or indirect mortality or disruption of these birds, nests or young. The appropriate buffer distance is dependent on the species, surrounding vegetation and topography and will be determined by a qualified biologist. Exclusion zones shall remain in place until all young have fledged or until the nest has been naturally abandoned or predated. Work may proceed if no active nests are found during surveys or once nests are determined by a qualified biologist to be inactive.
F. Cleared vegetation shall be collected and transported offsite to prevent birds from nesting in vegetative debris.
G. If there is a lapse in construction activity for more than 7 consecutive days or if construction activity is phased at the work site, preconstruction and nesting bird surveys shall be repeated.
H. The Tribe shall contribute to the funding of the environmental review and mitigation for traffic improvements identified in Section 3.17. The contribution shall be based on the amount of traffic generated by the Reduced Project as a percentage of the overall traffic volume. The Tribe's contribution shall include the cost of preparing environmental documents and the cost of mitigation for biological resources, including but not limited to purchases of land, contributions to mitigation banks or programs, and restoration of habitat. The Tribe's contribution shall be provided to the agency undertaking the improvement (e.g. Caltrans, Amador County, City of Plymouth).

| 3.6 CULTURAL RESOURCES Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Cause a substantial adverse change in the significance of an off-reservation historical or archeological resource? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Directly or indirectly destroy a unique offreservation paleontological resource or site or unique off-reservation geologic feature? | $\square$ | $\square$ | $\square$ | $\square$ |
| c) Disturb any off-reservation human remains, including those interred outside of formal cemeteries? | $\square$ | $\square$ | $\square$ | $\square$ |

## Questions A-C

A Cultural Resources Inventory and Evaluation of the Project Site was prepared in June 2004 and amended in July 2005. A literature and records search of the North Central Information Center ( NCIC ) of the California Historical Resources Information System was completed August 13, 2003 and an archaeological survey was conducted between August 14, 2003 and June 14, 2004. Nine historic archaeological sites, one standing historic building, and one historic district were identified during field reconnaissance of the project parcels. Six of the historic archaeological sites, the historic building, and the historic district, had previously been evaluated for inclusion on the California Register of Historical Resources and were found to be ineligible. Re-evaluation of these resources found that they were also ineligible for inclusion to the National Register of Historic Places (NRHP) (ECORP, 2005).

Due to the passage of time, a new NCIC record search was completed on October 30, 2023 (NCIC File No.: AMA-23-25). A total of 16 resources were reported in 2023 within the Project Site, with another 18 within a 0.5 -mile buffer area. Four archaeological surveys have covered the entirety of the Project Site and another ten have included portions of the Project Site buffer area. Most of the sites identified date to the historic era, however there are two prehistoric resources, a bedrock mortar outcrop and a combination of a residence, mining features, and a bedrock milling outcrop.

As described above in previous sections, with the exception of de minimis land disturbance that would occur as a result of the construction of traffic mitigation measures, the Reduced Project would not result in disturbance of off-reservation ground-based resources. As described in Section 3.17 and Section 3.19, three mitigation measures are proposed to address traffic impacts. The locations where these three Mitigation Measures would be constructed are:

- State Route 16 at Latrobe Road.
- Golden Chain Highway (SR 49) at Village Drive. This is the entrance to the Project Site.
- Golden Chain Highway (SR 49) at Randolph Street.

The last two locations are very close to each other. There are no documented resources within the
footprint of any of these locations, and therefore the proposed traffic improvements would have no Impact on known cultural resources. However, construction of these traffic improvements could result in the discovery of previously unknown buried cultural resources or human remains. Mitigation Measures
3.6-A and 3.6-B would be implemented to reduce impacts to resources uncovered during construction. There would be a less-than-significant impact with mitigation.

## Mitigation Measures

A. If unusual amounts of bone, stone, shell, glass, building materials, or other artifacts are uncovered during traffic improvement construction, all work within 50 feet of the find shall halt and the Tribe and BIA notified; a qualified professional archaeologist shall be retained to assess the find for its eligibility to the NRHP and recommend appropriate treatment measures. Construction shall not resume until appropriate assessment and treatment of the find has been completed.
B. If human remains are uncovered during construction, the County Coroner, Tribe, and BIA shall be notified immediately. If the coroner determines that the remains are Native American, compliance with the provisions of NAGPRA shall be required.

| $3.7 \quad$ GEOLOGY AND SOILS |
| :--- | :---: | :---: | :---: | :---: |
| Would the project: |

The dominant soil types on the Project Site is loams, and silty or rocky loams with low clay content (NRCS, 2019). The majority of soils identified on the Project Site belong to hydrologic group D, with the exception of ArC (Auburn Silt Loam) which is classified as hydrologic group C (NRCS, 2019). These soils are not identified as experiencing frequent ponding or flooding (NRCS, 2019). Further, the identified soils were found to have a low to moderate potential for sheet and rill erosion from wind and water. With regards to seismicity, the Project Site is located in an area with low potential for ground shaking as the closest faults are pre-quaternary. The nearest potentially active faults are part of the Bear Mountain Fault Zone, located approximately 23.5 miles north, and 11.5 miles south of the Project Site (California Geological Survey, 2023).

A recent geotechnical engineering study concluded that the location of the Project Site is one of low seismicity, and relatively shallow depth to bedrock. The risk of liquefaction and other related hazards such as slope instability, is low (Youngdahl, 2023). Although the geotechnical engineering study was conducted for the Reduced Project, the Project Site soils are characteristic of the surrounding area.

## Question A

The Project Site and off-reservation immediate surroundings are not within a designated Alquist-Priolo Fault Zone (California Geological Survey, 2021). The nearest faults and zones are approximately 11.5 miles away from the Reduced Project (USGS, 2023). As described in Section 2.1, all project structures built would be designed and constructed to meet the California Building Standards Code (including provisions related
to seismic), the California Public Safety Code and Title III of the Americans with Disabilities Act of 1990. For these reasons, the risk of exposing off-reservation people and structures to seismic hazards, and landslides is low. Off-reservation impacts are less than significant.

## Question B

Construction of the Reduced Project would involve soil disturbance in order to construct pads and/or foundations for various project components. Soils would be stored onsite to be used as fill. The Reduced Project is located on-reservation, and, aside from the entry to the reservation, soil would not be placed close to any project boundary. This would provide distance between the Reduced Project and any potential off-reservation erosion impacts.

Earth-moving activities and excavation could create the potential for off-reservation erosion should soils be transported off-reservation by stormwater. Runoff would be collected in on-reservation detention basins and would not be discharged directly off-reservation. Furthermore, prior to and during construction of the Reduced Project, the General Construction NPDES permit from the USEPA under federal requirements of the CWA will be complied with. Per the NPDES permit, a SWPPP shall be prepared and implemented prior to construction of the Reduced Project. The SWPPP will contain applicable BMPs to reduce off-reservation impacts associated with stormwater runoff that could potentially affect offreservation areas.

In the absence of mitigation measures, off-reservation soil erosion or the loss of topsoil could potentially be significant. The mitigation measures below, and the SWPPP would reduce impacts to less than significant levels.

## Mitigation Measures

A. In compliance with the Clean Water Act (CWA), the Tribe shall apply for coverage under the USEPA's National Pollutant Discharge Elimination System (NPDES) General Construction Permit (GCP). In compliance with permitting requirements, the Tribe shall develop a Storm Water Pollution Prevention Plan (SWPPP) that shall address water quality impacts associated with construction and operation of the project. Water quality control measures identified in the SWPPP shall include but not be limited to the following list.

## General Construction Activities

1. Existing vegetation shall be retained where possible. To the extent feasible, grading activities shall be limited to the immediate area required for construction.
2. Temporary erosion control measures (such as silt fences, fiber rolls, vegetated swales, a velocity dissipation structure, staked straw bales, temporary revegetation, rock bag dams, and sediment traps) shall be employed for disturbed areas.
3. No disturbed surfaces shall be left without erosion control measures in place during the winter and spring months.
4. Construction area entrances and exits shall be stabilized with crushed aggregate.
5. Sediment shall be retained on-site by a system of sediment basins, traps, or other appropriate measures.
6. A spill prevention and countermeasure plan shall be developed, if necessary, which shall identify proper storage, collection, and disposal measures for potential pollutants (such as fuel, fertilizers, pesticides, etc.) used on-site.
7. Petroleum products shall be stored, handled, used, and disposed of properly.
8. Construction materials, including topsoil and chemicals shall be stored, covered, and isolated to prevent runoff losses and contamination of groundwater.
9. Fuel and vehicle maintenance areas shall be established away from all drainage courses and designed to control runoff.
10. Sanitary facilities shall be provided for construction workers.
11. Disposal facilities shall be provided for soil wastes, including excess asphalt produced during construction.
12. The Tribe shall educate all workers in the proper handling, use, cleanup, and disposal of all chemical materials used during construction activities and provide appropriate facilities to store and isolate contaminants.
13. The Tribe shall educate all contractors involved in the project on the potential environmental damages resulting from soil erosion prior to development by conducting a pre-construction conference. Copies of the project's erosion control plan shall be distributed at this time. All construction bid packages, contracts, plans, and specifications shall contain language that requires adherence to the plan.
14. Construction activities shall be scheduled to minimize land disturbance during peak runoff periods. Soil conservation practices shall be completed during the fall or late winter to reduce erosion during spring runoff.
15. Creating construction zones and phasing construction through grading only one part of a construction zone at a time shall minimize exposed areas. If possible, grading on a particular zone shall be delayed until protective cover is restored on the previously graded zone.
16. Utility installations shall be coordinated to limit the number of excavations.
17. Preserving as much natural cover, topography, and drainage as possible shall protect disturbed soils from rainfall during construction. Trees and shrubs shall not be removed unnecessarily.
18. Disturbed areas shall be stabilized as promptly as possible, especially on long or steep slopes. Recommended plant materials and mulches shall be used to establish protective ground cover. Vegetation such as fast-growing annual and perennial grasses shall be used to shield and bind the soil. Mulches and artificial binders shall be used until vegetation is established. Where truck traffic is frequent, gravel approaches shall be used to reduce soil compaction and limit the tracking of sediment onto SR-49.
19. Surface water runoff shall be controlled by directing flowing water away from critical areas and by reducing runoff velocity. Diversion structures such as terraces, dikes, and ditches shall collect and direct runoff water around vulnerable areas to prepared drainage outlets. Surface roughening, berms, check dams, hay bales, or similar devices shall be used to reduce runoff velocity and erosion.
20. Sediment shall be contained when conditions are too extreme for treatment by surface protection. Temporary sediment traps, filter fabric fences, inlet protectors, vegetative filters and buffers, or settling basins shall be used to detain runoff water long enough for sediment particles to settle out.
21. Topsoil removed during construction shall be carefully stored and treated as an important resource. Berms shall be placed around topsoil stockpiles to prevent runoff during storm events.
22. An independent storm water inspector shall be hired by the Tribe to ensure all NPDES permitting requirements are being implemented. The inspector will have authority to require construction contractors as well as their subcontractors to stop work until all aspects of the NPDES permit are implemented.

## General Operation Measures

23. Storm drain inlets shall be labeled "No Dumping-Drains to Streams and Rivers."
24. The parking lot shall be designed to allow storm water runoff to be directed to vegetative filter strips to help control sediment and to control non-point source pollution, where possible.
25. Permanent energy dissipaters shall be included for drainage outlets.
26. The Tribe shall create, utilize, and update as necessary a maintenance plan for all BMPs for erosion and sediment control. BMPs will be selected and installed according to guidelines in the State of California Stormwater Quality Handbook and/or Caltrans Stormwater Quality Handbook.

| 3.8 Greenhouse Gas Emissions Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Generate greenhouse gas emissions, either directly or indirectly, that may have a significant impact on the off-reservation environment? | $\square$ | $\square$ | $\checkmark$ | $\square$ |
| b) Conflict with any off-reservation plan, policy, or regulation adopted for the purpose of reducing the emissions of greenhouse gases? | $\square$ | $\square$ | $\checkmark$ | $\square$ |

## Questions A and B

Global climate change is caused primarily by an increase in levels of greenhouse gas (GHG) emissions in the atmosphere. The major GHGs are carbon dioxide (CO2), methane (CH4), nitrous oxide ( N 2 O ), sulfur hexafluoride (SF6), hydrofluorocarbons (HFCs) and perfluorocarbons (PFCs). Individual GHGs are multiplied by their global warming potential to report emissions as carbon dioxide equivalents (CO2e). These GHGs absorb longwave radiant energy (heat) reflected by the earth which warms the atmosphere in a phenomenon known as the "greenhouse effect" The potential effects of global climate change include rising surface temperatures, loss in snowpack, sea level rise, ocean acidification, increase in the number of extreme eat days per year, increased occurrence and severity of wildfires and an increase in the number of drought years.

California established the first comprehensive GHG regulatory program in the U.S. and requires reduction in GHG emissions at key milestone years compared to 1990 levels. In 2020 emissions were to be equal to 1990 levels. In 2030 emissions are to be 40 percent below 1990 levels. This intermediate GHG emissions reduction target would make it possible to meet the ultimate GHG emissions reduction target of 80 percent below 1990 levels by 2050. California also has enacted mandatory reporting of GHG emissions for industrial sources and established a cap-and-trade program as part of the effort to achieve these goals. These were established in key legislation under Assembly Bill 32, Senate Bill 32 and several executive orders. The USEPA has mandatory GHG emission reporting for large industrial sources of GHG emissions. ACAPCD has not developed quantitative GHG thresholds for project-level analysis.

Table 6 provides a breakdown of project-related GHG emissions. Development of the Reduced Project would result in an increase in GHG emissions related to construction, mobile sources, and indirect sources related to electricity (combustion of fuels used to produce electricity), solid waste (solid waste decomposition at the landfill and haul trucks), wastewater processing, and water transport. CalEEMod was used to estimate construction, area, energy, mobile, stationary, water and wastewater, solid waste, and refrigeration related project-related GHG emissions. Assumptions were the same as described above for air quality.

As shown in Table 6, the combined amortized construction emissions and operational GHG emissions would be approximately 4,265 MT of $\mathrm{CO}_{2} e$ per year. Demolition of the Inn would result in a reduction of 624 MT of $\mathrm{CO}_{2} \mathrm{e}$ emissions, which was estimated using CalEEMod. This results in a net increase of 3,641

MT of $\mathrm{CO}_{2} \mathrm{e}$. The Reduced Project includes implementation of several green building standards into the design which are not fully captured in CalEEMod, as a specific reduction in energy from Title 24 building codes was not established. Additional water saving features were also not incorporated into CalEEMod. Mobile sources make up the majority of the GHG emissions from the Reduced Project. One metric used to determine if GHG emissions are less than significant is if the Reduced Project would be 15 percent below the existing vehicle miles travelled (VMT) per employee. According to the traffic impact study (Appendix E), the project average VMT per employee is 13.2 miles while the existing VMT per employee in Amador County is 17.9 miles. Since this is greater than a 15 percent reduction in employee average VMT for the County, the Reduced Project's GHG emissions would be less than significant. Thus, the Reduced Project would not conflict with the statewide goals for GHG emission reductions. The Reduced Project would not generate GHG emissions, either directly or indirectly, that may have a significant impact on the environment or conflict with an applicable plan, policy, or regulation adopted for the purpose of reducing the emissions of GHGs. The Reduced Project's contribution to cumulative effects associated with climate change is considered a less than significant impact.

TABLE 6: PROJECT-RELATED GHG EMISSIONS

| Emission Source |  |
| :--- | :---: |
| Construction (MT CO2e) | GHG Emissions <br> (Unmitigated) |
| Construction | 982 |
| Operation (MT CO22e/yr) |  |
| Area | 0.75 |
| Energy | 222 |
| Mobile | 3,749 |
| Waste | 45 |
| Water | 168 |
| Refrigeration | 2.2 |
| Vegetation | 44 |
| Amatized Construction ${ }^{1}$ |  |

## Mitigation Measures

None.

| 3.9 HAZARDS AND HAZARDOUS MATERIALS Would the project: | POTENTIALLY <br> SIGNIFICANT <br> IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Create a significant hazard to the off-reservation public or the off-reservation environment through the routine transport, use, or disposal of hazardous materials? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Create a significant hazard to the off-reservation public or the off-reservation environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment? | $\square$ | $\square$ | $\square$ | $\square$ |
| c) Emit hazardous emissions or handle hazardous or acutely hazardous materials, substances, or waste within one-quarter mile of an existing or proposed off-reservation school? | $\square$ | $\square$ | $\square$ | $\square$ |
| d) Expose off-reservation people or structures to a significant risk of loss, injury, or death involving wildland fires. | $\square$ | $\square$ | $\square$ | $\square$ |

A Phase I survey was completed in 2008 (AES, 2008) which noted the former Pioneer Mine and mine tailings on the eastern portion of the Project Site (Figure 6). Neither the Reduced Project improvements (Figures 4 and 6) nor Final EIS Alternative A project improvements (BIA, 2012) are located in the vicinity of the four former mines.

## Question A

As described in Section 2.1 and Section 3.7, grading activities of the Reduced Project would be balanced, with no significant import or export of material. In addition, as described above, the Reduced Project is not located in the vicinity of the former mining activities. Therefore, grading activities would have no impact to the off-reservation public or the off-reservation environment.

## Question B

Limited quantities of miscellaneous hazardous substances, such as gasoline, concrete reagents, fertilizers, etc. may be transported to the Project Site. Hazardous materials use on and off-reservation such as transport of various operational and facility chemicals and light disposal of conventional cleaning chemicals would be consistent with current hazardous material use on the Project Site and offreservation. Recommended mitigation measures for Final EIS Alternative A were listed in the ROD (BIA, 2012). These mitigation measures, which include BMPs, are applicable to the Reduced Project, and are listed below as Mitigation Measure 3.9-A. Off-reservation impacts from the reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment would be reduced to a less than significant level, with the incorporation of mitigation.

## Question C

There are no schools within a $1 / 4$ mile of the Reduced Project. The closest school is Plymouth Elementary School, located approximately 0.7 miles to the north of the northern border of the Project Site and Shenandoah Middle School, which is located approximately 1.0 mile to the northwest of the reservation border. In addition, the former Willow Springs School is located approximately 3.2 miles west of the Project Site. A group of local residents seek to restore the Willow Springs School. There are no known proposed new schools proposed in the vicinity of the Project Site. For these reasons, there would be no impact to existing or proposed off-reservation schools.

## Question D

Risks associated with potential off-reservation impacts from wildland fires are analyzed in Section 3.15. As discussed therein, off-reservation risks associated with wildland fires are less than significant.

## Mitigation Measures

A. Personnel shall follow written standard operating procedures (SOPs) for filling and servicing construction equipment and vehicles. These SOPs address storage and use of hazardous materials and would be implemented during both construction and operation of the casino. The SOPs, which are designed to reduce the potential for incidents involving the use and storage of hazardous materials, shall include the following where feasible and when reasonable:

1. Refueling shall be conducted only with approved pumps, hoses, and nozzles.
2. Catch-pans shall be placed under equipment to catch potential spills during servicing.
3. All disconnected hoses shall be placed in containers to collect residual fuel from the hose.
4. Vehicle engines shall be shut down during refueling.
5. No smoking, open flames, or welding shall be allowed in refueling or service areas.
6. Refueling shall be performed away from bodies of water to prevent contamination of water in the event of a leak or spill.
7. Service trucks shall be provided with fire extinguishers and spill containment equipment, such as absorbents.
8. Should a spill contaminate soil, the soil shall be put into containers and disposed of in accordance with local, state, and federal regulations.
9. All containers used to store hazardous materials shall be inspected at least once per week for signs of leaking or failure. All maintenance and refueling areas shall be inspected monthly. Results of inspections shall be recorded in a logbook that shall be maintained on-site.
10. Staging areas, welding areas, or areas slated for development using spark-producing equipment shall be cleared of dried vegetation or other materials that could serve as fire fuel. To the extent feasible, the contractor shall keep these areas clear of combustible materials in order to maintain a firebreak.
11. Any construction equipment that normally includes a spark arrester shall be equipped with an arrester in good working order.
B. The amount of hazardous materials used in project construction and operation shall be consistently kept at the lowest volumes needed.
C. During project operation, the least toxic material capable of achieving the intended result will consistently be used. These materials include industrial strength cleaners, detergents, pesticides, and degreasers. All potentially toxic materials would be used as directed according to federal labeling requirements. All materials shall be kept within their original containers and at no time would the labels be removed from the original containers.
D. A hazardous materials and hazardous waste minimization program shall be developed, implemented, and reviewed annually by the Tribe to determine if additional opportunities for hazardous materials and hazardous waste minimization are feasible, for both project construction and operation. A copy of the hazardous waste minimization program and a full inventory of flammable and hazardous materials will be provided to the Amador County Fire Department.
E. The contractor shall be requested to avoid and minimize the use of hazardous materials and petroleum products during the project's construction to the fullest extent practicable.
F. The Tribe shall minimize the use of pesticides and toxic chemicals to the greatest extent feasible in landscaping or use less toxic alternatives, such as integrated pest management techniques.
G. As part of the WWTP design, hazardous materials used for disinfection of water and treated effluent would be fully stored in the chemical room of the WWTP operations building. The storage and chemical metering facilities shall be located inside a chemical spill containment area, sized to contain 150 percent of the storage volume in case of an unintentional release. To the extent feasible, chemicals shall be stored as dry material in sealed containers, and then in a 50-gallon mixing tank when needed
H. In the event that contaminated soil and/or groundwater are encountered during construction related earth-moving activities, all work shall be halted until a professional hazardous materials specialist or a qualified individual can assess the extent of contamination. If contamination is determined to be significant, representatives of the Tribe shall consult with USEPA to determine the appropriate course of action, including the development of a Sampling Plan and Remediation Plan if necessary.
I. The Tribe shall establish a vegetative cover over mine tailings with California Flannelbush (Fremontodendron californicum), Yerba Santa (Eriodictyon crassifolium), Coyote Brush (Baccharis pilularis), or similar native plants used for soil stabilization/erosion control prior to public access to the project development. The Tribe will ensure the vegetative cover is maintained providing full coverage of the mine tailings. Additionally, the tailings area shall be fenced off to prevent public access.

| 3.10 Water Resources Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Violate any applicable off-reservation water quality standards or waste discharge requirements? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Substantially deplete off-reservation groundwater supplies or interfere substantially with groundwater recharge such that there should be a net deficit in aquifer volume or a lowering of the local groundwater table level? (e.g., the production rate of pre-existing nearby wells would drop to a level which would not support existing land uses or planned uses for which permits have been granted)? | $\square$ | $\square$ | $\square$ | $\square$ |
| c) Substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, in a manner which would result in substantial off-site erosion or siltation? | $\square$ | $\square$ | $\square$ | $\square$ |
| d) Substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, or substantially increase the rate or amount of surface runoff in a manner which would result in flooding off-site? | $\square$ | $\square$ | $\square$ | $\square$ |
| e) Create or contribute runoff water which would exceed the capacity of existing or planned storm water drainage systems or provide substantial additional sources of polluted runoff offreservation? | $\square$ | $\nabla$ | $\square$ | $\square$ |
| f) Place within a 100-year flood hazard area structures, which would impede or redirect offreservation flood flows? | $\square$ | $\square$ | $\square$ | $\square$ |
| g) Expose off-reservation people or structures to a significant risk of loss, injury, or death involving flooding, including flooding as a result of the failure of a levee or dam? | $\square$ | $\square$ | $\square$ | $\square$ |

As described in Section 2.1, water for the Reduced Project would be supplied by up to three water wells. Wastewater would be treated at an on-site WWTP, located to the east of the casino (Figure 4). The WWTP would be sized to treat the peak flows resulting from the Reduced Project. See Section $\mathbf{2 . 1}$ for a detailed description of water and wastewater infrastructure.

## Question A

As described in Appendix D, all wastewater generated by the Reduced Project would be treated and disposed of on-reservation. The recycled water generated at the on-site WWTP and used to irrigate landscaped areas of the Project Site, would be treated to disinfected tertiary recycled water standards under Title 22 of the California Code of Regulations (CCR). None of this treated water would flow offsite. Furthermore, as described in Section 3.7, the Tribe shall develop a Storm Water Pollution Prevention Plan (SWPPP) that would address water quality impacts associated with construction and operation of the project. For these reasons, impacts to off-reservation water quality standards or waste discharge requirements would be less than significant, with the incorporation of the mitigation listed in Section 3.7.

## Question B

Estimated ground water usage of the Reduced Project is 37,438 GPD (Appendix D). Final EIS Alternative A included two options for water supply. Under Option 2, which was the preferred option, water would be sourced from two groundwater wells located on the Project Site (designated as M1 and H1), and one well located adjacent to the Project Site (designated as M3). The Final EIS estimated the total sustained yield of the groundwater wells at approximately 116,640 GPD (BIA, 2009). Because these three wells are the only existing ground water sources on the Project Site and one of the adjacent properties, they represent a small fraction of the existing ground water capacity. In addition, the estimated ground water usage of the Reduced Project presents only 32 percent of Final EIS Alternative A, Option 2, which was approved in the ROD. Also, some portion of the WWTP discharge used for irrigation may contribute to ground water recharge. For these reasons, The Reduced Project would not substantially deplete off-reservation groundwater supplies or interfere substantially with groundwater recharge. Impacts would be less than significant. Impacts would be further reduced through the implementation of the mitigation measures listed below.

## Questions C and D

Approximately 9 acres of impervious surfaces would be created during construction (Section 2.1). Stormwater from newly created impervious surfaces would flow into two stormwater conveyance and detention systems. Under Option A, these stormwater improvements would consist of two stormwater ponds. Under Option B, the stormwater pond to the south would be replaced by an underground storage system. The amount of stormwater runoff resulting from the Reduced Project would be the same, or less than under existing conditions (Appendix D). In addition, as described in Section 3.7, the Tribe will develop a SWPPP that will address water quality issues associated with construction and operation of the project. As a result of these factors, impact to the existing drainage pattern of the Project Site or area would be less than significant. Impacts would be further reduced through the implementation of the mitigation measures listed below.

## Question E

The amount of stormwater runoff resulting from the Reduced Project would be the same, or less than under existing conditions (Appendix D). In addition, as described in Section 3.7, the Tribe will develop a SWPPP that will address water quality issues associated with construction and operation of the project. As a result of these factors, the Reduced Project would not create or contribute runoff water which would

exceed the capacity of existing or planned stormwater drainage systems. However, as described in Section 3.9, potential risks associated with hazardous materials (which are potential sources of pollution) would be reduced to less than significant levels with mitigation. Therefore, impacts would be less than significant with the incorporation of the mitigation listed below, and in Sections 3.7 and 3.9.

## Question F

As described in the Final EIS, (Section 3.3.2 and Figure 3.3-2) the majority of the Project Site is not located in a floodplain mapped by the Federal Emergency Management Agency (FEMA). Less than one-acre of Parcel \# 3 is within Flood Zone A, an area with a 1-percent annual chance of flooding, for which no base flood elevations have been determined (BIA, 2009). The majority of the Project Site, including the area planned for development, is within Zone $X$, an area outside the 1-percent and 0.2-percent annual chance floodplains. None of the Reduced Project improvements would be located in Flood Zone A (i.e., the 100year floodplain). There would be no impact.

## Question G

The drainage ponds described in Section 2.1 would not require a levee or dam, and thus would eliminate flooding risks associated with failure. The wastewater effluent storage pond (storage Option B) would use earthen berms in its construction. Water tanks would be used to store potable water and effluent under waste water storage Option A. Construction of the Reduced Project would adhere to the California Building Standards Code (including provisions related to seismic) and the California Public Safety Code. All water infrastructure, including ponds and tanks, would be designed by engineering professionals. For these reasons, the risk of flooding caused by failure would be less than significant.

## Mitigation Measures

A. In compliance with the Clean Water Act, the Tribe shall apply for coverage under the USEPA's NPDES GCP. In compliance with permitting requirements, the Tribe shall develop a SWPPP that shall address potential water quality impacts associated with construction and operation of the project. These measures are identified above in Mitigation Measure 3.7-A.
B. As part of the overall water sampling and monitoring program for the WWTP an irrigation field monitoring plan shall be developed and implemented to ensure potential tail water is being captured and that no tail water is discharged to surface waters. The monitoring plan will include, but not be limited to the following:

1. Water from irrigation field drift shall not migrate out of the irrigation field boundary.
2. All tail water and/or stormwater shall be collected and returned to the WWTP holding pond at all times when water is being applied to the irrigation field.
3. The Tribe shall use the irrigation fields only during periods of dry weather. The Tribe will not use the irrigation fields 24 hours prior to a forecasted rain event and will wait 24 hours after the rain event to return to irrigation field operation.
4. A tail water capture system will be operated to capture all effluent runoff, as well as stormwater runoff that occurs 24 hours after the last application of effluent to the irrigation fields.
5. The irrigation fields shall not be operated during periods of winds exceeding 30 mph .
6. A controlled 100-foot buffer shall be maintained around the irrigation field operating area.
C. The following additional conservation measures shall be implemented by the Tribe to further reduce water usage:
7. Checking steam traps and ensuring return of steam condensate to boiler for reuse.
8. Planting of drought resistant landscaping.
9. Limiting boiler blowdown and adjusting for optimal water usage.
10. Using low flow faucets and/or aerators in casino.
11. Using pressure washers and water brooms instead of hoses for cleaning.
12. Using garbage disposal on-demand in restaurant.
13. Incorporating a re-circulating cooling loop for water cooled refrigeration and ice machines in restaurants.
14. Serving water to customers on request at restaurant.
D. A sampling and monitoring program for the WWTP shall be developed and implemented. Treated effluent shall be monitored to determine the efficacy of the treatment process.

| 3.11 LAND USE |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Would the project: | POTENTIALLY <br> SIGNIFICANT <br> IMPACT | LESS THAN <br> SIGNIFICANT WITH <br> MITIGATION <br> INCORPORATION | LESS THAN <br> SIGNIFICANT <br> IMPACT | NO <br> IMPACT |
| a) Conflict with any off-reservation land use plan, <br> policy, or regulation of an agency adopted for the <br> purpose of avoiding or mitigating an <br> environmental effect? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Conflict with any applicable habitat conservation <br> plan or natural communities conservation plan <br> covering off-reservation lands? | $\square$ | $\square$ | $\square$ | $\square$ |

The Project Site is located on the Tribe's trust land within Amador County in the northwest corner of the "Amador City" USGS Quadrangle, on the southern border of the City of Plymouth, California. Most of the Project Site is undeveloped, with the exception of the Shenandoah Inn near the entrance to the Site, unpaved roads, and the remnants of an old mining station (Figure 4). The Project Site is accessible from Village Drive, via SR 49. Site topography on the site of the Reduced Project is irregular, with elevations ranging between approximately 1,000 to 1,175 feet above mean sea level (amsl).

A gas station, a donut shop, and a Mexican restaurant are located on the east side of SR 49, immediately to the west of the reservation.

## Question A

The reservation is bordered by areas under the jurisdiction of both the City of Plymouth and Amador County. Land use designations within the City of Plymouth near the Project Site include "HC - Highway Commercial" (City of Plymouth, 2014). County land use designations for off-reservation land in the vicinity of the Project Site include "RR- Rural Residential", Industrial (I), Agricultural General (AG) and "Federal Land" (Amador County, 2016). A portion of the Project Site is zoned as Highway Commercial under the City of Plymouth's General Plan (City of Plymouth, 2014). The Reduced Project would be largely consistent with the zoning within its vicinity.

The development of the Project Site would not convert designated on or off-reservation forest or farmland as the land within the vicinity of the Project Site and the Project Site itself is not reserved for agricultural or forestry uses. Consequently, development of the Reduced Project would not conflict with Amador County's General Plan (including policies outlined in its Economic Development or Conservation Chapters) with respect to impacts on agricultural resources.

For these reasons, the Reduced Project would not conflict with any off-reservation land use plan, policy, or agency adopted for the purpose of avoiding or mitigating an environmental effect.

## Question B

Amador County Resource Conservation District (ARCD) has several programs that have the potential to apply throughout the County (ARCD, 2023). These programs include Forest Health and Landowner

Assistance, Chipping Program (for reduction of roadside and residential fuels), Carbon Farm Plan (for soil health and carbon sequestration), On Farm Assistance, and the Irrigated Lands Regulatory Program. The Reduced Project will not conflict with these programs off-reservation, as the land within the vicinity of the Reduced Project is not used for farming or forestry-related operations. No other HCP or NCCP has been approved that would apply to the Reduced Project (California Department of Fish and Wildlife, 2023). There would be no impact.

## Mitigation Measures

None.

| 3.12 Mineral Resources Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Result in the loss of availability of a known offreservation mineral resource classified MRZ-2 by the State Geologist that would be of value to the region and the residents of the state? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Result in the loss of availability of an offreservation locally important mineral resource recovery site delineated on a local general plan, specific plan, or other land use plan? | $\square$ | $\square$ | $\square$ | $\square$ |

## Questions A and B

According to the Amador County General Plan Figure LU-1 the nearest MRZ is northeast of the Project Site (Amador County, 2016). The Mineral Resources Data System returns several listings for gold ore which appear to occur both on the Project Site and its vicinity (USGS, 2011). There is a mine located southwest of the Site. However, there is no evidence of recent mining activity at any of these locations. Construction and operation of the Reduced Project would have minimal effect to off-reservation mineral resources. Thus, the Reduced Project would not result in losses in the availability of any off-reservation mineral resources classified as MRZ-2. The Reduced Project would also have no impact on the availability of an off-reservation locally important mineral resource recovery site.

## Mitigation Measures

None.

| 3.13 NOISE <br> Would the project result in: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Exposure of off-reservation persons to noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies? | $\square$ | $\nabla$ | $\square$ | $\square$ |
| b) Exposure of off-reservation persons to excessive groundborne vibration or groundborne noise levels? | $\square$ | $\square$ | $\square$ | $\square$ |
| c) A substantial permanent Increase in ambient noise levels in the off-reservation vicinity of the project? | $\square$ | $\square$ | $\square$ | $\square$ |
| d) A substantial temporary or periodic increase in ambient noise levels in the off-reservation vicinity of the project? | $\square$ | $\nabla$ | $\square$ | $\square$ |

The Federal Highway Administration (FHWA) is a division of the United States Department of Transportation, and provides guidance over the construction, maintenance, and preservation of the Nation's Highways. The FWHA outlines construction thresholds for noise receptor locations and land uses, which are summarized below in Table 7.

TABLE 7: FEDERAL CONSTRUCTION NOISE THRESHOLDS

| Noise Receptor Locations and Land Uses | Daytime <br> (7 AM - 6 PM) | Evening <br> (6 PM - 10 PM) | Nighttime <br> (10 PM - 7 AM) |
| :--- | :--- | :--- | :--- | :--- |
|  | dBA, Leq1 |  |  |
| Noise Sensitive Locations (residences, institutions, <br> hotels, etc.) | 75 or Baseline +5 <br> (whichever is <br> louder) | Baseline +5 | Baseline + 5 (if <br> Baseline $<70$ or <br> Baseline +3 (if <br> Baseline > 70) |
| Commercial Areas (businesses, offices, stores, etc.) | 80 or Baseline +5 | None | None |
| Industrial Areas (factories, plants, etc.) | 85 or Baseline +5 | None | None |

Note: 1 Leq thresholds were empirically determined (FHWA, 2006).
Source: FHWA, 2006.

The FHWA also establishes Noise Abatement Criteria (NAC) for traffic noise. These criteria are based on land uses, which the FHWA defines as "activities." These criteria are outlined below In Table 8. The NAC for residential receptors is 67 dBA (FHWA, 2018).

TABLE 8: FEDERAL NOISE ABATEMENT CRITERIA HOURLY A-WEIGHTED SOUND LEVEL DECIBELS ${ }^{1}$

| Activity <br> Category | Activity <br> Criteria <br> Leq (h), dBA | Evaluation <br> Location | Activity Category Description |
| :---: | :---: | :---: | :--- |
| A | 57 | Exterior | Lands on which serenity and quiet are of extraordinary significance and serve <br> an important public need and where the preservation of those qualities is <br> essential if the area is to continue to serve its intended purpose. |
| B | 67 | Exterior | Residential. | | C |
| :---: |
| 67 |
| D |

Construction noise has the potential to reach 85 to $88 L_{\max }$ within 50 feet of activity (Table 9). Stationary point sources of construction noise decrease at a rate between 0 and 10 dBA per doubling of distance from the source, depending on environmental conditions.

TABLE 9: STANDARD CONSTRUCTION EQUIPMENT NOISE

| Type of Equipment | Maximim Level, <br> DB at 50 Feet |
| :--- | :---: |
| Backhoe | 80 |
| Compactor | 80 |
| Air Compressor | 80 |
| Dozer | 85 |
| Dump Truck | 84 |
| Excavator | 85 |
| Generator | 82 |
| Jackhammer | 85 |
| Pneumatic Tools | 85 |
| SOURCE: FHWA, 2006. |  |

Amador County regulations categorize noise thresholds from stationary sources (i.e., operational noise levels) based on land use compatibility and exterior/interior thresholds. These noise levels are measured in Community Noise Equivalent Level (CNEL). CNEL is measured at a location over 24 hour periods and
assesses a 10 dBA "penalty" in the noise-sensitive hours of 10:00 p.m. and 7:00 a.m. The Thresholds for single-family and duplex land uses are defined as 45 dBA noise levels for interior and 60 dBA for exterior (Amador County, 2016). The interior thresholds for noise generated by auditoriums, concert halls, and amphitheaters are 45 dBA .

Sensitive receptors include land uses that house or attract individuals susceptible to adverse impacts from noise pollution and should be given special consideration when evaluating the noise impacts of projects. Hospitals, schools, convalescent homes, parks, and residential areas are examples of sensitive receptors. Other land uses near the Project Site include commercial and rural residential.

## Questions A, C and D

The nearest sensitive receptors to the Project Site are two single-family residences that are located approximately 200 feet from the western boundary of the reservation, and approximately 400 feet from the western edge of the grade that would support the casino parking lot. SR 49 is located between these two houses and the casino. Thus, SR 49 traffic would be the most notable source of noise to these two houses.

## Construction

Project construction would consist of earthwork, foundation construction, erection of buildings, and finishing work. All construction would be conducted on-reservation using standard construction equipment. Construction activities associated with the Reduced Project would be intermittent and temporary. Construction of the Reduced Project would result in temporary maximum noise levels of less than or equal to approximately 67 dBA at the two nearest noise-sensitive receptors, which was calculated based on a distance of 400 feet. These noise levels are less than the Federal thresholds listed in Table 7. Effects would be less than significant.

## Construction Traffic

Construction traffic-related noise would likely be temporary and generated from construction workers and deliveries to the Project Site. These trips have the potential to increase noise on SR 49 within the immediate vicinity of the Project Site. Construction employees would be expected to conduct work between the hours of 7:00 a.m. and 4:00 p.m. As described in Appendix E, 15 heavy equipment truck trips are estimated throughout the demolition and construction of the Reduced Project. Construction material import and export would produce approximately 10 truck trips per day. Construction would generate approximately 130 vehicle trips during peak construction. Non-worker visits generated by deliveries or other visits would be approximately 20 to 30 trucks and automobiles per day.

There are currently approximately 14,000 daily trips on SR 49 (Appendix E). Hourly traffic is highest during peak PM commute hours (Appendix E, Table 3). Because the level of construction traffic would be relatively small in the context of baseline traffic levels, and because the construction traffic would be concentrated before peak PM traffic level, noise impacts from construction traffic would be less than significant.

## Operations Traffic

Noise levels related to the operation of the Reduced Project would be limited to traffic-related noise, noise generated from building operations (mostly HVAC units) and noise generated by events held at the outdoor entertainment venue. Given that the speed limit on SR 49 is 50 to 55 miles per hour, automobiles would generate estimated noise levels of up to 72 dB at a distance of 50 feet (Noise Pollution Clearinghouse, 2023). The Final EIS analyzed the operational traffic noise for Alternative A, and concluded that post-project traffic noise levels would be 63 Leq at a distance of 100 feet, and the change in noise stimulated by Alternative A would be 2 Leq (BIA, 2009). These levels are below the Noise Abatement Criteria identified by FHWA (Table 8). Traffic generated by the Reduced Project would be substantially less than that generated by EIS Alternative A. For these reasons, noise generated by operations traffic would be less than significant.

## Operations - Mechanical Equipment

A combination of chillers, compressors, fans, condensers, and pumps would be needed to meet the refrigeration and HVAC requirements of the Reduced Project. The Final EIS estimated noise levels from mechanical sources. Noise levels for Final EIS were estimated at $49 L_{\text {max }}$ at a distance of 400 feet to the two nearest sensitive receptors (BIA, 2009). Because the Reduced Project is substantially smaller in size that Final EIS Alternative A, noise levels would be lower. This noise level is lower than the 60 dBA exterior noise threshold established by Amador County. In addition, as described above, SR 49 is located between these two houses and the casino. Thus, SR 49 traffic would be the most notable noise source to these two houses. Any intervening structures or rooftop shielding would further reduce this predicted noise level. Nonetheless, because mechanical equipment noise levels can be variable, this is considered to be a potentially significant impact. The mitigation identified below is proposed to reduce impacts to less than significant levels.

## Operations - Loading Dock

Operation of the Reduced Project loading dock has the potential to create noise. However, the loading dock would be positioned on the east side of the casino structure, which would be approximately 800 feet from the two nearest sensitive receptors to the west. In addition, because of its location, the entire casino structure would shield the loading dock from the sensitive receptors. Loading dock activities would generate noise levels that would barely be perceptible to the sensitive receptors.

## Operations - Other Sources

The outdoor entertainment venue would be capable of seating 320 individuals. The noise generated from events at this venue would consist of entertainment noise (outdoor music) and talking. The County's exterior 60 dBA noise threshold for residential receptors (see above) would apply. The distance from the outdoor entertainment venue to the two residential receptors to the west is estimated at 800 feet. Noise measurements at a 2008 outdoor rock concert estimated noise levels of approximately 94 dBA Leq at a distance of 100 feet from the stage, and 56 dBA Leq at a distance of 800 feet (MEC, 2008). The latter would be below County noise threshold of 60 dBA , but in excess of the post 10:00 p.m. threshold, which is when the 10 dBA penalty applies. It should be noted that the Reduced Project outdoor entertainment venue would seat substantially less patrons than the rock concert described above. In addition, the outdoor entertainment venue is located on the north side of the casino building, and thus the sensitive
receptors are partially shielded. For these reasons, noise impacts would be less than significant prior to 10:00 p.m., but potentially significant after 10:00 p.m. Mitigation listed below would reduce noise levels to less than significant levels.

## Question B

As described above, the two nearest sensitive receptors are located approximately 200 feet to the west of the western boundary of the reservation and approximately 400 feet west to the earthworks that support the closest on-reservation parking lot. Parking lot construction would be the source of potentially significant vibration inducing construction activities. Thus, given the distance between sensitive receptors and sources of groundborne vibration and groundborne noise, groundborne vibration and groundborne noise levels would be negligible. There would be no impact.

## Mitigation Measures

A. Outdoor construction activities shall be limited to the hours of 6 a.m. to 6 p.m., Monday through Saturday.
B. Between the hours of 10:00 p.m. and 7:00 a.m., music sound generated at the outdoor entertainment venue shall be reduced to levels that are only audible to persons present at the venue.
C. Roof mounted mechanical equipment shall be designed and installed so that noise levels from the mechanical equipment shall not exceed 60 Leq at existing residential property lines.
\(\left.$$
\begin{array}{|l|c|c|c|c|}\hline \text { 3.14 POPULATION AND HOUSING } \\
\text { Would the project: }\end{array}
$$ $$
\begin{array}{c}\text { POTENTIALLY } \\
\text { SIGNIFICANT } \\
\text { IMPACT }\end{array}
$$ $$
\begin{array}{c}\begin{array}{c}\text { LESS THAN } \\
\text { SIGNIFICANT WITH } \\
\text { MITIGATION } \\
\text { INCORPORATION }\end{array}\end{array}
$$ \begin{array}{c}LESS THAN <br>
SIGNIFICANT <br>

IMPACT\end{array}\right]\)| NO |
| :---: |
| IMPACT |

As described in Section 2.1, the Reduced Project would be constructed within the Tribe's reservation, which is in Amador County (County) and located on the southern border of the City of Plymouth. The 2020 County population was estimated at 39,023 residents (US Census Bureau, 2020) and the 2021 population was an estimated 40,095 residents (US Census Bureau, 2021a). This represents an approximate 1,072 increase since 2020. According to the Amador County General Plan’s Housing Element, the County population is expected to increase to approximately 45,100 by the year 2060 (Amador County, 2015). The City of Plymouth estimated population was 1,138 in 2021 (US Census Bureau, 2021a). Population and employment data is summarized in Table 10.

TABLE 10: 2021 CENSUS AND EMPLOYMENT DATA

| Location | Population | Labor Force | Labor Force <br> Participation | Unemployment <br> Rate |
| :--- | :---: | :---: | :---: | :---: |
| Amador County | 40,095 | 16,213 | 15,114 | $3.2 \%$ |
| City of Plymouth | 1,138 | 622 | 593 | $2.9 \%$ |
| Source: U.S. Census Bureau, 2021a; U.S. Census Bureau, 2021b. |  |  |  |  |

As shown in Table 11, there were approximately 18,708 total housing units in the County in 2021. Of these total housing units, approximately 3,311 were vacant.

TABLE 11: 2021 REGIONAL HOUSING DATA

| Location | Total Housing <br> Units | Percent <br> Vacant | Estimated <br> Vacant Units |
| :--- | :---: | :---: | :---: |
| Amador County | 18,708 | $17,7 \%$ | 3,311 |
| City of Plymouth | 524 | $11.8 \%$ | 62 |

Source: U.S. Census Bureau, 2021c, with the exception of Estimate Vacant Units, where were calculated by multiplying the Housing Units by the Estimated Percent Vacant.

The Regional Housing Needs Allocation (RHNA) process identifies the total number of housing units, separated into four affordability levels, that local governments must plan to accommodate. As part of this process, a Housing Element is a required component of the General Plan, requiring updates with the State Housing Cycle. Amador County is currently leading the effort, in coordination with the cities of Amador City, Ione, Plymouth, Jackson, and Sutter Creek to prepare the Countywide $6^{\text {th }}$ Cycle Housing Element Update (Amador County, 2023b).

The Housing Element includes a Housing Plan, which lists specific quantified objectives. These are summarized in Table 12 for the Project Site and general vicinity.

TABLE 12: 2021-2029 QUANTIFIED OBJECTIVES

| Jurisdiction | Extremely <br> Low: <30\% <br> AMI | $\begin{array}{\|c} \text { Very Low: } \\ 30-50 \% \\ \text { AMI } \end{array}$ | Low: 5080\% AMI | Moderate: <br> 80-120\% <br> AMI | Above Moderate: 120\% + AMI | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Amador County: |  |  |  |  |  |  |
| New Construction | 25 | 25 | 50 | 60 | 134 | 294 |
| Rehabilitation and Maintenance | 15 | 15 | 10 | 20 | 100 | 180 |
| Conservation/Preservation | 809 | 1,072 | 1,671 |  |  |  |
|  |  |  |  |  |  |  |
| City of Plymouth: |  |  |  |  |  |  |
| New Construction | 10 | 10 | 20 | 5 | 13 | 58 |
| Rehabilitation and Maintenance | 3 | 3 | 2 | 5 | 25 | 34 |
| Conservation/Preservation | 8 | 65 | 70 |  |  |  |
|  |  |  |  |  |  |  |
| SOURCE: Amador County, 2023b. Housing Plan Table 2. AMI is an abbreviation for Area Median Income. |  |  |  |  |  |  |

## Question A

The Reduced Project would be a source of temporary employment during construction. The majority of workers are expected to reside locally or stay at regional hotels. Construction of the Proposed Project would generate approximately 300 temporary jobs (Section 2.1), although these employment positions would not occur simultaneously, as construction would be phased. Operation of the Reduced Project would occur once construction is largely complete, and would employ approximately 240 staff on a part-time to full-time basis (Section 2.1).

The 2021 unemployment rate for Amador County was 3.2 percent (Table 10), which equates to approximately 520 persons. Many or most operational employees would be comprised of permanent residents who currently live in Amador County. Many individuals seeking employment associated with the Reduced Project would likely be unemployed or underemployed. As described in Section 1.1, it is estimated that operations of the Reduced Project would employ approximately 240 persons. Although it is anticipated that the majority of these employees would already reside locally, there is room for accommodation to the extent that some relocation occurs. The anticipated number of employees constitutes approximately 0.6 percent of the population of Amador County. The Proposed Project would not Induce substantial off-reservation population growth. There would be a be less than significant impact.

## Question B

The Reduced Project does not include the construction, demolition, or displacement of housing. It is expected that most of the approximately 240 Reduced Project employees already reside in the County.

Some number of employees may commute to work from outside of Amador County, especially during construction of the Reduced Project, although construction would be temporary. However, some individuals may permanently relocate to the area to reduce the amount of time spent commuting. These employees and their families could be accommodated by existing vacant housing within the county.

The planned number of new low, very low and extremely low housing units in Amador County, as set forth in the Amador County Housing Plan, is 50, 25 and 25, respectively (Table 12). These 100 new housing units would comprise approximately 0.5 percent of the 18,708 current Amador County Housing units (Table 11). This is a relatively small percentage. Because of the moderate-income levels of typical casino employees, most of these workers would not be classified as low income. Thus, any in-migrating employees would not stimulate significant new demand for low-income housing. On average, employment at the Reduced Project would cause their income to increase, and their need for low income housing would stay the same or decrease.

For these reasons, the Reduced Project would not displace substantial numbers of existing housing (including affordable housing), necessitating the construction of replacement housing elsewhere offreservation. There would be a be less than significant impact.

## Mitigation Measures

None.

| 3.15 PUBLIC SERVICES Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Result in substantial adverse physical impacts associated with the provision of new or physically altered off-reservation governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or other performance objectives for any of the off-reservation public services: |  |  |  |  |
| i) Fire protection? | $\square$ | $\square$ | $\square$ | $\square$ |
| ii) Police protection? | $\square$ | $\checkmark$ | $\square$ | $\square$ |
| iii) Schools? | $\square$ | $\square$ | $\checkmark$ | $\square$ |
| iv) Parks? | $\square$ | $\square$ | $\checkmark$ | $\square$ |
| v) Other public facilities? | $\square$ | $\square$ | $\square$ | $\square$ |

## Fire Protection and Emergency Medical Services

The Amador Fire Protection District provides fire and emergency medical services (EMS) in the vicinity of the Project Site. The Amador Fire Protection District provides service to over 20,000 residents and 491 square miles of unincorporated Amador County and the City of Plymouth (Amador Fire Protection District, 2023). Fire resources are dispatched through CalFire ECC in Camino (Mountain Valley Emergency Services, 2023). The closest fire station to the Project Site is Fire Station 122, which is located about 1.0 mile to the north.

The Project Site is located in an area of high wildfire threat and the Project Site contains grassland, which is a wildfire threat in the area (COSFM, 2023). The California Department of Forestry and Fire Protection (CAL FIRE) aids local fire departments in wildfire situations. All the areas immediately outside of the reservation boundary are served by fire protection agencies. Lands within the City of Plymouth boundaries are served by the Amador Fire Protection District. Lands outside of the City limits and off-reservation are located within the State Responsibility Area (CBFFP, 2023) where CAL FIRE has a responsibility to provide wildland fire protection services. Because the reservation is federal land, the Project Site is not located in a State Responsibility Area (CBFFP, 2023). However, CAL FIRE is responsible for wildland fire protection, via a cooperative agreement with the Federal Government (CAL FIRE, 2023).

The exclusive provider of ambulance services within the County is American Legion Ambulance, which receives calls dispatched from the Amador County Sheriff's Department. Air ambulance service within Amador County is provided by several providers (Mountain Valley Emergency Services, 2023).

The nearest hospital to the Reduced Project is the Sutter-Amador Hospital located at 200 Mission Boulevard in Jackson, California.

## Law Enforcement

The Project Site is located within the service area of the Amador County Sheriff's Office (ACSO), which has jurisdiction to enforce criminal laws on the Reservation as authorized by Public Law 280. ACSO has various divisions (Amador County Sheriff's Office, 2023):

- Administration - Administrative functions, records request, process services and permits.
- Corrections - Operates the Amador County Correctional Facility. Also provides security services to the Amador Superior Court.
- Operations - Includes the Patrol Bureau, Investigation Bureau and Coroner. Approximately 27 deputies are assigned to the Patrol Bureau.

The ACSO is located at 700 Court Street Jackson, California. ACSO law enforcement activities are integrated with police departments of Amador County cities that maintain their own law enforcement presence. Police departments within the County are the Jackson Police Department, Sutter Creek Police Department, and the lone Police Department.

The Amador County District Attorney prosecutes cases that result from law enforcement actions in the County. The California Highway Patrol (CHP) has jurisdiction for traffic enforcement in the vicinity of the Project Site.

## Schools

The Amador County School District is comprised of 13 schools, six elementary schools, one primary school, two junior high schools, three high schools, one independent study, and one continuing high school (Amador County Unified School District, 2018). There are approximately 4,016 students enrolled in the district, with a student to teacher ratio of 20.09 (National center for Education Statistics, 2022). As described in Section 3.9, the closest school is Plymouth Elementary School, located approximately 0.7 miles to the north of the northern border of the Project Site and Shenandoah Middle School, which is located approximately 1.0 mile to the northwest of the reservation border.

## Parks

The nearest park is approximately 1.0 mile to northwest of the Reduced Project.

## Other Public Facilities

As described in the Final EIS, waste originating from Amador County that cannot be recycled is disposed of at the Sacramento County Landfill (Kiefer Landfill), which is located at 12701 Kiefer Boulevard in Sloughhouse. The landfill is approximately 1,084 acres (660 disposal acres), and is located approximately 20 miles west of the Reduced Project. The Kiefer Landfill is classified as a solid waste disposal facility with a permitted capacity of 10,815 tons/day, with an average day receiving rate of 2,050 tons/day. This facility has an estimated closure date of 2064 (CalRecycle, 2023), which is approximately 40 years in the future. Solid waste would be generated during the construction of the Reduced Project.

## Question A

## Fire Protection and Emergency Medical Services

As described in Section 2.1, construction and operation of the Reduced Project would occur within the reservation boundaries. CAL FIRE would continue to provide protection from wildfires, during both construction and operations of the Reduced Project. More typical fire protection and EMS services would likely be provided by the Amador Fire Protection District. EMS services would be provided by both the Amador Fire Protection District and American Legion Ambulance.

Construction-related impacts include the potential fire threat associated with equipment and vehicles coming into contact with vegetated areas. Construction vehicles and equipment such as welders, torches, and grinders may accidentally spark and ignite vegetation or building materials. The increased risks of fire during the construction of the Reduced Project would be similar to that found at other construction sites in the area. Mitigation measures listed in Section 3.9 would reduce the risk of fires started by construction to less than significant levels. Potential for calls for EMS generated by construction would be similar to that of demands placed by the construction of other projects constructed within the vicinity of the Reduced Project and would be minimal and temporary.

The operation of the Reduced Project would result in casino patronage, which would cause an increase in demand for fire and emergency services. The Reduced Project is substantially smaller than any of the alternatives analyzed in the EIS (see Section 2.2) and would not generate the need for existing infrastructure to be expanded or entirely new facilities to be built. However, the increase in demand for services would cause the Amador County Fire District to incur additional costs. In the absence of mitigation payments, the level of services provided by the Amador Fire Protection District could be affected. Impacts would be less than significant, with the implementation of the mitigation measures listed below.

## Law Enforcement

The ACSD would continue to provide services to the Project Site, once construction and operations commence. The operation of the Reduced Project would result in casino patronage, which would cause an increase in law enforcement services. The Reduced Project is substantially smaller than any of the alternatives analyzed in the EIS (see Section 2.2) and would not generate the need for existing infrastructure to be expanded or entirely new facilities to be built. However, the increase in demand for services would cause the ACSD to incur additional costs. In the absence of mitigation payments, the level of services provided by the ACSD could be affected. Impacts would be less than significant, with the implementation of the mitigation measures listed below.

## Schools

Similar to housing, potential effects to schools relate to the number of workers who in-migrate to the local area. As described in Section 3.14, a small number of workers may relocate to Amador County to fill open jobs. It is not anticipated that there will be enough employees with children who in-migrate to make a significant impact on the number of students in the Amador County School District. There would be a less than significant impact.

## Parks

Because the number of workers who in-migrate to the local area would be small in the context of the existing population, the Reduced Project would have a minimal impact on parks and other off-reservation public recreation facilities. There would be a less than significant impact.

## Other Public Facilities

Potential solid waste from construction are expected to include paper, wood, glass, plastics from packing materials, waste lumber, excess concrete, excess metal, insulation, and empty non-hazardous chemical containers. Production of construction waste would be limited and temporary in nature and would not exceed capacity of waste collection facilities. Generation of solid waste during the operation of the Reduced Project would be similar to other commercial enterprises. Because the Kiefer Landfill has an estimated remaining life of 40 years, the landfill has adequate capacity to absorb solid waste generated by the Reduced Project.

## Mitigation Measures

## Construction Related Solid Waste

A. The Tribe shall create and maintain an aggressive Waste Management Plan that implements recycling strategies to voluntarily meet State recycling and diversion requirements. The Waste Management Plan shall include the installation of a trash compactor for cardboard and paper products, and the placement of recycling bins throughout the construction area and facilities for glass, cans and paper products.
B. Environmentally preferable materials shall be acquired to the extent practical for construction of facilities.

## Operational Solid Waste

C. A trash compactor shall be installed for cardboard and paper products.
D. Recycling bins shall be installed throughout the facilities for glass, cans and paper products.
E. The Tribe shall adopt universal waste recycling requirements similar to California's Universal Waste Rule.

## Public Health and Safety

## Law Enforcement

F. The Tribe shall adopt a Responsible Alcoholic Beverage Policy that shall include, but not be limited to, requesting identification and refusing service to those who have had enough to drink. This policy shall be discussed with the California Highway Patrol and the ACSO.
G. All parking areas shall be well lit to prevent areas that would not be visible by patrolling security guards, and monitored by parking staff, and/or roving security guards at all times during operation. This will aid in the prevention of auto theft and other related criminal activity.
H. Exterior areas surrounding the gaming facilities not designed as patron waiting areas shall have "No Loitering" signs in place, shall be well lit to increase the visibility of security features (cameras and guards), and shall be patrolled regularly by roving security guards. This will aid in the prevention of illegal loitering and all crimes that relate to, or require, illegal loitering.
I. The Tribe shall provide traffic control with appropriate signage and the presence of traffic control staff when appropriate. This will aid in the prevention of off-site parking, which could create possible security issues.
J. The Tribe shall provide payments to Amador County to mitigate increased costs related to law enforcement actions generated by the Reduced Project. Prior to commencement of operations, the Tribe shall negotiate in good faith to provide reasonable payment for services with Amador County. As described in Section 1.2, if such an agreement is not entered into, the Tribe will enter into an enforceable binding letter agreement with the State of California under which the Tribe shall agree to perform the required mitigation pursuant to section 11.5(c) of the Compact.

## Emergency Call Taking and Dispatching

K. The Tribe shall negotiate in good faith to make a reasonable contribution to Amador County to cover increased operating costs of emergency dispatching in Amador County including dispatching contracted through the State that is attributable to the operation of the Reduced Project. As described in Section 1.2, if such an agreement is not entered into, the Tribe will enter into an enforceable binding letter agreement with the State of California under which the Tribe shall agree to perform the required mitigation pursuant to section 11.5(c) of the Compact.

## Fire and EMS

L. The Tribe shall provide payments to Amador Fire Protection District (District) to mitigate increased costs to the District as they relate to fire protection and emergency medical services generated by the Reduced Project. Prior to commencement of operations, the Tribe shall negotiate in good faith to provide reasonable payment for services with the District. As described in Section 1.2, if such an agreement is not entered into, the Tribe will enter into an enforceable binding letter agreement with the State of California under which the Tribe shall agree to perform the required mitigation pursuant to section 11.5(c) of the Compact.

| 3.16 RECREATION Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Increase the use of existing off-reservation neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated? | $\square$ | $\square$ | $\square$ | $\square$ |

## Question A

As described above in Section 3.15, the Reduced Project would not result in a significant increase in the use of off-reservation recreational facilities nor require the construction or expansion of other recreational facilities that could result in adverse physical effects on the environment. There would be a less than significant impact.

## Mitigation Measures

None.

| 3.17 TRANSPORTATION / TRAFFIC <br> Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the off-reservation circulation system, taking into account all modes of transportation including mass transit and nonmotorized travel and relevant components of the circulation system, including, but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Conflict with an applicable congestion management program, including, but not limited to, level of service standards and travel demand measures, or other standards established by the county congestion management agency for designated off-reservation roads or highways? | $\square$ | $\square$ | $\square$ | $\square$ |
| c) Substantially increase hazards to an off-reservation design feature (e g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)? | $\square$ | $\square$ | $\square$ | $\square$ |
| d) Result in inadequate emergency access for offreservation responders? | $\square$ | $\square$ | $\square$ | $\square$ |

A transportation impact study (TIS) was prepared for the Project (Appendix E). The TIS describes the existing and future conditions for transportation with and without the Project.

## Standards and Objective

Caltrans - The California Department of Transportation (Caltrans) has jurisdiction over State highways. Therefore, Caltrans controls all construction, modification, and maintenance of State highways, such as State Route 49 (SR 49). Any improvements to these roadways would require Caltrans' approval.

Amador County Transportation Commission (ACTC) - Amador County has designated the ACTC as the agency responsible for monitoring the network of key roadways that carry the majority of the County's traffic. This network, the Congestion Management Plan (CMP) network, was created to monitor roadway performance in relation to established LOS standards and recommend improvement when LOS is found to be deficient. The Highway Capacity Manual's (HCM) recommended practice for evaluation of traffic operations on urban streets involves calculating free-flow speeds of the roadway and assigning a LOS.

Amador County General Plan - The Transportation and Circulation Element included in the Amador County General Plan was prepared pursuant to Section 65302(b) of the California Government Code. The Transportation and Circulation Element addresses the location and extent of existing and planned transportation routes, terminals, and other local public utilities and facilities. The General Plan identifies
roadway and transit goals and policies that have been adopted to ensure that the transportation system of the County will have adequate capacity to serve planned growth. These goals and policies are intended to provide a plan and implementation measures for an integrated, multi-modal transportation system that will safely and efficiently meet the transportation needs of all economic and social segments of the County.

City of Plymouth General Plan - The Circulation Element included in the City of Plymouth General Plan also identifies roadway and transit goals and policies that have been adopted to ensure that the transportation system of the City will continue to have adequate capacity to serve planned growth.

## Existing Conditions

The primary basis of the analysis is the peak hour level of service for the key intersections. The hours identified as the "peak" hours are generally between 7:15 a.m. and 8:15 a.m. and 4:00 p.m. and 5:00 p.m. for the transportation facilities described, based on the intersection turning movement counts collected for this analysis. These peak hours will be identified as the AM and PM peak hours. These volumes represent the conditions on a typical weekday (Tuesday through Thursday). The peak hour of casino traffic generally occurs after the PM peak hour of adjacent street traffic but to be conservative the analysis assumes the peak hour of casino traffic combined with the peak hour street traffic in the afternoon (4:00 p.m. and 5:00 p.m.). An analysis of project impacts on Friday evening traffic conditions (the worst-case scenario) is presented in Appendix E.

It should be noted that the final traffic study prepared for the Final EIS clearly indicated the Friday plus project scenario was essentially the worst-case scenario at all of the project study intersections. Although the casino would generate slightly higher volumes on a Saturday afternoon, the Saturday afternoon background traffic is so much lower than Friday afternoon traffic that Saturday conditions come out substantially better than Friday conditions in all cases. Therefore, the Friday analysis is considered the worst-case scenario and no additional useful information about the potential for project impacts would be anticipated even if additional analysis of Saturday afternoon conditions was conducted.

Bicycle and pedestrian facilities in the project study area are currently very limited with no bike lanes or sidewalks provided in the vicinity of the project. Bicycle paths, lanes and routes are typical examples of bicycle transportation facilities, which are defined by Caltrans as being in one of the four classes.

Bus transit service in the project area is provided by Amador Transit. Amador Transit operates local bus route 3 within the City of Plymouth. The route operates twice a day with stops near the project site Monday through Friday from about 8:30 a.m. to 4:00 p.m. Limited Saturday service is also offered. The routes provide connections to regional transit via intercity routes 1, 2, and 7. The nearest bus stops to the project are located adjacent to the site at the intersection of Village Drive at SR 49.

## Intersection Analysis Methodology

Existing operational conditions at the eleven (11) study intersections have been evaluated according to the requirements set forth by the Amador County and City of Plymouth General Plans. Analysis of traffic operations was conducted using the $6^{\text {th }}$ Edition of the Highway Capacity Manual (HCM) Level of Service
(LOS) methodology with Synchro software. Level of service is an expression, in the form of a scale, of the relationship between the capacity of an intersection (or roadway segment) to accommodate the volume of traffic moving through it at any given time.

The level of service scale describes traffic flow with six ratings ranging from $A$ to $F$, with " $A$ " indicating relatively free flow of traffic and " $F$ " indicating stop-and-go traffic characterized by traffic jams. As the amount of traffic moving through a given intersection or roadway segment increases, the traffic flow conditions that motorists experience rapidly deteriorate as the capacity of the intersection or roadway segment is reached. Under such conditions, there is general instability in the traffic flow, which means that relatively small incidents (e.g., momentary engine stall) can cause considerable fluctuations in speeds and delays that lead to traffic congestion. This near-capacity situation is labeled level of service (LOS) E. Beyond LOS E, the intersection or roadway segment capacity has been exceeded, and arriving traffic will generally exceed the ability of the intersection to accommodate it.

## Existing Conditions

Existing traffic conditions are shown below in Table 13.

TABLE 13: EXISTING INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | PEAK HOUR | EXISTING |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | LOS |
| 1 | GOLDEN CHAIN HWY (SR 49) \& MILLER WAY |  | Side Street Stop | AM | 9.0 | A |
|  |  | PM |  | 9.1 | A |
| 2 | GOLDEN CHAIN HWY (SR 49) \& MAIN STREET | Roundabout | AM | 4.4 | A |
|  |  |  | PM | 4.9 | A |
| 3 | GOLDEN CHAIN HWY (SR 49) \& POPLAR STREET | Side Street Stop | AM | 10.0 | B |
|  |  |  | PM | 10.1 | B |
| 4 | GOLDEN CHAIN HWY (SR 49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | AM | 15.9 | C |
|  |  |  | PM | 14.8 | B |
| 5 | GOLDEN CHAIN HWY (SR 49) \& 49ER VILLAGE / EMPIRE STREET | Side Street <br> Stop | AM | 12.1 | B |
|  |  |  | PM | 13.0 | B |
| 6 | GOLDEN CHAIN HIGHWAY (SR 49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street Stop | AM | 13.5 | B |
|  |  |  | PM | 15.7 | C |
| 7 | GOLDEN CHAIN HIGHWAY (SR 49) \& SR16 | Signalized | AM | 11.9 | B |
|  |  |  | PM | 11.9 | B |
| 8 | SR 16 \& PLYMOUTH HIGHWAY (SR 124) | Side Street <br> Stop | AM | 12.6 | B |
|  |  |  | PM | 14.5 | B |
| 9 | SR 16 \& LATROBE ROAD | Side Street Stop | AM | 15.2 | C |
|  |  |  | PM | 19.7 | C |
| 10 | JACKSON ROAD (SR 16) \& IONE ROAD | Side Street Stop | AM | 15.2 | C |
|  |  |  | PM | 17.4 | C |
| 11 | JACKSON ROAD (SR 16) \& GRANT LINE ROAD | Signalized | AM | 57.9 | E |
|  |  |  | PM | 77.5 | E |

Source: Appendix E, Table 3.

## Project Trip Generation

The peak-hour trip generation of the proposed casino was reviewed based on information published in Institute of Transportation Engineers (ITE) Trip Generation Manual (Eleventh Edition, 2021). The trip generation forecasts include all traffic in and out of the site including patrons, employees, vendors, and deliveries. The trip generation forecasts are presented in Table 14.

TABLE 14: PROJECT TRIP GENERATION CALCULATIONS

| Land Use | Size | ADT | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Indian Casino Trip Rates Trips per Square Feet |  | 98.21 | 1.78 | 1.64 | 3.42 | 3.10 | 3.64 | 6.74 |
| Proposed Casino Expansion Trip Generation | $\begin{gathered} 25,200 \\ \text { sq. ft. } \end{gathered}$ | 2,475 | 45 | 41 | 86 | 78 | 92 | 170 |
| ITE Hotel Trip Rates - Trips per Room |  | 7.99 | 0.26 | 0.20 | 0.46 | 0.30 | 0.29 | 0.59 |
| Shenandoah Inn Trip Generation (To be demolished) | $\begin{gathered} 46 \\ \text { rooms } \end{gathered}$ | 368 | 12 | 9 | 21 | 14 | 13 | 27 |
| Net New Project Trip Generation |  | 2,108 | 33 | 32 | 65 | 64 | 79 | 143 |

Source: Appendix E, Table 4.

## Question A

## Baseline Plus Project Traffic Capacity

The Baseline plus project traffic forecasts were developed by adding traffic from the Project to the baseline traffic volumes. The traffic volumes for each of the study intersections for the Baseline Plus Project scenario are shown in Figure 8 of Appendix E. As shown in Table 15, all of the study intersections would continue to have acceptable conditions under the Baseline Plus Project scenario during the weekday AM and PM peak hours, with the exception of Jackson Road (SR 16) at Grant Line Road. The intersection of Jackson Road (SR 16) and Grant Line Road is forecast to exceed the LOS standards regardless of whether or not the Reduced Project is implemented and the Project would not increase the average delay by more than five seconds per vehicle.

TABLE 15: BASELINE PLUS PROJECT INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION | CONTROL | PEAK <br> HOUR | BASELINE |  | BASELINE PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Delay | LOS | Delay | LOS |
| GOLDEN CHAIN HWY (SR 49) \& MILLER WAY | Side Street Stop | AM | 9.3 | A | 9.3 | A |
|  |  | PM | 9.4 | A | 9.5 | A |
| GOLDEN CHAIN HWY (SR 49) \& MAIN STREET | Roundabout | AM | 4.9 | A | 5.0 | A |
|  |  | PM | 5.7 | A | 5.9 | A |
| GOLDEN CHAIN HWY (SR 49) \& POPLAR STREET | Side Street Stop | AM | 10.6 | B | 10.7 | B |
|  |  | PM | 10.9 | B | 11.0 | B |
| GOLDEN CHAIN HWY (SR 49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | AM | 19.5 | C | 20.0 | C |
|  |  | PM | 18.2 | C | 19.0 | C |
| GOLDEN CHAIN HWY (SR 49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | AM | 14.5 | B | 14.8 | B |
|  |  | PM | 16.8 | C | 17.5 | C |
| GOLDEN CHAIN HIGHWAY (SR 49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street Stop | AM | 18.0 | C | 19.6 | C |
|  |  | PM | 24.1 | C | 32.4 | D |
| GOLDEN CHAIN HIGHWAY (SR 49) \& SR 16 | Signalized | AM | 19.2 | B | 19.6 | B |
|  |  | PM | 19.7 | B | 20.2 | C |
| SR 16 \& PLYMOUTH HIGHWAY (SR 124) | Side Street Stop | AM | 13.8 | B | 14.1 | B |
|  |  | PM | 17.2 | C | 18.6 | C |
| SR 16 \& LATROBE ROAD | Side Street Stop | AM | 17.8 | C | 18.6 | C |
|  |  | PM | 29.2 | D | 34.7 | D |
| JACKSON ROAD (SR 16) \& IONE ROAD | Side Street Stop | AM | 16.9 | C | 17.4 | C |
|  |  | PM | 20.3 | C | 21.7 | C |
| JACKSON ROAD (SR 16) \& GRANT LINE ROAD | Signalized | AM | 68.1 | E | 69.7 | E |
|  |  | PM | >80.0 | F | >80.0 | F |
| Source: Appendix E, Table 6. |  |  |  |  |  |  |

Vehicle Miles Traveled
The TIS analyzed the extent of the Vehicle Miles Travelled (VMT)-related transportation impacts caused by the Project. The Governor's Office of Planning and Research (OPR) recommends that VMT thresholds for residential and employment-based land use projects be set at fifteen percent below the baseline VMT/capita or VMT/employee. The Project is not located in a Transit Priority Area and, subject to Amador County approval, would not otherwise be screened out from VMT analysis because of its location in a relatively high VMT generating area.

For this analysis, the California Statewide Travel Demand Model (CSTDM) was used. The model calculates VMT based on the number of vehicles multiplied by the typical distance traveled by each vehicle originating from or driving to a certain area. The volume of traffic and distance traveled depends on mix of land use types, density, and location as well as the existing and planned transportation system, including availability of public transportation. The model divides areas within the County into transportation analysis zones, or TAZs, which are used for transportation analysis and other planning purposes. The conclusions would be expected to be the same using the Amador County Transportation

Commission's Travel Demand Model due to the project's location on SR 49 directly adjacent to the city limits of one of Amador County's five unincorporated Cities.

Based on the CSTDM Travel Demand Model the County's average VMT per employee is estimated to be 17.9 miles. The employees of the Project would be expected to have similar VMT to existing employees within the TAZ where the project is located, and in other surrounding TAZ's with similar land uses. the Project is forecast to have an average Near-Term Plus Project VMT per employee of 13.2 miles. Thus, Data from the CSTDM model indicates that the project would not have a significant impact on VMT in the County.

## Transit Impacts

The Project would not result in degradation of the level of service (or a significant increase in delay) on any roadway segments currently being utilized by bus transit in the area and, as such, no significant impacts to bus transit are expected. The Project is not expected to significantly impact the operating capacity any existing Amador Transit bus routes. The Project could potentially help support existing bus services with additional transit ridership and would not conflict with any transit plans or goals of the County or Amador Transit. Although the Project does have the potential to increase patronage on bus lines in the area, no significant effects on transit capacity are anticipated given that the additional ridership would be added primarily in the non-peak directions. As a result, the Project would not be expected to result in any significant impacts to bus transit service in the area.

## Pedestrians, Bicycles and Non-Motorized Vehicular Travel

The County does not have level of service standards for pedestrian or bicycle facilities. Nevertheless, use of existing facilities by the users of the Project would not be expected to overcrowd those facilities or decrease their performance or safety. The project will add some pedestrians and bicyclists in the area but the volumes added would not be expected to significantly impact any existing facilities. In relation to the existing conditions, the Project would not cause substantial changes to the pedestrian or bicycle traffic in the area and would not significantly impact or require changes to the design of any existing bicycle or pedestrian facilities.

For the reasons described above, conflicts with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the off-reservation circulation system would be less than significant.

## Question B

## Heavy Equipment

Approximately 15 truck trips per day are estimated throughout the demolition and construction of the Project. Heavy equipment transport to and from the site could cause traffic impacts in the vicinity of the project site during construction. The Project would implement a Traffic Control Plan.

The requirements within the Traffic Control Plan include, but are not limited to, the following: truck drivers would be notified of and required to use the most direct routes; all site ingress and egress would occur only at the main driveways to the project site and construction activities may require installation of
temporary traffic signals; specifically designated travel routes for large vehicles would be monitored and controlled by flaggers for large construction vehicle ingress and egress; warning signs indicating frequent truck entry and exit would be posted on SR 49; and any debris and mud on nearby streets caused by trucks would be monitored daily and may require instituting a street cleaning program. In addition, the ten loads of heavy equipment being hauled to and from the site each month would be short-term and temporary.

## Employees

The weekday work is expected to begin around 7:00 a.m. and end around 4:00 p.m. The construction worker arrival peak would occur between 6:30 a.m. and 7:30 a.m., and the departure peak would occur between 4:00 p.m. and 5:00 p.m. These peak hours are slightly before the countywide commute peaks. It should be noted that the number of trips generated during construction would not only be temporary, but would also be substantially less than the Reduced Project at buildout. Based on estimates of the number of construction workers, the project could require parking for up to 300 vehicles during the peak construction period. Additionally, deliveries, visits, and other activities may generate peak non-worker parking demand of 40 to 50 trucks and automobiles per day. Therefore, up to 350 vehicle parking spaces may be required during the peak construction period for the construction employees. Because the construction of the project can be staged so that employee parking demand is met by using on-site parking, the impacts of construction-related employee traffic and parking are considered less than significant.

## Construction Material Import/Export

The Project would also require removal of existing debris as well as the importation of construction material, including raw materials for the building pads, the buildings, the parking area, and landscaping. During the maximum peak construction period, it is estimated material import and export could generate approximately 150 truck trips per day.

## Traffic Control Plan

The Traffic Control Plan listed in Mitigation Measure 3.17-B would indicate how parking for construction workers would be provided during construction on adjacent land currently held in trust by the Tribe to ensure a safe flow of traffic in the project area during construction. This analysis assumed construction of the entire project in one phase to identify the potential worst-case traffic effects. If the project is built in phases over time, the effects of each phase will be the same or less. Therefore, the demolition and construction activities associated with the Reduced Project or its individual phases would not lead to noticeable congestion in the vicinity of the site or the perception of decreased traffic safety resulting in a less than significant impact with the implementation of the Traffic Control Plan.

## Question C

The TIS did not identify any on-site circulation issues that would cause a traffic safety problem or any unusual traffic congestion or delay. However, current Project Site access via the northern intersection of SR 49 with Village Drive could potentially result in safety impacts due to potential conflicts in the two-way left turn lane with left turns into Randolph Drive. This is an existing safety issue due to the off-set of the two approaches but it currently operates acceptably because of the low volume of left turns into the two side streets. With the higher left turn volumes from the Project, this configuration could have increased
left turn conflicts in the center two-way left-turn with an increased potential for head-on collisions. Mitigation Measure 3.17-E would reduce impacts to less than significant levels.

## Question D

Sufficient emergency access is determined by factors such as number of access points, roadway width, and proximity to fire stations. Project Site access would be via the main entrance on SR 49 and will include a secondary emergency vehicle access. All lane widths within the Project Site would meet the minimum width that can accommodate an emergency vehicle; therefore, the width of the internal roadways would be adequate. In addition, with the proposed mitigation measures, the addition of Project traffic would not result in any significant changes to emergency vehicle response times in the area. Therefore, the Project is expected to have a less than significant impact regarding emergency vehicle access for off-reservation responders.

## Mitigation Measures

## Access

A. The Tribe shall require at least three Tribal security personnel to be educated in traffic control procedures. These security personnel will perform traffic control at the access roads during special events at the event center to make sure that when fire/emergency vehicles need to leave the site, traffic control is provided at the exit of the service entrance to allow smooth movement of emergency vehicles.

## Construction

B. A Traffic Management Plan (TMP) shall be prepared to identify which lanes require closure, where night construction is proposed, and other standards set forth in the Manual on Uniform Traffic Control Devices for Streets and Highways (US DOT FHWA, 2003). The TMP shall be submitted to each affected local jurisdiction and/or agency.
C. Prior to the finalization of construction plans, the Tribe shall notify potentially affected parties in the immediate vicinity of the project site. Notification shall include a construction schedule, locations of construction activities, duration of construction period, and alternative access provisions.
D. Also prior to the finalization of construction plans, the Tribe shall consult with emergency service providers to avoid restricting emergency response service. Police, fire, ambulance, and other emergency response providers shall be notified in advance of the construction schedule, locations of construction activities, duration of construction period, and any access restrictions that could impact emergency response services. Traffic Management Plans shall include details regarding emergency service coordination. Copies of the TMPs shall be provided to affected emergency service providers.

## Operation

E. SR 49 at Village Drive (the Project Site entrance) - Relocate Project access to one of two other recommended locations:

1. Line up the Project entrance with Randolph Street.
2. Design the Project access to connect only to the other (southern) intersection of Village Drive with SR 49.

| 3.18 UTILITIES AND SERVICE SYSTEMS Would the project: | POTENTIALLY SIGNIFICANT IMPACT | LESS THAN SIGNIFICANT WITH MITIGATION INCORPORATION | LESS THAN SIGNIFICANT IMPACT | $\begin{gathered} \text { NO } \\ \text { IMPACT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| a) Exceed off-reservation wastewater treatment requirements of the applicable Regional Water Quality Control Board? | $\square$ | $\square$ | $\square$ | $\square$ |
| b) Require or result in the construction of new water or wastewater treatment facilities or expansion of existing facilities, the construction of which could cause significant off-reservation environmental effects? | $\square$ | $\nabla$ | $\square$ | $\square$ |
| c) Require or result in the construction of new storm water drainage facilities or expansion of existing facilities, the construction of which could cause significant off-reservation environmental effects? | $\square$ | $\nabla$ | $\square$ | $\square$ |
| d) Result in a determination by an off-reservation wastewater treatment provider (if applicable), which serves or may serve the project that it has inadequate capacity to serve the project's projected demand in addition to the provider's existing commitments? | $\square$ | $\square$ | $\square$ | $\square$ |

## Question A

As described in Section 2.1, all Reduced Project wastewater would be treated on-reservation. There would be no impact.

## Question B

As described in Section 2.1, all water and wastewater would be treated on-reservation. Consequently, the Reduced Project would not stimulate the construction of new water or wastewater facilities offreservation. The construction process of the on-reservation water and wastewater facilities is described in Section 2.1, and are an integral part of the Reduced Project. The construction process would not cause off-reservation environmental effects, other than those already described in this document, including those listed in Sections 3.4, 3.8, 3.17 and 3.19. Impacts would be less than significant, with the implementation of mitigation measures.

## Question C

As described in Section 3.10, the Reduced Project would not require or result in the construction of new off-reservation stormwater drainage facilities or expansion of existing facilities, the construction of which could cause significant off-reservation environmental effects. The construction process of the onreservation stormwater drainage facilities is described in Section 2.1, and are an integral part of the Reduced Project. The construction process would not cause off-reservation environmental effects, other
than those already described in this document, including those listed in Sections 3.4, 3.8, 3.17 and 3.19. Impacts would be less than significant, with the implementation of mitigation measures.

## Question D

As described in Section 2.1, all Reduced Project wastewater would be treated on-reservation. There would be no impact.

## Mitigation Measures

None.

| 3.19 CUMULATIVE EFFECTS | POTENTIALLY <br> SIGNIFICANT <br> IMPACT | LESS THAN <br> SIGNIFICANT WITH <br> MITIGATION <br> INCORPORATION | LESS THAN <br> SIGNIFICANT <br> IMPACT | NO <br> IMPACT |
| :--- | :---: | :---: | :---: | :---: |
| a) Have impacts that are individually limited, but |  |  |  |  |
| cumulatively considerable off-reservation? <br> "Cumulatively considerable" means that the <br> incremental effects of a project are considerable <br> when viewed in connection with the effects of past, <br> current, or probable future projects. | $\square$ | $\square$ | $\square$ | $\square$ |

## Question A

## Transportation / Traffic

TABLE 16: FRIDAY EVENING CUMULATIVE PLUS PROJECT INTERSECTION LOS CONDITIONS

| INTERSECTION |  | CONTROL | CUMULATIVE |  | CUMULATIVE PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay | LOS | Delay | LOS |
| 1 | GOLDEN CHAIN HWY (SR 49) \& MILLER WAY |  | Side Street Stop | 9.9 | A | 10.1 | B |
| 2 | GOLDEN CHAIN HWY (SR 49) \& MAIN STREET | Roundabout | 7.2 | A | 7.6 | A |
| 3 | GOLDEN CHAIN HWY (SR 49) \& POPLAR STREET | Side Street Stop | 12.3 | B | 12.7 | B |
| 4 | GOLDEN CHAIN HWY (SR 49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | 15.9 | C | 16.9 | C |
| 5 | GOLDEN CHAIN HWY (SR 49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | 23.4 | C | 26.1 | D |
| 6 | GOLDEN CHAIN HIGHWAY (SR 49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street <br> Stop | 39.4 | E | > 50.0 | F |
| 7 | $\begin{aligned} & \text { GOLDEN CHAIN HIGHWAY (SR 49) \& SR } \\ & 16 \end{aligned}$ | Signalized | 23.5 | C | 25.6 | C |
| 8 | SR 16 \& PLYMOUTH HIGHWAY (SR 124) | Side Street Stop | 19.5 | C | 23.6 | C |
| 9 | SR 16 \& LATROBE ROAD | Side Street Stop | > 50.0 | F | > 50.0 | F |
| 10 | JACKSON ROAD (SR 16) \& IONE ROAD | Side Street Stop | 23.6 | C | 27.2 | D |
| 11 | JACKSON ROAD (SR 16) \& GRANT LINE ROAD | Signalized | 24.7 | C | 25.7 | C |

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## Cumulative Plus Project Traffic Capacity

Friday evening cumulative and cumulative plus Project conditions are presented in Table 16. As described in the TIS (Appendix E), Friday evening traffic flows represent the worst-case scenario. As shown in the table, all of the project study intersections would continue to have acceptable operations (LOS D or better) under cumulative plus project conditions during the Friday PM peak hours, except for the intersection of SR 16 with Latrobe Road and also the intersection of SR 49 with Village Drive (the Proposed entrance). Cumulative impacts would be reduced to less than significant levels, with implementation of the Mitigation Measures listed below.

## Vehicle Miles Traveled

The Project was not found to have a significant impact on VMT in the near-term scenario (Appendix E). Therefore, the Reduced Project's cumulative VMT impacts would be less than significant.

## Transit, Pedestrians, Bicycles and Non-Motorized Vehicular Travel

As described in the TIS (Appendix E, cumulative effects to transit, pedestrians, bicycles and non-motorized vehicular travel would be less than significant.

## Mitigation Measures

A. State Route 16 at Latrobe Road - Payment of a proportionate share of the cost to install a traffic signal, meeting the County's requirements. Using Caltrans' methodology and the volume forecasts in the TIS, the estimated proportional share contribution from the Project for this improvement would be 55\%.
B. SR 49 at Village Drive (the Project Site entrance) - Payment of a proportionate share of the cost to widen Village Drive to allow for separate right and left turn lanes on the westbound approach to SR 49 (i.e., two lanes for traffic exiting the Project Site at SR 49). With this improvement the intersection would meet the established standards. Using Caltrans' methodology and the volume forecasts in the TIS, the estimated proportional share contribution from the Project for this improvement would be 81\%.

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## APPENDIX A

Air Quality Modeling Output Files and Calculations

## Project in Amador County Custom Report

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## 1. Basic Project Information

### 1.1. Basic Project Information

| Data Field | Value |
| :---: | :---: |
| Project Name | Project in Amador County |
| Construction Start Date | 1/1/2024 |
| Operational Year | 2025 |
| Lead Agency | - |
| Land Use Scale | Project/site |
| Analysis Level for Defaults | County |
| Windspeed (m/s) | 2.70 |
| Precipitation (days) | 21.2 |
| Location | 38.46570305052646, -120.85329250452098 |
| County | Amador |
| City | Unincorporated |
| Air District | Amador County APCD |
| Air Basin | Mountain Counties |
| TAZ | 3003 |
| EDFZ | 4 |
| Electric Utility | Pacific Gas \& Electric Company |
| Gas Utility | Pacific Gas \& Electric |
| App Version | 2022.1.1.20 |

### 1.2. Land Use Types

| Land Use Subtype | Size | Unit | Lot Acreage | Building Area (sq ft) | Landscape Area (sq ft) | Special Landscape <br> Area (sq ft) | Population | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| User Defined Recreational | 25.2 | User Defined Unit | 7.16 | 25,205 | 87,120 | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High Turnover (Sit Down Restaurant) | 4.03 | 1000sqft | 0.00 | 4,034 | 0.00 | - | - | - |
| Fast Food <br> Restaurant w/o Drive Thru | 4.46 | 1000sqft | 0.00 | 4,457 | 0.00 | - | - | - |
| User Defined Commercial | 17.6 | User Defined Unit | 0.00 | 17,614 | 0.00 | - | - | - |
| Parking Lot | 672 | Space | 6.05 | 0.00 | - | - | - | - |

### 1.3. User-Selected Emission Reduction Measures by Emissions Sector

| Sector | $\#$ |  | Measure Title |
| :--- | :--- | :--- | :--- |
| Construction | C-2* | Limit Heavy-Duty Diesel Vehicle Idling |  |
| Water | W-1 | Use Reclaimed Non-Potable Water |  |

* Qualitative or supporting measure. Emission reductions not included in the mitigated emissions results.


## 2. Emissions Summary

### 2.1. Construction Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Un/Mit. | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 1.63 | 68.8 | 11.9 | 15.5 | 0.03 | 0.50 | 0.26 | 0.76 | 0.46 | 0.06 | 0.53 | - | 2,881 | 2,881 | 0.11 | 0.07 | 1.64 | 2,906 |
| Mit. | 1.63 | 68.8 | 11.9 | 15.5 | 0.03 | 0.50 | 0.26 | 0.76 | 0.46 | 0.06 | 0.53 | - | 2,881 | 2,881 | 0.11 | 0.07 | 1.64 | 2,906 |
| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unmit. | 5.19 | 4.35 | 90.0 | 36.1 | 0.33 | 1.85 | 19.8 | 21.4 | 1.74 | 10.1 | 11.6 | - | 31,840 | 31,840 | 0.29 | 3.97 | 1.07 | 33,032 |
| Mit. | 5.19 | 4.35 | 90.0 | 36.1 | 0.33 | 1.85 | 19.8 | 21.4 | 1.74 | 10.1 | 11.6 | - | 31,840 | 31,840 | 0.29 | 3.97 | 1.07 | 33,032 |
| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Average Daily <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 1.61 | 4.22 | 16.4 | 13.4 | 0.04 | 0.53 | 2.00 | 2.53 | 0.49 | 0.76 | 1.25 | - | 4,586 | 4,586 | 0.10 | 0.38 | 1.92 | 4,704 |
| Mit. | 1.61 | 4.22 | 16.4 | 13.4 | 0.04 | 0.53 | 2.00 | 2.53 | 0.49 | 0.76 | 1.25 | - | 4,586 | 4,586 | 0.10 | 0.38 | 1.92 | 4,704 |
| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 0.29 | 0.77 | 2.98 | 2.44 | 0.01 | 0.10 | 0.37 | 0.46 | 0.09 | 0.14 | 0.23 | - | 759 | 759 | 0.02 | 0.06 | 0.32 | 779 |
| Mit. | 0.29 | 0.77 | 2.98 | 2.44 | 0.01 | 0.10 | 0.37 | 0.46 | 0.09 | 0.14 | 0.23 | - | 759 | 759 | 0.02 | 0.06 | 0.32 | 779 |
| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

### 2.2. Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Year | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 1.63 | 1.38 | 11.9 | 15.5 | 0.03 | 0.50 | 0.26 | 0.76 | 0.46 | 0.06 | 0.53 | - | 2,881 | 2,881 | 0.11 | 0.07 | 1.64 | 2,906 |
| 2025 | 1.53 | 68.8 | 11.1 | 15.3 | 0.03 | 0.44 | 0.26 | 0.70 | 0.40 | 0.06 | 0.46 | - | 2,874 | 2,874 | 0.11 | 0.07 | 1.59 | 2,898 |
| Daily - <br> Winter <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| 2024 | 5.19 | 4.35 | 90.0 | 36.1 | 0.33 | 1.85 | 19.8 | 21.4 | 1.74 | 10.1 | 11.6 | - | 31,840 | 31,840 | 0.29 | 3.97 | 1.07 | 33,032 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2025 | 1.51 | 1.27 | 11.1 | 14.7 | 0.03 | 0.44 | 0.26 | 0.70 | 0.40 | 0.06 | 0.46 | - | 2,850 | 2,850 | 0.11 | 0.07 | 0.04 | 2,874 |
| Average Daily | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 1.61 | 1.36 | 16.4 | 13.4 | 0.04 | 0.53 | 2.00 | 2.53 | 0.49 | 0.76 | 1.25 | - | 4,586 | 4,586 | 0.10 | 0.38 | 1.92 | 4,704 |
| 2025 | 0.49 | 4.22 | 3.55 | 4.81 | 0.01 | 0.14 | 0.08 | 0.22 | 0.13 | 0.02 | 0.15 | - | 894 | 894 | 0.03 | 0.02 | 0.21 | 901 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 0.29 | 0.25 | 2.98 | 2.44 | 0.01 | 0.10 | 0.37 | 0.46 | 0.09 | 0.14 | 0.23 | - | 759 | 759 | 0.02 | 0.06 | 0.32 | 779 |
| 2025 | 0.09 | 0.77 | 0.65 | 0.88 | < 0.005 | 0.03 | 0.01 | 0.04 | 0.02 | $<0.005$ | 0.03 | - | 148 | 148 | 0.01 | < 0.005 | 0.04 | 149 |

### 2.3. Construction Emissions by Year, Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Year | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 1.63 | 1.38 | 11.9 | 15.5 | 0.03 | 0.50 | 0.26 | 0.76 | 0.46 | 0.06 | 0.53 | - | 2,881 | 2,881 | 0.11 | 0.07 | 1.64 | 2,906 |
| 2025 | 1.53 | 68.8 | 11.1 | 15.3 | 0.03 | 0.44 | 0.26 | 0.70 | 0.40 | 0.06 | 0.46 | - | 2,874 | 2,874 | 0.11 | 0.07 | 1.59 | 2,898 |
| Daily Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 5.19 | 4.35 | 90.0 | 36.1 | 0.33 | 1.85 | 19.8 | 21.4 | 1.74 | 10.1 | 11.6 | - | 31,840 | 31,840 | 0.29 | 3.97 | 1.07 | 33,032 |
| 2025 | 1.51 | 1.27 | 11.1 | 14.7 | 0.03 | 0.44 | 0.26 | 0.70 | 0.40 | 0.06 | 0.46 | - | 2,850 | 2,850 | 0.11 | 0.07 | 0.04 | 2,874 |
| Average Daily | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 1.61 | 1.36 | 16.4 | 13.4 | 0.04 | 0.53 | 2.00 | 2.53 | 0.49 | 0.76 | 1.25 | - | 4,586 | 4,586 | 0.10 | 0.38 | 1.92 | 4,704 |
| 2025 | 0.49 | 4.22 | 3.55 | 4.81 | 0.01 | 0.14 | 0.08 | 0.22 | 0.13 | 0.02 | 0.15 | - | 894 | 894 | 0.03 | 0.02 | 0.21 | 901 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2024 | 0.29 | 0.25 | 2.98 | 2.44 | 0.01 | 0.10 | 0.37 | 0.46 | 0.09 | 0.14 | 0.23 | - | 759 | 759 | 0.02 | 0.06 | 0.32 | 779 |


| 2025 | 0.09 | 0.77 | 0.65 | 0.88 | < 0.005 | 0.03 | 0.01 | 0.04 | 0.02 | < 0.005 | 0.03 | - | 148 | 148 | 0.01 | < 0.005 | 0.04 |  | 149 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 2.4. Operations Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Un/Mit. | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 24.3 | 24.2 | 24.4 | 154 | 0.23 | 0.42 | 17.7 | 18.1 | 0.40 | 4.52 | 4.92 | 114 | 25,035 | 25,149 | 46.1 | 1.49 | 114 | 26,859 |
| Mit. | 24.3 | 24.2 | 24.4 | 154 | 0.23 | 0.42 | 17.7 | 18.1 | 0.40 | 4.52 | 4.92 | 114 | 25,035 | 25,149 | 46.1 | 1.49 | 114 | 26,859 |
| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 20.8 | 20.7 | 27.5 | 132 | 0.22 | 0.41 | 17.7 | 18.1 | 0.39 | 4.52 | 4.92 | 114 | 23,391 | 23,504 | 46.3 | 1.61 | 15.9 | 25,155 |
| Mit. | 20.8 | 20.7 | 27.5 | 132 | 0.22 | 0.41 | 17.7 | 18.1 | 0.39 | 4.52 | 4.92 | 114 | 23,391 | 23,504 | 46.3 | 1.61 | 15.9 | 25,155 |
| \% Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Average <br> Daily <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 21.3 | 21.2 | 26.6 | 133 | 0.22 | 0.41 | 17.5 | 17.9 | 0.40 | 4.46 | 4.86 | 114 | 23,769 | 23,883 | 46.2 | 1.56 | 56.6 | 25,560 |
| Mit. | 21.3 | 21.2 | 26.6 | 133 | 0.22 | 0.41 | 17.5 | 17.9 | 0.40 | 4.46 | 4.86 | 114 | 23,769 | 23,883 | 46.2 | 1.56 | 56.6 | 25,560 |
| \% Reduced | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 3.89 | 3.87 | 4.85 | 24.3 | 0.04 | 0.08 | 3.19 | 3.27 | 0.07 | 0.81 | 0.89 | 18.8 | 3,935 | 3,954 | 7.65 | 0.26 | 9.38 | 4,232 |
| Mit. | 3.89 | 3.87 | 4.85 | 24.3 | 0.04 | 0.08 | 3.19 | 3.27 | 0.07 | 0.81 | 0.89 | 18.8 | 3,935 | 3,954 | 7.65 | 0.26 | 9.38 | 4,232 |


| \% <br> Reduced | - | - | - | - | - | - | - | - | - | - | - | - | < 0.5\% | < 0.5\% | - | - | - | < $0.5 \%$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 2.5. Operations Emissions by Sector, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Sector | TOG | Rog | Nox | co | SO2 | PM10E | PM10D | Рм10т | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | СН4 | N2O | R | coze |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 23.9 | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |
| Area | 0.40 | 1.86 | 0.02 | 2.23 | <0.005 | <0.005 | - | < 0.005 | <0.005 | - | < 0.005 | - | 9.18 | 9.18 | <0.005 | < 0.005 | - | 9.21 |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | <0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |
| Total | 24.3 | 24.2 | 24.4 | 154 | 0.23 | 0.42 | 17.7 | 18.1 | 0.40 | 4.52 | 4.92 | 114 | 25,035 | 25,149 | 46.1 | 1.49 | 114 | 26,859 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 20.7 | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| Area | - | 1.49 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | <0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio <br> n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |
| Total | 20.8 | 20.7 | 27.5 | 132 | 0.22 | 0.41 | 17.7 | 18.1 | 0.39 | 4.52 | 4.92 | 114 | 23,391 | 23,504 | 46.3 | 1.61 | 15.9 | 25,155 |


| Average Daily | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mobile | 21.0 | 19.5 | 25.9 | 132 | 0.22 | 0.36 | 17.5 | 17.8 | 0.35 | 4.46 | 4.81 | - | 22,129 | 22,129 | 1.34 | 1.47 | 43.4 | 22,644 |
| Area | 0.20 | 1.68 | 0.01 | 1.10 | $<0.005$ | $<0.005$ | - | $<0.005$ | < 0.005 | - | $<0.005$ | - | 4.53 | 4.53 | $<0.005$ | < 0.005 | - | 4.54 |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | $<0.005$ | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |
| Total | 21.3 | 21.2 | 26.6 | 133 | 0.22 | 0.41 | 17.5 | 17.9 | 0.40 | 4.46 | 4.86 | 114 | 23,769 | 23,883 | 46.2 | 1.56 | 56.6 | 25,560 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 3.84 | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |
| Area | 0.04 | 0.31 | $<0.005$ | 0.20 | $<0.005$ | < 0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 0.75 | 0.75 | < 0.005 | < 0.005 | - | 0.75 |
| Energy | 0.01 | 0.01 | 0.11 | 0.10 | $<0.005$ | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 221 | 221 | 0.03 | < 0.005 | - | 222 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 12.9 | 0.00 | 12.9 | 1.29 | 0.00 | - | 45.0 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 2.20 | 2.20 |
| Vegetatio n | - | - | - | - | - | - | - | - | - | - | - | - | 44.1 | 44.1 | - | - | - | 44.1 |
| Total | 3.89 | 3.87 | 4.85 | 24.3 | 0.04 | 0.08 | 3.19 | 3.27 | 0.07 | 0.81 | 0.89 | 18.8 | 3,935 | 3,954 | 7.65 | 0.26 | 9.38 | 4,232 |

### 2.6. Operations Emissions by Sector, Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Sector | TOG | ROG | NOx | cO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 23.9 | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |


| Area | 0.40 | 1.86 | 0.02 | 2.23 | < 0.005 | < 0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 9.18 | 9.18 | < 0.005 | <0.005 | - | 9.21 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio <br> n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |
| Total | 24.3 | 24.2 | 24.4 | 154 | 0.23 | 0.42 | 17.7 | 18.1 | 0.40 | 4.52 | 4.92 | 114 | 25,035 | 25,149 | 46.1 | 1.49 | 114 | 26,859 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 20.7 | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| Area | - | 1.49 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio <br> n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |
| Total | 20.8 | 20.7 | 27.5 | 132 | 0.22 | 0.41 | 17.7 | 18.1 | 0.39 | 4.52 | 4.92 | 114 | 23,391 | 23,504 | 46.3 | 1.61 | 15.9 | 25,155 |
| Average Daily | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 21.0 | 19.5 | 25.9 | 132 | 0.22 | 0.36 | 17.5 | 17.8 | 0.35 | 4.46 | 4.81 | - | 22,129 | 22,129 | 1.34 | 1.47 | 43.4 | 22,644 |
| Area | 0.20 | 1.68 | 0.01 | 1.10 | < 0.005 | < 0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 4.53 | 4.53 | < 0.005 | <0.005 | - | 4.54 |
| Energy | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 1,336 | 1,336 | 0.16 | 0.01 | - | 1,344 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Vegetatio n | - | - | - | - | - | - | - | - | - | - | - | - | 266 | 266 | - | - | - | 266 |


| Total | 21.3 | 21.2 | 26.6 | 133 | 0.22 | 0.41 | 17.5 | 17.9 | 0.40 | 4.46 | 4.86 | 114 | 23,769 | 23,883 | 46.2 | 1.56 | 56.6 | 25,560 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 3.84 | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |
| Area | 0.04 | 0.31 | < 0.005 | 0.20 | < 0.005 | $<0.005$ | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 0.75 | 0.75 | < 0.005 | < 0.005 | - | 0.75 |
| Energy | 0.01 | 0.01 | 0.11 | 0.10 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 221 | 221 | 0.03 | < 0.005 | - | 222 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 12.9 | 0.00 | 12.9 | 1.29 | 0.00 | - | 45.0 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 2.20 | 2.20 |
| Vegetatio <br> n | - | - | - | - | - | - | - | - | - | - | - | - | 44.1 | 44.1 | - | - | - | 44.1 |
| Total | 3.89 | 3.87 | 4.85 | 24.3 | 0.04 | 0.08 | 3.19 | 3.27 | 0.07 | 0.81 | 0.89 | 18.8 | 3,935 | 3,954 | 7.65 | 0.26 | 9.38 | 4,232 |

## 4. Operations Emissions Details

### 4.1. Mobile Emissions by Land Use

### 4.1.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation | $\begin{aligned} & 23.9 \\ & \text { nal } \end{aligned}$ | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |
| High <br> Turnover (Sit Down Restaurart) | 0.00 t) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |


| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commerc | 0.00 al | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 23.9 | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation | 20.7 <br> nal | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| High <br> Turnover <br> (Sit Down <br> Restaurar | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Fast <br> Food <br> Restaurar <br> w/o Drive Thru | $0.00$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| User Defined Commerc | $0.00$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 20.7 | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation | $3.84$ <br> nal | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |


| High <br> Turnover <br> (Sit Down <br> Restaurar | 0.00 t) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 3.84 | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |

### 4.1.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreatio | $\begin{aligned} & 23.9 \\ & \text { nal } \end{aligned}$ | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |
| High Turnover (Sit Down Restaurar | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |


| User Defined Commerc | $0.00$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 23.9 | 22.4 | 23.8 | 151 | 0.23 | 0.36 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 23,390 | 23,390 | 1.26 | 1.40 | 100 | 23,939 |
| Daily, Winter <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined Recreation | 20.7 <br> nal | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| High <br> Turnover (Sit Down Restaurar | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Fast <br> Food Restaurar w/o Drive Thru | $0.00$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking <br> Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 20.7 | 19.1 | 26.9 | 131 | 0.21 | 0.37 | 17.7 | 18.1 | 0.35 | 4.52 | 4.87 | - | 21,754 | 21,754 | 1.42 | 1.51 | 2.60 | 22,244 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined Recreation | $3.84$ <br> nal | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |
| High <br> Turnover (Sit Down Restaurar | $0.00$ <br> t) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |


| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commerc | 0.00 al | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 3.84 | 3.56 | 4.74 | 24.0 | 0.04 | 0.07 | 3.19 | 3.26 | 0.06 | 0.81 | 0.88 | - | 3,664 | 3,664 | 0.22 | 0.24 | 7.18 | 3,749 |

### 4.2. Energy

### 4.2.1. Electricity Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation |  | - | - | - | - | - | - | - | - | - | - | - | 273 | 273 | 0.04 | 0.01 | - | 276 |
| High <br> Turnover <br> (Sit Down <br> Restaurart |  | - | - | - | - | - | - | - | - | - | - | - | 90.5 | 90.5 | 0.01 | < 0.005 | - | 91.4 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | - | 100 | 100 | 0.02 | < 0.005 | - | 101 |


| User Defined Commercal | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parking - Lot | - | - | - | - | - | - | - | - | - | - | - | 129 | 129 | 0.02 | $<0.005$ | - | 130 |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 592 | 592 | 0.10 | 0.01 | - | 598 |
| Daily, - <br> Winter  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $\begin{aligned} & \text { User } \quad- \\ & \text { Defined } \\ & \text { Recreational } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | 273 | 273 | 0.04 | 0.01 | - | 276 |
| $\begin{aligned} & \text { High } \\ & \text { Turnover } \\ & \text { (Sit Down } \\ & \text { Restaurart) } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | 90.5 | 90.5 | 0.01 | $<0.005$ | - | 91.4 |
| Fast <br> Food <br> Restaurart w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | - | 100 | 100 | 0.02 | $<0.005$ | - | 101 |
| User Defined Commercial | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | 129 | 129 | 0.02 | $<0.005$ | - | 130 |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 592 | 592 | 0.10 | 0.01 | - | 598 |
| Annual - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreational | - | - | - | - | - | - | - | - | - | - | - | 45.2 | 45.2 | 0.01 | $<0.005$ | - | 45.6 |
| High Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | 15.0 | 15.0 | $<0.005$ | $<0.005$ | - | 15.1 |


| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | - | 16.6 | 16.6 | < 0.005 | $<0.005$ | - | 16.7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | - | 21.4 | 21.4 | < 0.005 | $<0.005$ | - | 21.6 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 98.1 | 98.1 | 0.02 | $<0.005$ | - | 99.0 |

### 4.2.2. Electricity Emissions By Land Use - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land TOG <br> Use  | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{l\|l} \hline \text { Daily, } & \text { - } \\ \text { Summer } & \\ \text { (Max) } \end{array}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
|  | - | - | - | - | - | - | - | - | - | - | - | 273 | 273 | 0.04 | 0.01 | - | 276 |
| High Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | 90.5 | 90.5 | 0.01 | $<0.005$ | - | 91.4 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | - | - | - | - | - | - | - | - | - | - | - | 100 | 100 | 0.02 | < 0.005 | - | 101 |
| User $\quad-$ Defined Commercial | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |


| Parking - Lot | - | - | - | - | - | - | - | - | - | - | - | 129 | 129 | 0.02 | $<0.005$ | - | 130 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 592 | 592 | 0.10 | 0.01 | - | 598 |
| Daily, <br> Winter <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User - <br> Defined <br> Recreational | - | - | - | - | - | - | - | - | - | - | - | 273 | 273 | 0.04 | 0.01 | - | 276 |
| High <br> Turnover <br> (Sit Down <br> Restaurart) | - | - | - | - | - | - | - | - | - | - | - | 90.5 | 90.5 | 0.01 | $<0.005$ | - | 91.4 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | - | 100 | 100 | 0.02 | $<0.005$ | - | 101 |
| User $\qquad$ Defined Commercal | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking - Lot | - | - | - | - | - | - | - | - | - | - | - | 129 | 129 | 0.02 | $<0.005$ | - | 130 |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 592 | 592 | 0.10 | 0.01 | - | 598 |
| Annual - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreational | - | - | - | - | - | - | - | - | - | - | - | 45.2 | 45.2 | 0.01 | $<0.005$ | - | 45.6 |
| High $\qquad$ Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | 15.0 | 15.0 | $<0.005$ | $<0.005$ | - | 15.1 |


| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | - | 16.6 | 16.6 | < 0.005 | $<0.005$ | - | 16.7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | - | 21.4 | 21.4 | < 0.005 | $<0.005$ | - | 21.6 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 98.1 | 98.1 | 0.02 | $<0.005$ | - | 99.0 |

### 4.2.3. Natural Gas Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, - <br> Summer  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User $\quad 0.04$ Defined Recreational | 0.02 | 0.35 | 0.29 | < 0.005 | 0.03 | - | 0.03 | 0.03 | - | 0.03 | - | 412 | 412 | 0.04 | < 0.005 | - | 413 |
| High 0.01 Turnover (Sit Down Restaurart) | 0.01 | 0.13 | 0.11 | $<0.005$ | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 158 | 158 | 0.01 | $<0.005$ | - | 158 |
| Fast 0.02 <br> Food  <br> Restaurart  <br> w/o Drive  <br> Thru  <br>   | 0.01 | 0.15 | 0.12 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 174 | 174 | 0.02 | < 0.005 | - | 175 |
| User 0.00 Defined Commercal al | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |


| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 743 | 743 | 0.07 | < 0.005 | - | 745 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation | $0.04$ | 0.02 | 0.35 | 0.29 | < 0.005 | 0.03 | - | 0.03 | 0.03 | - | 0.03 | - | 412 | 412 | 0.04 | < 0.005 | - | 413 |
| High Turnover (Sit Down Restaurart) | 0.01 t) | 0.01 | 0.13 | 0.11 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 158 | 158 | 0.01 | < 0.005 | - | 158 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | $0.02$ | 0.01 | 0.15 | 0.12 | $<0.005$ | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 174 | 174 | 0.02 | $<0.005$ | - | 175 |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 743 | 743 | 0.07 | < 0.005 | - | 745 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined <br> Recreation | $0.01$ | $<0.005$ | 0.06 | 0.05 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 68.2 | 68.2 | 0.01 | $<0.005$ | - | 68.4 |
| High <br> Turnover (Sit Down Restaurart) | $<0.005$ | $<0.005$ | 0.02 | 0.02 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 26.1 | 26.1 | $<0.005$ | $<0.005$ | - | 26.2 |


| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | $<0.005$ | < 0.005 | 0.03 | 0.02 | $<0.005$ | < 0.005 | - | $<0.005$ | <0.005 | - | < 0.005 | - | 28.8 | 28.8 | < 0.005 | $<0.005$ | - | 28.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | 0.01 | 0.01 | 0.11 | 0.10 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 123 | 123 | 0.01 | $<0.005$ | - | 123 |

### 4.2.4. Natural Gas Emissions By Land Use - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, - <br> Summer  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User $\quad 0.04$ Defined Recreational | 0.02 | 0.35 | 0.29 | < 0.005 | 0.03 | - | 0.03 | 0.03 | - | 0.03 | - | 412 | 412 | 0.04 | < 0.005 | - | 413 |
| High 0.01 Turnover (Sit Down Restaurart) | 0.01 | 0.13 | 0.11 | $<0.005$ | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 158 | 158 | 0.01 | $<0.005$ | - | 158 |
| Fast 0.02 <br> Food  <br> Restaurart  <br> w/o Drive  <br> Thru  <br>   | 0.01 | 0.15 | 0.12 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 174 | 174 | 0.02 | < 0.005 | - | 175 |
| User 0.00 Defined Commercal al | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |


| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 743 | 743 | 0.07 | < 0.005 | - | 745 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation | $0.04$ | 0.02 | 0.35 | 0.29 | < 0.005 | 0.03 | - | 0.03 | 0.03 | - | 0.03 | - | 412 | 412 | 0.04 | < 0.005 | - | 413 |
| High Turnover (Sit Down Restaurart) | 0.01 t) | 0.01 | 0.13 | 0.11 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 158 | 158 | 0.01 | < 0.005 | - | 158 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | $0.02$ | 0.01 | 0.15 | 0.12 | $<0.005$ | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 174 | 174 | 0.02 | $<0.005$ | - | 175 |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | 0.07 | 0.03 | 0.62 | 0.52 | < 0.005 | 0.05 | - | 0.05 | 0.05 | - | 0.05 | - | 743 | 743 | 0.07 | < 0.005 | - | 745 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined <br> Recreation | $0.01$ | $<0.005$ | 0.06 | 0.05 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 68.2 | 68.2 | 0.01 | $<0.005$ | - | 68.4 |
| High <br> Turnover (Sit Down Restaurart) | $<0.005$ | $<0.005$ | 0.02 | 0.02 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 26.1 | 26.1 | $<0.005$ | $<0.005$ | - | 26.2 |


| Fast <br> Food <br> Restaurar <br> w/o Drive <br> Thru | $<0.005$ | < 0.005 | 0.03 | 0.02 | $<0.005$ | < 0.005 | - | $<0.005$ | <0.005 | - | < 0.005 | - | 28.8 | 28.8 | < 0.005 | $<0.005$ | - | 28.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Commerc | $\begin{aligned} & 0.00 \\ & \text { al } \end{aligned}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 | 0.00 | - | 0.00 | - | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | 0.01 | 0.01 | 0.11 | 0.10 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 123 | 123 | 0.01 | $<0.005$ | - | 123 |

### 4.3. Area Emissions by Source

### 4.3.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Source | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum er Products | - | 1.12 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.38 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Landsca pe Equipme nt | 0.40 | 0.37 | 0.02 | 2.23 | < 0.005 | < 0.005 | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 9.18 | 9.18 | $<0.005$ | < 0.005 | - | 9.21 |
| Total | 0.40 | 1.86 | 0.02 | 2.23 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 9.18 | 9.18 | $<0.005$ | $<0.005$ | - | 9.21 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Consum Products | - | 1.12 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Architect ural Coatings | - | 0.38 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | 1.49 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum er Products | - | 0.20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.07 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Landsca pe Equipme nt | 0.04 | 0.03 | $<0.005$ | 0.20 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 0.75 | 0.75 | < 0.005 | < 0.005 | - | 0.75 |
| Total | 0.04 | 0.31 | < 0.005 | 0.20 | < 0.005 | < 0.005 | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 0.75 | 0.75 | < 0.005 | <0.005 | - | 0.75 |

### 4.3.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Source | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum <br> er <br> Products | - | 1.12 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.38 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Landsca pe Equipme nt | 0.40 | 0.37 | 0.02 | 2.23 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 9.18 | 9.18 | $<0.005$ | $<0.005$ | - | 9.21 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 0.40 | 1.86 | 0.02 | 2.23 | < 0.005 | < 0.005 | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 9.18 | 9.18 | < 0.005 | < 0.005 | - | 9.21 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum er Products | - | 1.12 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.38 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | 1.49 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum er Products | - | 0.20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.07 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Landsca pe Equipme nt | 0.04 | 0.03 | < 0.005 | 0.20 | < 0.005 | < 0.005 | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 0.75 | 0.75 | $<0.005$ | $<0.005$ | - | 0.75 |
| Total | 0.04 | 0.31 | < 0.005 | 0.20 | < 0.005 | < 0.005 | - | $<0.005$ | $<0.005$ | - | < 0.005 | - | 0.75 | 0.75 | $<0.005$ | < 0.005 | - | 0.75 |

### 4.4. Water Emissions by Land Use

4.4.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (Ib/day for daily, MT/yr for annual)

| Land <br> Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| $\begin{array}{l\|l} \text { Daily, } & \text { - } \\ \text { Summer } & \\ \text { (Max) } \end{array}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User $\quad-$ Defined Recreational | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| High $\qquad$ Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast $\qquad$ <br> Food <br> Restaurart <br> w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| User Defined Commercal | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking - Lot | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Daily, - <br> Winter  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreational | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| High Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast $\qquad$ <br> Food <br> Restaurart w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |

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| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parking <br> Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreationa |  | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |
| High Turnover (Sit Down Restaurart) | - rt) | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |

### 4.4.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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| User Defined Recreational | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { High } \\ & \text { Turnover } \\ & \text { (Sit Down } \\ & \text { Restaurart) } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| User Defined Commercial | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Daily, - <br> Winter  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User $\quad-$ Defined Recreational | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| High <br> Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| $\begin{aligned} & \text { User } \\ & \text { Defined } \\ & \text { Commercial } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |

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| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 35.9 | 34.1 | 70.0 | 36.9 | 0.08 | - | 1,016 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreationa |  | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |
| High Turnover (Sit Down Restaurart) | t) | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| User Defined Commerca |  | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Parking <br> Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 5.94 | 5.65 | 11.6 | 6.11 | 0.01 | - | 168 |

### 4.5. Waste Emissions by Land Use

### 4.5.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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| User <br> Defined <br> Recreational | - | - | - | - | - | - | - | - | - | - | 14.3 | 0.00 | 14.3 | 1.43 | 0.00 | - | 49.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { High } \\ & \text { Turnover } \\ & \text { (Sit Down } \\ & \text { Restaurart) } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | 25.9 | 0.00 | 25.9 | 2.59 | 0.00 | - | 90.5 |
| Fast $\qquad$ <br> Food <br> Restaurart w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | 27.7 | 0.00 | 27.7 | 2.77 | 0.00 | - | 96.8 |
| User Defined Commercial | - | - | - | - | - | - | - | - | - | - | 9.97 | 0.00 | 9.97 | 1.00 | 0.00 | - | 34.9 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Daily, - <br> Winter  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined <br> Recreational | - | - | - | - | - | - | - | - | - | - | 14.3 | 0.00 | 14.3 | 1.43 | 0.00 | - | 49.9 |
| $\begin{aligned} & \text { High } \\ & \text { Turnover } \\ & \text { (Sit Down } \\ & \text { Restaurart) } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | 25.9 | 0.00 | 25.9 | 2.59 | 0.00 | - | 90.5 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | 27.7 | 0.00 | 27.7 | 2.77 | 0.00 | - | 96.8 |
| User Defined Commercial | - | - | - | - | - | - | - | - | - | - | 9.97 | 0.00 | 9.97 | 1.00 | 0.00 | - | 34.9 |

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| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreationa |  | - | - | - | - | - | - | - | - | - | - | 2.36 | 0.00 | 2.36 | 0.24 | 0.00 | - | 8.26 |
| High Turnover (Sit Down Restaurart) | t) | - | - | - | - | - | - | - | - | - | - | 4.28 | 0.00 | 4.28 | 0.43 | 0.00 | - | 15.0 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | 4.58 | 0.00 | 4.58 | 0.46 | 0.00 | - | 16.0 |
| User Defined Commerca |  | - | - | - | - | - | - | - | - | - | - | 1.65 | 0.00 | 1.65 | 0.16 | 0.00 | - | 5.77 |
| Parking <br> Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 12.9 | 0.00 | 12.9 | 1.29 | 0.00 | - | 45.0 |

### 4.5.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User Defined Recreation |  | - | - | - | - | - | - | - | - | - | - | 14.3 | 0.00 | 14.3 | 1.43 | 0.00 | - | 49.9 |

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| High <br> Turnover <br> (Sit <br> Down <br> Restaurart) |  | - | - | - | - | - | - | - | - | - | - | 25.9 | 0.00 | 25.9 | 2.59 | 0.00 | - | 90.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru |  | - | - | - | - | - | - | - | - | - | - | 27.7 | 0.00 | 27.7 | 2.77 | 0.00 | - | 96.8 |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | 9.97 | 0.00 | 9.97 | 1.00 | 0.00 | - | 34.9 |
| Parking <br> Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| User <br> Defined <br> Recreation | $\qquad$ <br> - <br> nal | - | - | - | - | - | - | - | - | - | - | 14.3 | 0.00 | 14.3 | 1.43 | 0.00 | - | 49.9 |
| High <br> Turnover (Sit Down Restaurart |  | - | - | - | - | - | - | - | - | - | - | 25.9 | 0.00 | 25.9 | 2.59 | 0.00 | - | 90.5 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru |  | - | - | - | - | - | - | - | - | - | - | 27.7 | 0.00 | 27.7 | 2.77 | 0.00 | - | 96.8 |
| User <br> Defined <br> Commerca |  | - | - | - | - | - | - | - | - | - | - | 9.97 | 0.00 | 9.97 | 1.00 | 0.00 | - | 34.9 |
| Parking Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 77.8 | 0.00 | 77.8 | 7.77 | 0.00 | - | 272 |

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| Annual - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreationa |  | - | - | - | - | - | - | - | - | - | - | 2.36 | 0.00 | 2.36 | 0.24 | 0.00 | - | 8.26 |
| High <br> Turnover (Sit Down Restaurart) |  | - | - | - | - | - | - | - | - | - | - | 4.28 | 0.00 | 4.28 | 0.43 | 0.00 | - | 15.0 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru |  | - | - | - | - | - | - | - | - | - | - | 4.58 | 0.00 | 4.58 | 0.46 | 0.00 | - | 16.0 |
| User Defined Commercial |  | - | - | - | - | - | - | - | - | - | - | 1.65 | 0.00 | 1.65 | 0.16 | 0.00 | - | 5.77 |
| Parking <br> Lot | - | - | - | - | - | - | - | - | - | - | - | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | 0.00 |
| Total - | - | - | - | - | - | - | - | - | - | - | - | 12.9 | 0.00 | 12.9 | 1.29 | 0.00 | - | 45.0 |

### 4.6. Refrigerant Emissions by Land Use

4.6.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| High <br> Turnover <br> (Sit Down <br> Restaurart) |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.31 | 6.31 |


| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.97 | 6.97 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User $\quad-$ Defined Recreational | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| User $\qquad$ Defined Commercial | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| Total - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Daily, <br> Winter <br> (Max) - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| High $\qquad$ Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.31 | 6.31 |
| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.97 | 6.97 |
| User Defined Recreational | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| User $\qquad$ <br> Defined Commercal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | < 0.005 |
| Total - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Annual - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| High Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 1.04 | 1.04 |


| Fast <br> Food <br> Restaurart <br> w/o Drive <br> Thru |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 1.15 | 1.15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreation |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | < 0.005 | $<0.005$ |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 2.20 | 2.20 |

### 4.6.2. Mitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| High <br> Turnover <br> (Sit Down <br> Restaurart |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.31 | 6.31 |
| Fast <br> Food <br> Restaurart <br> w/o Drive Thru |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.97 | 6.97 |
| User Defined Recreation |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| User Defined Commercia |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |


| Total - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, - <br> Winter  <br> (Max)  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| High $\qquad$ Turnover (Sit Down Restaurart) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.31 | 6.31 |
| Fast $\qquad$ <br> Food <br> Restaurart w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 6.97 | 6.97 |
| $\begin{aligned} & \text { User } \quad- \\ & \text { Defined } \\ & \text { Recreational } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | < 0.005 |
| $\begin{aligned} & \text { User } \\ & \text { Defined } \\ & \text { Commerc al } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| Total - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 13.3 | 13.3 |
| Annual - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $\begin{aligned} & \text { High } \\ & \text { Turnover } \\ & \text { (Sit Down } \\ & \text { Restaurart) } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 1.04 | 1.04 |
| Fast <br> Food <br> Restaurart w/o Drive Thru | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 1.15 | 1.15 |
| User <br> Defined <br> Recreational | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |
| $\begin{aligned} & \text { User } \quad- \\ & \text { Defined } \\ & \text { Commercial } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $<0.005$ | $<0.005$ |



### 4.7. Offroad Emissions By Equipment Type

### 4.7.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| $\begin{aligned} & \text { Equipme } \\ & \text { nt } \\ & \text { Type } \end{aligned}$ | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

4.7.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Equipme nt Type | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

### 4.8. Stationary Emissions By Equipment Type

### 4.8.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Equipme <br> nt Type | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

4.8.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Equipme <br> nt Type | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

### 4.9. User Defined Emissions By Equipment Type

### 4.9.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Equipme nt Type | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

4.9.2. Mitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Equipme <br> nt <br> Type | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

### 4.10. Soil Carbon Accumulation By Vegetation Type

4.10.1. Soil Carbon Accumulation By Vegetation Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Vegetatio <br> n | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 9.38 | 9.38 | - | - | - | 9.38 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 9.38 | 9.38 | - | - | - | 9.38 |

### 4.10.2. Above and Belowground Carbon Accumulation by Land Use Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Shrublan d | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Shrublan <br> d | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Shrublan d | - | - | - | - | - | - | - | - | - | - | - | - | 34.7 | 34.7 | - | - | - | 34.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 34.7 | 34.7 | - | - | - | 34.7 |

### 4.10.3. Avoided and Sequestered Emissions by Species - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Species | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Avoided | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Sequest ered | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Remove d | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, <br> Winter <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Avoided | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Sequest <br> ered | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Remove | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Avoided | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Sequest ered | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $\begin{aligned} & \text { Remove } \\ & \text { d } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

### 4.10.4. Soil Carbon Accumulation By Vegetation Type - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Vegetatio | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 56.7 | 56.7 | - | - | - | 56.7 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Grazing | - | - | - | - | - | - | - | - | - | - | - | - | 9.38 | 9.38 | - | - | - | 9.38 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 9.38 | 9.38 | - | - | - | 9.38 |

### 4.10.5. Above and Belowground Carbon Accumulation by Land Use Type - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Shrublan d | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Shrublan d | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 210 | 210 | - | - | - | 210 |


| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shrublan d | - | - | - | - | - | - | - | - | - | - | - | - | 34.7 | 34.7 | - | - | - | 34.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 34.7 | 34.7 | - | - | - | 34.7 |

4.10.6. Avoided and Sequestered Emissions by Species - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Species | TOG | ROG | Nox | co | SO2 | PM10E | PMM0D | PM10t | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | СО2т | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Avoided | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Sequest ered | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $\begin{aligned} & \text { Remove } \\ & \text { d } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Avoided | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Sequest ered | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $\begin{aligned} & \text { Remove } \\ & \text { d } \end{aligned}$ | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Subtotal | - | - | - | - | - | - | - | - |  | - | - | - | - | - | - | - | - | - |



## 5. Activity Data

### 5.1. Construction Schedule

| Phase Name | Phase Type | Start Date | End Date | Days Per Week | Work Days per Phase | Phase Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Demolition | Demolition | 1/1/2024 | 1/29/2024 | 5.00 | 20.0 | - |
| Site Preparation | Site Preparation | 1/30/2024 | 2/13/2024 | 5.00 | 10.0 | - |
| Grading | Grading | 2/14/2024 | 3/27/2024 | 5.00 | 30.0 | - |
| Building Construction | Building Construction | 3/28/2024 | 5/22/2025 | 5.00 | 300 | - |
| Paving | Paving | 5/23/2025 | 6/20/2025 | 5.00 | 20.0 | - |
| Architectural Coating | Architectural Coating | 6/21/2025 | 7/19/2025 | 5.00 | 20.0 | - |

### 5.2. Off-Road Equipment

### 5.2.1. Unmitigated

| Demolition | Rubber Tired Dozers | Diesel | Average | 2.00 | 8.00 | 367 | 0.40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Demolition | Excavators | Diesel | Average | 3.00 | 8.00 | 36.0 | 0.38 |
| Demolition | Concrete/Industrial Saws | Diesel | Average | 1.00 | 8.00 | 33.0 | 0.73 |
| Site Preparation | Rubber Tired Dozers | Diesel | Average | 3.00 | 8.00 | 367 | 0.40 |
| Site Preparation | Tractors/Loaders/Backh oes | Diesel | Average | 4.00 | 8.00 | 84.0 | 0.37 |
| Grading | Graders | Diesel | Average | 1.00 | 8.00 | 148 | 0.41 |
| Grading | Excavators | Diesel | Average | 2.00 | 8.00 | 36.0 | 0.38 |
| Grading | Tractors/Loaders/Backh oes | Diesel | Average | 2.00 | 8.00 | 84.0 | 0.37 |
| Grading | Scrapers | Diesel | Average | 2.00 | 8.00 | 423 | 0.48 |
| Grading | Rubber Tired Dozers | Diesel | Average | 1.00 | 8.00 | 367 | 0.40 |
| Building Construction | Forklifts | Diesel | Average | 3.00 | 8.00 | 82.0 | 0.20 |
| Building Construction | Generator Sets | Diesel | Average | 1.00 | 8.00 | 14.0 | 0.74 |
| Building Construction | Cranes | Diesel | Average | 1.00 | 7.00 | 367 | 0.29 |
| Building Construction | Welders | Diesel | Average | 1.00 | 8.00 | 46.0 | 0.45 |
| Building Construction | Tractors/Loaders/Backh oes | Diesel | Average | 3.00 | 7.00 | 84.0 | 0.37 |
| Paving | Pavers | Diesel | Average | 2.00 | 8.00 | 81.0 | 0.42 |
| Paving | Paving Equipment | Diesel | Average | 2.00 | 8.00 | 89.0 | 0.36 |
| Paving | Rollers | Diesel | Average | 2.00 | 8.00 | 36.0 | 0.38 |
| Architectural Coating | Air Compressors | Diesel | Average | 1.00 | 6.00 | 37.0 | 0.48 |

### 5.2.2. Mitigated

| Phase Name | Equipment Type | Fuel Type | Engine Tier | Number per Day | Hours Per Day | Horsepower | Load Factor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Demolition | Rubber Tired Dozers | Diesel | Average | 2.00 | 8.00 | 367 | 0.40 |
| Demolition | Excavators | Diesel | Average | 3.00 | 8.00 | 36.0 | 0.38 |

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| Demolition | Concrete/Industrial Saws | Diesel | Average | 1.00 | 8.00 | 33.0 | 0.73 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Preparation | Rubber Tired Dozers | Diesel | Average | 3.00 | 8.00 | 367 | 0.40 |
| Site Preparation | Tractors/Loaders/Backh oes | Diesel | Average | 4.00 | 8.00 | 84.0 | 0.37 |
| Grading | Graders | Diesel | Average | 1.00 | 8.00 | 148 | 0.41 |
| Grading | Excavators | Diesel | Average | 2.00 | 8.00 | 36.0 | 0.38 |
| Grading | Tractors/Loaders/Backh oes | Diesel | Average | 2.00 | 8.00 | 84.0 | 0.37 |
| Grading | Scrapers | Diesel | Average | 2.00 | 8.00 | 423 | 0.48 |
| Grading | Rubber Tired Dozers | Diesel | Average | 1.00 | 8.00 | 367 | 0.40 |
| Building Construction | Forklifts | Diesel | Average | 3.00 | 8.00 | 82.0 | 0.20 |
| Building Construction | Generator Sets | Diesel | Average | 1.00 | 8.00 | 14.0 | 0.74 |
| Building Construction | Cranes | Diesel | Average | 1.00 | 7.00 | 367 | 0.29 |
| Building Construction | Welders | Diesel | Average | 1.00 | 8.00 | 46.0 | 0.45 |
| Building Construction | Tractors/Loaders/Backh oes | Diesel | Average | 3.00 | 7.00 | 84.0 | 0.37 |
| Paving | Pavers | Diesel | Average | 2.00 | 8.00 | 81.0 | 0.42 |
| Paving | Paving Equipment | Diesel | Average | 2.00 | 8.00 | 89.0 | 0.36 |
| Paving | Rollers | Diesel | Average | 2.00 | 8.00 | 36.0 | 0.38 |
| Architectural Coating | Air Compressors | Diesel | Average | 1.00 | 6.00 | 37.0 | 0.48 |

### 5.3. Construction Vehicles

### 5.3.1. Unmitigated

| Phase Name | Trip Type | One-Way Trips per Day | Miles per Trip | Vehicle Mix |
| :---: | :---: | :---: | :---: | :---: |
| Demolition | - | - | - | - |
| Demolition | Worker | 15.0 | 14.1 | LDA,LDT1,LDT2 |
| Demolition | Vendor | - | 8.98 | HHDT,MHDT |

Project in Amador County Custom Report, 11/10/2023

| Demolition | Hauling | 13.0 | 20.0 | HHDT |
| :---: | :---: | :---: | :---: | :---: |
| Demolition | Onsite truck | - | - | HHDT |
| Site Preparation | - | - | - | - |
| Site Preparation | Worker | 17.5 | 14.1 | LDA,LDT1,LDT2 |
| Site Preparation | Vendor | - | 8.98 | HHDT,MHDT |
| Site Preparation | Hauling | 0.00 | 20.0 | HHDT |
| Site Preparation | Onsite truck | - | - | HHDT |
| Grading | - | - | - | - |
| Grading | Worker | 20.0 | 14.1 | LDA,LDT1,LDT2 |
| Grading | Vendor | - | 8.98 | HHDT,MHDT |
| Grading | Hauling | 300 | 20.0 | HHDT |
| Grading | Onsite truck | - | - | HHDT |
| Building Construction | - | - | - | - |
| Building Construction | Worker | 19.8 | 14.1 | LDA,LDT1,LDT2 |
| Building Construction | Vendor | 8.41 | 8.98 | HHDT,MHDT |
| Building Construction | Hauling | 0.00 | 20.0 | HHDT |
| Building Construction | Onsite truck | - | - | HHDT |
| Paving | - | - | - | - |
| Paving | Worker | 15.0 | 14.1 | LDA,LDT1,LDT2 |
| Paving | Vendor | - | 8.98 | HHDT,MHDT |
| Paving | Hauling | 0.00 | 20.0 | HHDT |
| Paving | Onsite truck | - | - | HHDT |
| Architectural Coating | - | - | - | - |
| Architectural Coating | Worker | 3.96 | 14.1 | LDA,LDT1,LDT2 |
| Architectural Coating | Vendor | - | 8.98 | HHDT,MHDT |
| Architectural Coating | Hauling | 0.00 | 20.0 | HHDT |
| Architectural Coating | Onsite truck | - | - | HHDT |

### 5.3.2. Mitigated

| Phase Name | Trip Type | One-Way Trips per Day | Miles per Trip | Vehicle Mix |
| :---: | :---: | :---: | :---: | :---: |
| Demolition | - | - | - | - |
| Demolition | Worker | 15.0 | 14.1 | LDA,LDT1,LDT2 |
| Demolition | Vendor | - | 8.98 | HHDT,MHDT |
| Demolition | Hauling | 13.0 | 20.0 | HHDT |
| Demolition | Onsite truck | - | - | HHDT |
| Site Preparation | - | - | - | - |
| Site Preparation | Worker | 17.5 | 14.1 | LDA,LDT1,LDT2 |
| Site Preparation | Vendor | - | 8.98 | HHDT,MHDT |
| Site Preparation | Hauling | 0.00 | 20.0 | HHDT |
| Site Preparation | Onsite truck | - | - | HHDT |
| Grading | - | - | - | - |
| Grading | Worker | 20.0 | 14.1 | LDA,LDT1,LDT2 |
| Grading | Vendor | - | 8.98 | HHDT,MHDT |
| Grading | Hauling | 300 | 20.0 | HHDT |
| Grading | Onsite truck | - | - | HHDT |
| Building Construction | - | - | - | - |
| Building Construction | Worker | 19.8 | 14.1 | LDA,LDT1,LDT2 |
| Building Construction | Vendor | 8.41 | 8.98 | HHDT,MHDT |
| Building Construction | Hauling | 0.00 | 20.0 | HHDT |
| Building Construction | Onsite truck | - | - | HHDT |
| Paving | - | - | - | - |
| Paving | Worker | 15.0 | 14.1 | LDA,LDT1,LDT2 |
| Paving | Vendor | - | 8.98 | HHDT,MHDT |
| Paving | Hauling | 0.00 | 20.0 | HHDT |
| Paving | Onsite truck | - | - | HHDT |


| Architectural Coating | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: |
| Architectural Coating | Worker | 3.96 | 14.1 | LDA,LDT1,LDT2 |
| Architectural Coating | Vendor | - | 8.98 | HHDT,MHDT |
| Architectural Coating | Hauling | 0.00 | 20.0 | HHDT |
| Architectural Coating | Onsite truck | - | - | HHDT |

### 5.4. Vehicles

### 5.4.1. Construction Vehicle Control Strategies


5.5. Architectural Coatings

| Phase Name | Residential Interior Area Coated (sq ft) | Residential Exterior Area Coated (sq ft) | Non-Residential Interior Area Coated (sq ft) | Non-Residential Exterior Area Coated (sq ft) | Parking Area Coated (sq ft) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Architectural Coating | 0.00 | 0.00 | 76,965 | 25,655 | 15,807 |

### 5.6. Dust Mitigation

### 5.6.1. Construction Earthmoving Activities

| Phase Name | Material Imported (cy) | Material Exported (cy) | Acres Graded (acres) | Material Demolished (Building Square Footage) | Acres Paved (acres) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Demolition | 0.00 | 0.00 | 0.00 | 22,526 | - |
| Site Preparation | - | - | 15.0 | 0.00 | - |
| Grading | 36,009 | 36,042 | 90.0 | 0.00 | - |
| Paving | 0.00 | 0.00 | 0.00 | 0.00 | 6.05 |

### 5.6.2. Construction Earthmoving Control Strategies

Non-applicable. No control strategies activated by user.

### 5.7. Construction Paving

| Land Use | Area Paved (acres) | \% Asphalt |
| :---: | :---: | :---: |
| User Defined Recreational | 0.00 | 0\% |
| High Turnover (Sit Down Restaurant) | 0.00 | 0\% |
| Fast Food Restaurant w/o Drive Thru | 0.00 | 0\% |
| User Defined Commercial | 0.00 | 0\% |
| Parking Lot | 6.05 | 100\% |

### 5.8. Construction Electricity Consumption and Emissions Factors

kWh per Year and Emission Factor ( $\mathrm{l} / \mathrm{MWh}$ )

| Year | kWh per Year | CO 2 | CH4 | N2O |
| :---: | :---: | :---: | :---: | :---: |
| 2024 | 0.00 | 204 | 0.03 | < 0.005 |
| 2025 | 0.00 | 204 | 0.03 | < 0.005 |

### 5.9. Operational Mobile Sources

5.9.1. Unmitigated

| Land Use Type | Trips/Weekday | Trips/Saturday | Trips/Sunday | Trips/Year | VMT/Weekday | VMT/Saturday | VMT/Sunday | VMT/Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreational | 2,475 | 2,475 | 2,475 | 903,515 | 24,676 | 24,676 | 24,676 | 9,006,649 |
| High Turnover (Sit Down Restaurant) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Fast Food <br> Restaurant w/o Drive Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| User Defined Commercial | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 5.9.2. Mitigated

| Land Use Type | Trips/Weekday | Trips/Saturday | Trips/Sunday | Trips/Year | VMT/Weekday | VMT/Saturday | VMT/Sunday | VMT/Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreational | 2,475 | 2,475 | 2,475 | 903,515 | 24,676 | 24,676 | 24,676 | 9,006,649 |
| High Turnover (Sit Down Restaurant) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Fast Food Restaurant w/o Drive Thru | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| User Defined Commercial | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 5.10. Operational Area Sources

### 5.10.2. Architectural Coatings

| Residential Interior Area Coated (sq ft) | Residential Exterior Area Coated (sq ft) | Non-Residential Interior Area Coated <br> $(\mathrm{sq} \mathrm{ft})$ | Non-Residential Exterior Area Coated <br> $(\mathrm{sq} \mathrm{ft})$ | Parking Area Coated (sq ft) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0.00 | 76,965 | 25,655 |  |

### 5.10.3. Landscape Equipment

| Season | Unit | Value |
| :--- | :--- | :--- | :--- |
| Snow Days | day/yr | 0.00 |
| Summer Days | day/yr | 180 |

5.10.4. Landscape Equipment - Mitigated

| Season | Unit | Value |
| :--- | :--- | :--- |
| Snow Days | day/yr | 0.00 |

### 5.11. Operational Energy Consumption

### 5.11.1. Unmitigated

Electricity (kWh/yr) and CO2 and CH4 and N 2 O and Natural Gas (kBTU/yr)

| Land Use | Electricity (kWh/yr) | CO2 | CH4 | N2O | Natural Gas (kBTU/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreational | 488,171 | 204 | 0.0330 | 0.0040 | 1,284,660 |
| High Turnover (Sit Down Restaurant) | 161,980 | 204 | 0.0330 | 0.0040 | 491,546 |
| Fast Food Restaurant w/o Drive Thru | 178,965 | 204 | 0.0330 | 0.0040 | 543,089 |
| User Defined Commercial | 0.00 | 204 | 0.0330 | 0.0040 | 0.00 |
| Parking Lot | 230,783 | 204 | 0.0330 | 0.0040 | 0.00 |

### 5.11.2. Mitigated

Electricity (kWh/yr) and CO2 and CH4 and N 2 O and Natural Gas (kBTU/yr)

| Land Use | Electricity (kWh/yr) | CO2 | CH 4 | N2O | Natural Gas (kBTU/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| User Defined Recreational | 488,171 | 204 | 0.0330 | 0.0040 | 1,284,660 |
| High Turnover (Sit Down Restaurant) | 161,980 | 204 | 0.0330 | 0.0040 | 491,546 |
| Fast Food Restaurant w/o Drive Thru | 178,965 | 204 | 0.0330 | 0.0040 | 543,089 |
| User Defined Commercial | 0.00 | 204 | 0.0330 | 0.0040 | 0.00 |
| Parking Lot | 230,783 | 204 | 0.0330 | 0.0040 | 0.00 |

5.12. Operational Water and Wastewater Consumption
5.12.1. Unmitigated

| Land Use | Indoor Water (gal/year) | Outdoor Water (gal/year) |
| :---: | :---: | :---: |
| User Defined Recreational | 16,790,000 | 3,650,000 |
| High Turnover (Sit Down Restaurant) | 0.00 | 0.00 |
| Fast Food Restaurant w/o Drive Thru | 0.00 | 0.00 |
| User Defined Commercial | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 |

### 5.12.2. Mitigated

| Land Use | Indoor Water (gal/year) | Outdoor Water (gal/year) |
| :---: | :---: | :---: |
| User Defined Recreational | 16,790,000 | 3,650,000 |
| High Turnover (Sit Down Restaurant) | 0.00 | 0.00 |
| Fast Food Restaurant w/o Drive Thru | 0.00 | 0.00 |
| User Defined Commercial | 0.00 | 0.00 |
| Parking Lot | 0.00 | 0.00 |

### 5.13. Operational Waste Generation

### 5.13.1. Unmitigated

| Land Use | Waste (ton/year) | Cogeneration (kWh/year) |
| :---: | :---: | :---: |
| User Defined Recreational | 26.5 | - |
| High Turnover (Sit Down Restaurant) | 48.0 | - |
| Fast Food Restaurant w/o Drive Thru | 51.3 | - |
| User Defined Commercial | 18.5 | - |
| Parking Lot | 0.00 | - |

### 5.13.2. Mitigated

| Land Use | Waste (ton/year) | Cogeneration (kWh/year) |  |
| :--- | :--- | :--- | :--- |
| User Defined Recreational | 26.5 | - |  |
| High Turnover (Sit Down Restaurant) | 48.0 | - |  |
| Fast Food Restaurant w/o Drive Thru | 51.3 | - |  |
| User Defined Commercial | 18.5 | - |  |
| Parking Lot | 0.00 | - |  |

### 5.14. Operational Refrigeration and Air Conditioning Equipment

### 5.14.1. Unmitigated

| Land Use Type | Equipment Type | Refrigerant | GWP | Quantity (kg) | Operations Leak Rate | Service Leak Rate | Times Serviced |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High Turnover (Sit Down Restaurant) | Household refrigerators and/or freezers | R-134a | 1,430 | 0.00 | 0.60 | 0.00 | 1.00 |
| High Turnover (Sit Down Restaurant) | Other commercial A/C and heat pumps | R-410A | 2,088 | 1.80 | 4.00 | 4.00 | 18.0 |
| High Turnover (Sit Down Restaurant) | Walk-in refrigerators and freezers | R-404A | 3,922 | $<0.005$ | 7.50 | 7.50 | 20.0 |
| Fast Food Restaurant w/o Drive Thru | Household refrigerators and/or freezers | R-134a | 1,430 | 0.00 | 0.60 | 0.00 | 1.00 |
| Fast Food Restaurant w/o Drive Thru | Other commercial A/C and heat pumps | R-410A | 2,088 | 1.80 | 4.00 | 4.00 | 18.0 |
| Fast Food Restaurant w/o Drive Thru | Walk-in refrigerators and freezers | R-404A | 3,922 | $<0.005$ | 7.50 | 7.50 | 20.0 |
| User Defined Recreational | Other commercial A/C and heat pumps | R-410A | 2,088 | $<0.005$ | 0.04 | 0.04 | 18.0 |
| User Defined Commercial | Other commercial A/C and heat pumps | R-410A | 2,088 | $<0.005$ | 0.04 | 0.04 | 18.0 |
| User Defined Commercial | Stand-alone retail refrigerators and freezers | R-134a | 1,430 | 0.04 | 0.01 | 0.00 | 1.00 |

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| User Defined <br> Recreational | Stand-alone retail <br> refrigerators and <br> freezers | R-134a | 1,430 | 0.04 | 0.01 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

### 5.14.2. Mitigated

| Land Use Type | Equipment Type | Refrigerant | GWP | Quantity (kg) | Operations Leak Rate | Service Leak Rate | Times Serviced |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High Turnover (Sit Down Restaurant) | Household refrigerators and/or freezers | R-134a | 1,430 | 0.00 | 0.60 | 0.00 | 1.00 |
| High Turnover (Sit Down Restaurant) | Other commercial A/C and heat pumps | R-410A | 2,088 | 1.80 | 4.00 | 4.00 | 18.0 |
| High Turnover (Sit Down Restaurant) | Walk-in refrigerators and freezers | R-404A | 3,922 | < 0.005 | 7.50 | 7.50 | 20.0 |
| Fast Food Restaurant w/o Drive Thru | Household refrigerators and/or freezers | R-134a | 1,430 | 0.00 | 0.60 | 0.00 | 1.00 |
| Fast Food Restaurant w/o Drive Thru | Other commercial A/C and heat pumps | R-410A | 2,088 | 1.80 | 4.00 | 4.00 | 18.0 |
| Fast Food Restaurant w/o Drive Thru | Walk-in refrigerators and freezers | R-404A | 3,922 | $<0.005$ | 7.50 | 7.50 | 20.0 |
| User Defined Recreational | Other commercial A/C and heat pumps | R-410A | 2,088 | $<0.005$ | 0.04 | 0.04 | 18.0 |
| User Defined Commercial | Other commercial A/C and heat pumps | R-410A | 2,088 | < 0.005 | 0.04 | 0.04 | 18.0 |
| User Defined Commercial | Stand-alone retail refrigerators and freezers | R-134a | 1,430 | 0.04 | 0.01 | 0.00 | 1.00 |
| User Defined Recreational | Stand-alone retail refrigerators and freezers | R-134a | 1,430 | 0.04 | 0.01 | 0.00 | 1.00 |

### 5.18. Vegetation

### 5.18.1. Land Use Change

### 5.18.1.1. Unmitigated

| Vegetation Land Use Type | Vegetation Soil Type | Initial Acres | Final Acres |
| :---: | :---: | :---: | :---: |
| Grazing | Entisols | 13.2 | 0.00 |
| 5.18.1.2. Mitigated |  |  |  |
| Vegetation Land Use Type | Vegetation Soil Type | Initial Acres | Final Acres |
| Grazing | Entisols | 13.2 | 0.00 |

### 5.18.1. Biomass Cover Type

### 5.18.1.1. Unmitigated

| Biomass Cover Type | Initial Acres | Final Acres |
| :--- | :--- | :--- |
| Shrubland | 13.2 | 0.00 |
|  |  |  |
| 5.18.1.2. Mitigated |  |  |
| Biomass Cover Type | 13.2 | Finitial Acres |
| Shrubland |  | 0.00 |

### 5.18.2. Sequestration

5.18.2.1. Unmitigated

| Tree Type | Number | Electricity Saved (kWh/year) | Natural Gas Saved (btu/year) |
| :--- | :--- | :--- | :--- |

### 5.18.2.2. Mitigated

| Tree Type | Number | Electricity Saved (kWh/year) | Natural Gas Saved (btu/year) |
| :---: | :---: | :---: | :---: |

## 8. User Changes to Default Data

| Screen | Justification |
| :---: | :---: |
| Land Use | site specific information. Recreational user defined is casino floor, commercial user defined is back of house. High turnover is bar and fast food is cafe. <br> It was assumed all acreage to the first land use and parking. Assumed 2 acres of landscaping. |
| Operations: Vehicle Data | used the traffic report ADT of 2475. Assumed all trips were primary trips since this is a destination. |
| Operations: Energy Use | Used data from EIA 2018 CBECS study for Other Public Assembly $11.4 \mathrm{kWh} / \mathrm{sqft}$ and kbtu/sqft and combined casino and back of floor square footage. Others are default. Used T24 and NonT24 from Movie theater for casino splits. |
| Operations: Water and Waste Water | Based on estimate of 46,000 gpd inside and 10,000 gpd exterior. Project is building membrane bioreactor and will process solids offsite. <br> Recycled water will be used which is assumed to be up to $17,000 \mathrm{gpd}$. Water is allocated to first land use but includes all from project. |
| Operations: Solid Waste | Estimated casino similar to regional shopping center. |
| Operations: Refrigerants | Added other commercial $A / C$ heat pumps and stand alone refrigeration at rates similar to shopping center. |

## Amador Hotel Custom Report

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8. User Changes to Default Data

## 1. Basic Project Information

### 1.1. Basic Project Information

| Data Field | Value |
| :---: | :---: |
| Project Name | Amador Hotel |
| Operational Year | 2025 |
| Lead Agency | - |
| Land Use Scale | Project/site |
| Analysis Level for Defaults | County |
| Windspeed (m/s) | 2.70 |
| Precipitation (days) | 21.2 |
| Location | 38.46655475780352, -120.85385747969197 |
| County | Amador |
| City | Plymouth |
| Air District | Amador County APCD |
| Air Basin | Mountain Counties |
| TAZ | 3003 |
| EDFZ | 4 |
| Electric Utility | Pacific Gas \& Electric Company |
| Gas Utility | Pacific Gas \& Electric |
| App Version | 2022.1.1.20 |

### 1.2. Land Use Types

| Land Use Subtype | Size | Unit | Lot Acreage | Building Area (sq ft) | Landscape Area (sq ft) | Special Landscape <br> Area (sq ft) | Population | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hotel | 46.0 | Room | 1.53 | 22,526 | 0.20 | 0.00 | - | - |

### 1.3. User-Selected Emission Reduction Measures by Emissions Sector

## No measures selected

## 2. Emissions Summary

### 2.4. Operations Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Un/Mit. | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 3.74 | 4.12 | 3.73 | 23.6 | 0.04 | 0.07 | 2.63 | 2.70 | 0.07 | 0.67 | 0.74 | 15.8 | 3,787 | 3,803 | 1.81 | 0.22 | 50.1 | 3,962 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 3.10 | 3.48 | 4.19 | 19.6 | 0.03 | 0.07 | 2.63 | 2.70 | 0.07 | 0.67 | 0.74 | 15.8 | 3,540 | 3,556 | 1.83 | 0.23 | 35.6 | 3,706 |
| Average Daily <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 3.23 | 3.61 | 4.05 | 20.2 | 0.03 | 0.07 | 2.60 | 2.67 | 0.07 | 0.66 | 0.73 | 15.8 | 3,598 | 3,613 | 1.82 | 0.23 | 41.7 | 3,768 |
| Annual (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Unmit. | 0.59 | 0.66 | 0.74 | 3.68 | 0.01 | 0.01 | 0.47 | 0.49 | 0.01 | 0.12 | 0.13 | 2.62 | 596 | 598 | 0.30 | 0.04 | 6.90 | 624 |

### 2.5. Operations Emissions by Sector, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Sector | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Mobile | 3.54 | 3.32 | 3.53 | 22.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,473 | 3,473 | 0.19 | 0.21 | 14.9 | 3,554 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area | 0.17 | 0.79 | 0.01 | 0.98 | < 0.005 | <0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 4.03 | 4.03 | $<0.005$ | < 0.005 | - | 4.04 |
| Energy | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 308 | 308 | 0.03 | $<0.005$ | - | 309 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Total | 3.74 | 4.12 | 3.73 | 23.6 | 0.04 | 0.07 | 2.63 | 2.70 | 0.07 | 0.67 | 0.74 | 15.8 | 3,787 | 3,803 | 1.81 | 0.22 | 50.1 | 3,962 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 3.08 | 2.84 | 4.00 | 19.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,230 | 3,230 | 0.21 | 0.22 | 0.39 | 3,303 |
| Area | - | 0.63 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Energy | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 308 | 308 | 0.03 | $<0.005$ | - | 309 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Total | 3.10 | 3.48 | 4.19 | 19.6 | 0.03 | 0.07 | 2.63 | 2.70 | 0.07 | 0.67 | 0.74 | 15.8 | 3,540 | 3,556 | 1.83 | 0.23 | 35.6 | 3,706 |
| Average Daily | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 3.12 | 2.90 | 3.85 | 19.5 | 0.03 | 0.05 | 2.60 | 2.65 | 0.05 | 0.66 | 0.71 | - | 3,286 | 3,286 | 0.20 | 0.22 | 6.44 | 3,362 |
| Area | 0.09 | 0.70 | $<0.005$ | 0.48 | < 0.005 | <0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 1.99 | 1.99 | < 0.005 | $<0.005$ | - | 1.99 |
| Energy | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 308 | 308 | 0.03 | $<0.005$ | - | 309 |
| Water | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Total | 3.23 | 3.61 | 4.05 | 20.2 | 0.03 | 0.07 | 2.60 | 2.67 | 0.07 | 0.66 | 0.73 | 15.8 | 3,598 | 3,613 | 1.82 | 0.23 | 41.7 | 3,768 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Mobile | 0.57 | 0.53 | 0.70 | 3.56 | 0.01 | 0.01 | 0.47 | 0.48 | 0.01 | 0.12 | 0.13 | - | 544 | 544 | 0.03 | 0.04 | 1.07 | 557 |
| Area | 0.02 | 0.13 | <0.005 | 0.09 | < 0.005 | < 0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 0.33 | 0.33 | < 0.005 | < 0.005 | - | 0.33 |


| Energy | $<0.005$ | $<0.005$ | 0.04 | 0.03 | $<0.005$ | $<0.005$ | - | < 0.005 | $<0.005$ | - | < 0.005 | - | 51.0 | 51.0 | 0.01 | < 0.005 | - | 51.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Water | - | - | - | - | - | - | - | - | - | - | - | 0.37 | 0.35 | 0.72 | 0.04 | $<0.005$ | - | 1.94 |
| Waste | - | - | - | - | - | - | - | - | - | - | - | 2.25 | 0.00 | 2.25 | 0.22 | 0.00 | - | 7.86 |
| Refrig. | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 5.83 | 5.83 |
| Total | 0.59 | 0.66 | 0.74 | 3.68 | 0.01 | 0.01 | 0.47 | 0.49 | 0.01 | 0.12 | 0.13 | 2.62 | 596 | 598 | 0.30 | 0.04 | 6.90 | 624 |

## 4. Operations Emissions Details

### 4.1. Mobile Emissions by Land Use

### 4.1.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | 3.54 | 3.32 | 3.53 | 22.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,473 | 3,473 | 0.19 | 0.21 | 14.9 | 3,554 |
| Total | 3.54 | 3.32 | 3.53 | 22.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,473 | 3,473 | 0.19 | 0.21 | 14.9 | 3,554 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | 3.08 | 2.84 | 4.00 | 19.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,230 | 3,230 | 0.21 | 0.22 | 0.39 | 3,303 |
| Total | 3.08 | 2.84 | 4.00 | 19.5 | 0.03 | 0.05 | 2.63 | 2.69 | 0.05 | 0.67 | 0.72 | - | 3,230 | 3,230 | 0.21 | 0.22 | 0.39 | 3,303 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | 0.57 | 0.53 | 0.70 | 3.56 | 0.01 | 0.01 | 0.47 | 0.48 | 0.01 | 0.12 | 0.13 | - | 544 | 544 | 0.03 | 0.04 | 1.07 | 557 |
| Total | 0.57 | 0.53 | 0.70 | 3.56 | 0.01 | 0.01 | 0.47 | 0.48 | 0.01 | 0.12 | 0.13 | - | 544 | 544 | 0.03 | 0.04 | 1.07 | 557 |

4.2. Energy

### 4.2.1. Electricity Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | 77.1 | 77.1 | 0.01 | $<0.005$ | - | 77.9 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 77.1 | 77.1 | 0.01 | < 0.005 | - | 77.9 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | 77.1 | 77.1 | 0.01 | < 0.005 | - | 77.9 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 77.1 | 77.1 | 0.01 | < 0.005 | - | 77.9 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | 12.8 | 12.8 | $<0.005$ | $<0.005$ | - | 12.9 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | 12.8 | 12.8 | $<0.005$ | $<0.005$ | - | 12.9 |

### 4.2.3. Natural Gas Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 231 | 231 | 0.02 | < 0.005 | - | 231 |
| Total | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 231 | 231 | 0.02 | < 0.005 | - | 231 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Hotel | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 231 | 231 | 0.02 | < 0.005 | - | 231 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | 0.02 | 0.01 | 0.19 | 0.16 | < 0.005 | 0.01 | - | 0.01 | 0.01 | - | 0.01 | - | 231 | 231 | 0.02 | < 0.005 | - | 231 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | < 0.005 | < 0.005 | 0.04 | 0.03 | < 0.005 | <0.005 | - | $<0.005$ | < 0.005 | - | < 0.005 | - | 38.2 | 38.2 | < 0.005 | < 0.005 | - | 38.3 |
| Total | < 0.005 | < 0.005 | 0.04 | 0.03 | < 0.005 | < 0.005 | - | < 0.005 | < 0.005 | - | < 0.005 | - | 38.2 | 38.2 | < 0.005 | < 0.005 | - | 38.3 |

### 4.3. Area Emissions by Source

### 4.3.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (Ib/day for daily, MT/yr for annual)

| Source | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, <br> Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum <br> er <br> Products | - | 0.48 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural Coatings | - | 0.14 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Landsca pe Equipme nt | 0.17 | 0.16 | 0.01 | 0.98 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 4.03 | 4.03 | $<0.005$ | < 0.005 | - | 4.04 |
| Total | 0.17 | 0.79 | 0.01 | 0.98 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 4.03 | 4.03 | $<0.005$ | $<0.005$ | - | 4.04 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum er Products | - | 0.48 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Architect ural Coatings | - | 0.14 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total | - | 0.63 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Consum <br> er <br> Products | - | 0.09 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Architect ural <br> Coatings | - | 0.03 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Landsca pe Equipme nt | 0.02 | 0.01 | < 0.005 | 0.09 | < 0.005 | $<0.005$ | - | < 0.005 | < 0.005 | - | $<0.005$ | - | 0.33 | 0.33 | $<0.005$ | $<0.005$ | - | 0.33 |
| Total | 0.02 | 0.13 | $<0.005$ | 0.09 | $<0.005$ | $<0.005$ | - | $<0.005$ | $<0.005$ | - | $<0.005$ | - | 0.33 | 0.33 | < 0.005 | $<0.005$ | - | 0.33 |

### 4.4. Water Emissions by Land Use

### 4.4.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH 4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 2.24 | 2.13 | 4.36 | 0.23 | 0.01 | - | 11.7 |


| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 0.37 | 0.35 | 0.72 | 0.04 | $<0.005$ | - | 1.94 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 0.37 | 0.35 | 0.72 | 0.04 | < 0.005 | - | 1.94 |

### 4.5. Waste Emissions by Land Use

### 4.5.1. Unmitigated

Criteria Pollutants (Ib/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land Use | TOG | ROG | NOx | co | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Daily, Winter (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 13.6 | 0.00 | 13.6 | 1.36 | 0.00 | - | 47.5 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | 2.25 | 0.00 | 2.25 | 0.22 | 0.00 | - | 7.86 |
| Total | - | - | - | - | - | - | - | - | - | - | - | 2.25 | 0.00 | 2.25 | 0.22 | 0.00 | - | 7.86 |

### 4.6. Refrigerant Emissions by Land Use

4.6.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

| Land <br> Use | TOG | ROG | NOx | CO | SO2 | PM10E | PM10D | PM10T | PM2.5E | PM2.5D | PM2.5T | BCO2 | NBCO2 | CO2T | CH4 | N2O | R | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| Daily, Summer (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Daily, <br> Winter <br> (Max) | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 35.2 | 35.2 |
| Annual | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Hotel | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 5.83 | 5.83 |
| Total | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 5.83 | 5.83 |

## 5. Activity Data

### 5.9. Operational Mobile Sources

### 5.9.1. Unmitigated

| Land Use Type | Trips/Weekday | Trips/Saturday | Trips/Sunday | Trips/Year | VMT/Weekday | VMT/Saturday | VMT/Sunday | VMT/Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hotel | 368 | 368 | 368 | 134,152 | 3,664 | 3,664 | 3,664 | 1,337,290 |

### 5.10. Operational Area Sources

### 5.10.2. Architectural Coatings

| Residential Interior Area Coated (sq ft) | Residential Exterior Area Coated (sq ft) | Non-Residential Interior Area Coated <br> $(\mathrm{sq} \mathrm{ft})$ | Non-Residential Exterior Area Coated <br> $(\mathrm{sq} \mathrm{ft})$ | Parking Area Coated (sq ft) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0.00 | 33,789 | 11,263 |  |

### 5.10.3. Landscape Equipment

| Season | Unit | Value |
| :--- | :--- | :--- |
| Snow Days | day/yr | 0.00 |
| Summer Days | daylyr | 180 |

### 5.11. Operational Energy Consumption

### 5.11.1. Unmitigated

Electricity (kWh/yr) and CO2 and CH4 and N2O and Natural Gas (kBTU/yr)

| Land Use | Electricity (kWh/yr) | CO2 | CH4 | N2O | Natural Gas (kBTU/yr) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Hotel | 138,041 | 204 | 0.0330 | 0.0040 | 719,863 |

### 5.12. Operational Water and Wastewater Consumption

### 5.12.1. Unmitigated

| Land Use | Indoor Water (gal/year) | Outdoor Water (gal/year) |
| :--- | :--- | :--- |
| Hotel | $1,166,871$ | 2.38 |

### 5.13. Operational Waste Generation

### 5.13.1. Unmitigated

| Land Use | Waste (ton/year) | Cogeneration (kWh/year) |
| :--- | :--- | :--- |
| Hotel | 25.2 | - |

5.14. Operational Refrigeration and Air Conditioning Equipment

### 5.14.1. Unmitigated

| Land Use Type | Equipment Type | Refrigerant | GWP | Quantity (kg) | Operations Leak Rate | Service Leak Rate | Times Serviced |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hotel | Household refrigerators and/or freezers | R-134a | 1,430 | 0.00 | 0.60 | 0.00 | 1.00 |
| Hotel | Other commercial A/C and heat pumps | R-410A | 2,088 | 1.80 | 4.00 | 4.00 | 18.0 |
| Hotel | Walk-in refrigerators and freezers | R-404A | 3,922 | $<0.005$ | 7.50 | 7.50 | 20.0 |

## 8. User Changes to Default Data

| Screen | Justification |
| :--- | :--- |
| Land Use | This is the hotel to be demolished as part of the project. This is to determine emissions that will be <br> netted out. |
| Operations: Vehicle Data | Value adjusted to match traffic study ADT |

## APPENDIX B

## Biological Resources Documents



# United States Department of the Interior 

FISH AND WILDLIFE SERVICE<br>Sacramento Fish And Wildlife Office Federal Building<br>2800 Cottage Way, Room W-2605<br>Sacramento, CA 95825-1846

Phone: (916) 414-6600 Fax: (916) 414-6713

In Reply Refer To:
December 06, 2023
Project Code: 2024-0023851
Project Name: IONE PLYMOUTH CASINO PROJECT
Subject: List of threatened and endangered species that may occur in your proposed project location or may be affected by your proposed project

## To Whom It May Concern:

The enclosed species list identifies threatened, endangered, proposed, and candidate species, as well as proposed and final designated critical habitat, that may occur within the boundary of your proposed project and/or may be affected by your proposed project. The species list fulfills the requirements of the U.S. Fish and Wildlife Service (Service) under section 7(c) of the Endangered Species Act (Act) of 1973, as amended (16 U.S.C. 1531 et seq.).

New information based on updated surveys, changes in the abundance and distribution of species, changed habitat conditions, or other factors could change this list. Please feel free to contact us if you need more current information or assistance regarding the potential impacts to federally proposed, listed, and candidate species and federally designated and proposed critical habitat. Please note that under 50 CFR 402.12(e) of the regulations implementing section 7 of the Act, the accuracy of this species list should be verified after 90 days. This verification can be completed formally or informally as desired. The Service recommends that verification be completed by visiting the IPaC website at regular intervals during project planning and implementation for updates to species lists and information. An updated list may be requested through IPaC by completing the same process used to receive the enclosed list.

The purpose of the Act is to provide a means whereby threatened and endangered species and the ecosystems upon which they depend may be conserved. Under sections 7(a)(1) and 7(a)(2) of the Act and its implementing regulations ( 50 CFR 402 et seq.), Federal agencies are required to utilize their authorities to carry out programs for the conservation of threatened and endangered species and to determine whether projects may affect threatened and endangered species and/or designated critical habitat.

A Biological Assessment is required for construction projects (or other undertakings having similar physical impacts) that are major Federal actions significantly affecting the quality of the human environment as defined in the National Environmental Policy Act (42 U.S.C. 4332(2)
(c)). For projects other than major construction activities, the Service suggests that a biological evaluation similar to a Biological Assessment be prepared to determine whether the project may affect listed or proposed species and/or designated or proposed critical habitat. Recommended contents of a Biological Assessment are described at 50 CFR 402.12.

If a Federal agency determines, based on the Biological Assessment or biological evaluation, that listed species and/or designated critical habitat may be affected by the proposed project, the agency is required to consult with the Service pursuant to 50 CFR 402. In addition, the Service recommends that candidate species, proposed species and proposed critical habitat be addressed within the consultation. More information on the regulations and procedures for section 7 consultation, including the role of permit or license applicants, can be found in the "Endangered Species Consultation Handbook" at: https://www.fws.gov/sites/default/files/documents/ endangered-species-consultation-handbook.pdf

Migratory Birds: In addition to responsibilities to protect threatened and endangered species under the Endangered Species Act (ESA), there are additional responsibilities under the Migratory Bird Treaty Act (MBTA) and the Bald and Golden Eagle Protection Act (BGEPA) to protect native birds from project-related impacts. Any activity, intentional or unintentional, resulting in take of migratory birds, including eagles, is prohibited unless otherwise permitted by the U.S. Fish and Wildlife Service (50 C.F.R. Sec. 10.12 and 16 U.S.C. Sec. 668(a)). For more information regarding these Acts, see Migratory Bird Permit | What We Do | U.S. Fish \& Wildlife Service (fws.gov).

The MBTA has no provision for allowing take of migratory birds that may be unintentionally killed or injured by otherwise lawful activities. It is the responsibility of the project proponent to comply with these Acts by identifying potential impacts to migratory birds and eagles within applicable NEPA documents (when there is a federal nexus) or a Bird/Eagle Conservation Plan (when there is no federal nexus). Proponents should implement conservation measures to avoid or minimize the production of project-related stressors or minimize the exposure of birds and their resources to the project-related stressors. For more information on avian stressors and recommended conservation measures, see https://www.fws.gov/library/collections/threats-birds.

In addition to MBTA and BGEPA, Executive Order 13186: Responsibilities of Federal Agencies to Protect Migratory Birds, obligates all Federal agencies that engage in or authorize activities that might affect migratory birds, to minimize those effects and encourage conservation measures that will improve bird populations. Executive Order 13186 provides for the protection of both migratory birds and migratory bird habitat. For information regarding the implementation of Executive Order 13186, please visit https://www.fws.gov/partner/council-conservation-migratory-birds.

We appreciate your concern for threatened and endangered species. The Service encourages Federal agencies to include conservation of threatened and endangered species into their project planning to further the purposes of the Act. Please include the Consultation Code in the header of this letter with any request for consultation or correspondence about your project that you submit to our office.

## Attachment(s):

- Official Species List


## OFFICIAL SPECIES LIST

This list is provided pursuant to Section 7 of the Endangered Species Act, and fulfills the requirement for Federal agencies to "request of the Secretary of the Interior information whether any species which is listed or proposed to be listed may be present in the area of a proposed action".

This species list is provided by:
Sacramento Fish And Wildlife Office
Federal Building
2800 Cottage Way, Room W-2605
Sacramento, CA 95825-1846
(916) 414-6600

## PROJECT SUMMARY

Project Code: 2024-0023851
Project Name: IONE PLYMOUTH CASINO PROJECT
Project Type: Commercial Development
Project Description: Casino Project
Project Location:
The approximate location of the project can be viewed in Google Maps: https:// www.google.com/maps/@38.46561625,-120.85052905125497,14z


Counties: Amador County, California

## ENDANGERED SPECIES ACT SPECIES

There is a total of 4 threatened, endangered, or candidate species on this species list.
Species on this list should be considered in an effects analysis for your project and could include species that exist in another geographic area. For example, certain fish may appear on the species list because a project could affect downstream species.

IPaC does not display listed species or critical habitats under the sole jurisdiction of NOAA Fisheries ${ }^{\underline{1}}$, as USFWS does not have the authority to speak on behalf of NOAA and the Department of Commerce.

See the "Critical habitats" section below for those critical habitats that lie wholly or partially within your project area under this office's jurisdiction. Please contact the designated FWS office if you have questions.

1. NOAA Fisheries, also known as the National Marine Fisheries Service (NMFS), is an office of the National Oceanic and Atmospheric Administration within the Department of Commerce.

## REPTILES

NAME STATUS

Northwestern Pond Turtle Actinemys marmorata
Proposed
No critical habitat has been designated for this species.
Threatened
Species profile: https://ecos.fws.gov/ecp/species/1111

## AMPHIBIANS

NAME STATUS

California Red-legged Frog Rana draytonii Threatened
There is final critical habitat for this species. Your location does not overlap the critical habitat. Species profile: https://ecos.fws.gov/ecp/species/2891

Foothill Yellow-legged Frog Rana boylii Endangered
Population: South Sierra Distinct Population Segment (South Sierra DPS) No critical habitat has been designated for this species.
Species profile: https://ecos.fws.gov/ecp/species/5133

## INSECTS

NAME STATUS
Monarch Butterfly Danaus plexippus
Candidate
No critical habitat has been designated for this species.
Species profile: https://ecos.fws.gov/ecp/species/9743

## CRITICAL HABITATS

THERE ARE NO CRITICAL HABITATS WITHIN YOUR PROJECT AREA UNDER THIS OFFICE'S JURISDICTION.

YOU ARE STILL REQUIRED TO DETERMINE IF YOUR PROJECT(S) MAY HAVE EFFECTS ON ALL ABOVE LISTED SPECIES.

## IPAC USER CONTACT INFORMATION

Agency: Ione Band of Miwok Indians of California
Name: Cedrick Villasenor
Address: 1801 7th Street, Suite 100
City: Sacramento
State: CA
Zip: 95811
Email cvillasenor@montrose-env.com
Phone: 9164473479


Esri, NASA, NGA, USGS | California State Parks, Esri, HERE, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, USDA


## NMFS ESA Critical Habitat Mapper


_- All_critical_habitat_line_20220404


## California Department of Fish and Wildlife

California Natural Diversity Database

## Query Criteria:

Quad<span style='color:Red'> IS </span>(Fiddletown (3812057)<span style='color:Red'> OR </span>Latrobe (3812058)<span style='color:Red'> OR </span>Aukum (3812056)<span style='color:Red'> OR </span>lrish Hill (3812048)<span style='color:Red'> OR </span>Amador City (3812047)<span style='color:Red'> OR </span>Pine Grove (3812046)<span style='color:Red'> OR </span>lone (3812038)<span style='color:Red'> OR </span>Jackson (3812037)<span style='color:Red'> OR </span>Mokelumne Hill (3812036))

| Element Code | Species | Federal Status | State Status | Global Rank | State Rank | Rare Plant <br> Rank/CDFW <br> SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AAAAA01181 | Ambystoma californiense pop. 1 <br> California tiger salamander - central California DPS | Threatened | Threatened | G2G3T3 | S3 | WL |
| AAABH01022 | Rana draytonii <br> California red-legged frog | Threatened | None | G2G3 | S2S3 | SSC |
| AAABH01055 | Rana boylii pop. 5 foothill yellow-legged frog - south Sierra DPS | Endangered | Endangered | G3T2 | S2 |  |
| ABNGA04010 | Ardea herodias great blue heron | None | None | G5 | S4 |  |
| ABNSB12040 | Strix nebulosa great gray owl | None | Endangered | G5 | S1 |  |
| ABPBXB0020 | Agelaius tricolor tricolored blackbird | None | Threatened | G1G2 | S2 | SSC |
| AMACC08010 | Corynorhinus townsendii <br> Townsend's big-eared bat | None | None | G4 | S2 | SSC |
| AMACC10010 | Antrozous pallidus pallid bat | None | None | G4 | S3 | SSC |
| AMAFJ01010 | Erethizon dorsatum <br> North American porcupine | None | None | G5 | S3 |  |
| ARAAD02030 | Emys marmorata western pond turtle | Proposed <br> Threatened | None | G3G4 | S3 | SSC |
| CARA2443CA | Central Valley Drainage Hardhead/Squawfish Stream Central Valley Drainage Hardhead/Squawfish Stream | None | None | GNR | SNR |  |
| CTT37D00CA | Ione Chaparral Ione Chaparral | None | None | G1 | S1.1 |  |
| ICMAL05460 | Stygobromus gradyi Grady's Cave amphipod | None | None | G1 | S1 |  |
| ICMAL05920 | Stygobromus grahami <br> Graham's Cave amphipod | None | None | G2 | S2 |  |
| IICOL48011 | Desmocerus californicus dimorphus valley elderberry longhorn beetle | Threatened | None | G3T3 | S3 |  |
| IICOL55040 | Hydroporus leechi <br> Leech's skyline diving beetle | None | None | G1? | S2S3 |  |
| IIHYM24260 | Bombus pensylvanicus <br> American bumble bee | None | None | G3G4 | S2 |  |
| IIHYM24480 | Bombus crotchii <br> Crotch bumble bee | None | Candidate Endangered | G2 | S2 |  |
| IIHYM72010 | Chrysis tularensis <br> Tulare cuckoo wasp | None | None | G1G2 | S2 |  |


| Element Code | Species | Federal Status | State Status | Global Rank | State Rank | Rare Plant Rank/CDFW SSC or FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IIPLE23020 | Cosumnoperla hypocrena <br> Cosumnes stripetail | None | None | G2 | S2 |  |
| ILARA14080 | Banksula rudolphi <br> Rudolph's cave harvestman | None | None | G1 | S1 |  |
| PDAPIOZOPO | Eryngium pinnatisectum Tuolumne button-celery | None | None | G2 | S2 | 1B. 2 |
| PDAST11061 | Balsamorhiza macrolepis big-scale balsamroot | None | None | G2 | S2 | 1B. 2 |
| PDCIS020F0 | Crocanthemum suffrutescens <br> Bisbee Peak rush-rose | None | None | G2?Q | S2? | 3.2 |
| PDERI04240 | Arctostaphylos myrtifolia lone manzanita | Threatened | None | G1 | S1 | 1B. 2 |
| PDONA05053 | Clarkia biloba ssp. brandegeeae <br> Brandegee's clarkia | None | None | G4G5T4 | S4 | 4.2 |
| PDPGN080F1 | Eriogonum apricum var. apricum Ione buckwheat | Endangered | Endangered | G2T1 | S1 | 1B. 1 |
| PDPGN080F2 | Eriogonum apricum var. prostratum Irish Hill buckwheat | Endangered | Endangered | G2T1 | S1 | 1 B .1 |
| PDPHR01130 | Erythranthe marmorata <br> Stanislaus monkeyflower | None | None | G2? | S2? | 1B. 1 |
| PDPLMOC0X1 | Navarretia myersii ssp. myersii pincushion navarretia | None | None | G2T2 | S2 | 1B. 1 |
| PDROSOWOC0 | Horkelia parryi Parry's horkelia | None | None | G2 | S2 | 1B. 2 |
| PMLIL0G020 | Chlorogalum grandiflorum <br> Red Hills soaproot | None | None | G3 | S3 | 1B. 2 |
| PMPOA5T030 | Sphenopholis obtusata prairie wedge grass | None | None | G5 | S2 | 2B. 2 |

## Search Results

23 matches found. Click on scientific name for details

Search Criteria: Quad is one of [3812058:3812057:3812056:3812048:3812046:3812038:3812037:3812036]

| - SCIENTIFIC Name | COMMON NAME | FAMILY | $\begin{aligned} & \text { FED } \\ & \text { LIST } \end{aligned}$ | STATE LIST | GLOBAL RANK | STATE <br> RANK | CA RARE PLANT RANK | OTHER STATUS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Arctostaphylos myrtifolia | Ione manzanita | Ericaceae | FT | None | G1 | S1 | 1 B .2 | SB_UCBG |
| Balsamorhiza macrolepis | big-scale balsamroot | Asteraceae | None | None | G2 | S2 | 1 B .2 | BLM_S; USFS_S |
| Bryum chryseum | brassy bryum | Bryaceae | None | None | G5 | S3 | 4.3 |  |
| Chlorogalum grandiflorum | Red Hills soaproot | Agavaceae | None | None | G3 | S3 | 1 B .2 | BLM_S; SB_SBBG |
| Clarkia biloba ssp. brandegeeae | Brandegee's clarkia | Onagraceae | None | None | G4G5T4 | S4 | 4.2 | SB_UCSC |
| Clarkia virgata | Sierra clarkia | Onagraceae | None | None | G3 | S3 | 4.3 | SB_CalBG/RSABG |
| Claytonia parviflora ssp. grandiflora | streambank spring beauty | Montiaceae | None | None | G5T3 | S3 | 4.2 |  |
| Crocanthemum suffrutescens | Bisbee Peak rush-rose | Cistaceae | None | None | G2?Q | S2? | 3.2 |  |
| Eriogonum apricum var. apricum | Ione buckwheat | Polygonaceae | FE | CE | G2T1 | S1 | 18. 1 | SB_UCBG |
| Eriogonum apricum var. prostratum | Irish Hill buckwheat | Polygonaceae | FE | CE | G2T1 | S1 | 18. 1 |  |
| Eriogonum tripodum | tripod buckwheat | Polygonaceae | None | None | G4 | S4 | 4.2 | USFS_S |
| Eriophyllum confertiflorum var. tanacetiflorum | tansy-flowered woolly sunflower | Asteraceae | None | None | G5T2?Q | S2? | 4.3 | SB_CalBG/RSABG |
| Eryngium pinnatisectum | Tuolumne buttoncelery | Apiaceae | None | None | G2 | S2 | 1B. 2 | SB_UCSC |
| Erythranthe inconspicua | small-flowered monkeyflower | Phrymaceae | None | None | G4 | S4 | 4.3 |  |
| Erythranthe marmorata | Stanislaus monkeyflower | Phrymaceae | None | None | G2? | S2? | 1B. 1 |  |
| Githopsis pulchella ssp. serpentinicola | serpentine bluecup | Campanulaceae | None | None | G4T3 | S3 | 4.3 |  |
| Horkelia parryi | Parry's horkelia | Rosaceae | None | None | G2 | S2 | 1B. 2 | BLM_S; USFS_S |
| Jepsonia heterandra | foothill jepsonia | Saxifragaceae | None | None | G3 | S3 | 4.3 |  |
| Lilium humboldtii ssp. <br> humboldtii | Humboldt lily | Liliaceae | None | None | G4T3 | S3 | 4.2 | SB_UCSC |
| Navarretia myersii ssp. myersii | pincushion navarretia | Polemoniaceae | None | None | G2T2 | S2 | 1B. 1 |  |
| Perideridia bacigalupii | Bacigalupi's yampah | Apiaceae | None | None | G3 | S3 | 4.2 |  |
| Sphenopholis obtusata | prairie wedge grass | Poaceae | None | None | G5 | S2 | 2B. 2 |  |
| Trichostema rubisepalum | Hernandez bluecurls | Lamiaceae | None | None | G4 | S4 | 4.3 | SB_CalBG/RSABG |

Showing 1 to 23 of 23 entries

## Suggested Citation:

California Native Plant Society, Rare Plant Program. 2023. Rare Plant Inventory (online edition, v9.5). Website https://www.rareplants.cnps.org [accessed 7 December 2023].

3

## National Wetlands Inventory

## Ione Band of Miwok



December 19, 2023

## Wetlands

Freshwater Emergent WetlandLake
$\square$ Other
Riverine

Estuarine and Marine DeepwaterEstuarine and Marine Wetland $\square$ Freshwater Forested/Shrub Wetland
Freshwater Pond

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should Wetlands Mapper web site.

## Appendix C <br> Preliminary Drainage Analysis

## TECHNICAL MEMORANDUM

TO: Jai Singh, PE
FROM: Donald Jones, PE
DATE: January 9, 2024
SUBJECT: Preliminary Drainage Analysis
PROJECT: Miwok Casino

## Project Description

This Technical Memorandum (TM) assesses the drainage effects of constructing a Casino Development on the east side of State Route 49 south of the City of Plymouth, California. This commercial facility will be located as shown in Figure 1, Site Plan. The project location drains primarily to the north where it is tributary to Little Indian Creek. The portion that currently drains southerly contributes to Dry Creek. The development of the Casino site will increase the amount of runoff moving both north to Little Indian Creek and south to Dry Creek. A large area west of SR 49 also contributes runoff to both the north and south.

The limits of the drainage areas were chosen to compare peak flows in both the existing, developed, and proposed conditions. The Existing Condition analysis includes establishing a "baseline" condition to determine peak flows leaving the project site and combining with other offsite areas. The Developed Condition scenario includes the proposed improvements to allow a comparison with the existing conditions. The Proposed Condition includes adding two stormwater treatment and detention ponds (extended detention) that will provide detention storage that reduce peak flows to less than the Existing Condition.

The intent of this memorandum is to detail the necessary improvements to mitigate increases in runoff due to the construction of the improvements necessary for the Casino. This includes verifying that the downstream hydraulic structures such as highway culverts are adequately sized to convey up to a 100-year peak flows. In addition, this report explores providing water quality treatment through post-construction Best Management Practices (BMP's).


Figure 1. Site Plan

## Hydrology

Figure 2, Existing Conditions Drainage Areas, shows the over 140-acre drainage area (project site) contributing to Little Indian Creek and the 8 acres contributing to Dry Creek. The development of the Casino site will increase the amount of runoff moving both north to Little Indian Creek and south to Dry Creek. A large area west of SR 49 also contributes runoff to both the north and south. As shown on Figure 2, Existing Conditions Drainage Areas, all subbasins flowing to Little Indian Creek are labeled 101, 102, 103, and 104. Those subbasins labeled 201, 202, and 203 flow south towards Dry Creek.

The drainage area delineation is based on a LiDAR dataset developed for the El Dorado National Forest in 2019 and made available by the United States Geologic Survey (USGS). This analysis is based on the horizontal datum of the California Coordinate System, Zone 2. The vertical datum used was the North American Vertical Datum of 1988 (NAVD 88).


Figure 2. Existing Conditions Drainage Areas
The hydrologic model developed for this analysis utilized the United States Natural Resource Conservation Service's (NRCS) Technical Release 55, Urban Hydrology for Small Watersheds, manual for determining runoff. The United States Corps of Engineers' Hydrologic Modeling System (HEC-HMS Version 4.11 Beta 16) software program was used to analyze the existing drainage watershed and the planned impacts from the proposed project. Rainfall depths were established based on the National Oceanic and Atmospheric Administration's (NOAA) Atlas 14 and the use of a SCS Type 1 rainfall distribution. Table 1, Rainfall Depths, shows the rainfall depths for return periods from 2-year to 100-year.

Table 1. Rainfall Depths

| Precipitation (in) |  |
| :---: | :---: |
| $100-\mathrm{yr} / 24-\mathrm{hr}$ | 5.53 |
| $50-\mathrm{yr} / 24-\mathrm{hr}$ | 5.02 |
| $25-\mathrm{yr} / 24-\mathrm{hr}$ | 4.51 |
| $10-\mathrm{yr} / 24-\mathrm{hr}$ | 3.83 |
| $2-\mathrm{yr} / 24-\mathrm{hr}$ | 2.68 |

Soils information was developed using the USGS Soil Survey website to determine hydrologic soil groups. Figure 3 shows the extent of soil types in the watershed. A composite runoff curve number (RCN) was chosen based on the hydrologic soils groups, vegetated cover type, and impervious surface amount.


Figure 3. Hydrologic Group Soils Map
The rainfall to runoff transformation was based on determining a lag time for each catchment and applying a USGS TR-55 standard unit hydrograph. A complete list of inputs for this analysis is included in Table 2, Existing Conditions Hydrologic Model Inputs.

Table 2. Existing Conditions Hydrologic Model Inputs

| Catchment | Area <br> (acres) | Land Use | Hydrologic Soil Group | \% Impervious | RCN | Lag Time <br> (Minutes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101 | 73.0 | Rural with some Highway Commercial | D | 2\% | 80 | 15.4 |
| 102 | 43.9 | Rural with some Highway Commercial | D | 8\% | 80 | 16.9 |
| 103 | 72.2 | Rural | D | 0\% | 80 | 14.9 |
| 104 | 53.0 | Rural with some Highway Commercial | D | 4\% | 80 | 24.3 |
| 201 | 7.5 | Rural with some Highway Commercial | D | 4\% | 80 | 11.3 |
| 202 | 14.5 | Rural with some Highway Commercial | D | 3\% | 80 | 8.8 |
| 203 | 9.1 | Rural | D | 0\% | 80 | 11.1 |

The existing conditions drainage catchments were updated to use in the Developed Conditions model as shown on Figure 4, Developed Conditions Drainage Areas.


Figure 4. Developed Conditions Drainage Areas
The existing conditions drainage catchments, impervious surface delineation, and lag times were then updated to use in the Developed conditions model as shown in Table 3, Developed Conditions Model Inputs.

Table 3. Developed Conditions Hydrologic Model Inputs

| Catchment | Area <br> (acres) | Land Use | Hydrologic <br> Soil Group | \% <br> Impervious | RCN | Lag Time |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (Minutes) |  |  |  |  |  |  |


| Catchment | Area <br> (acres) | Land Use | Hydrologic <br> Soil Group | \% <br> Impervious | RCN | Lag Time <br> (Minutes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 201 | 7.5 | Rural with some <br> Highway <br> Commercial | D | $4 \%$ | 80 | 11.3 |
| 202 A | 2.2 | Casino Site | D | $90 \%$ | 80 | 1.5 |
| $202 B$ | 12.1 | Rural with some <br> Highway <br> Commercial |  |  |  |  |
| 203 A | 1.4 | CasinoSite | D | $90 \%$ | 80 | 8.8 |
| $203 B$ | 8.5 | Rural | D | $0 \%$ | 80 | 1.4 |

The comparison of existing versus developed shows an increase in the peak, 100 -year events ranging from 3.0 cfs at the north end of the project (Junction 3) and 0.9 cfs at the south end of the project (Junction 2) as shown in Table 4, Hydrologic Model Results (without detention).

Table 4. Hydrologic Model Results (without detention)

| Results Comparison |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 10-Year |  | 100-Year |  |
| Hydrologic <br> Node | Existing | Developed | Existing | Developed |
| 101 | 29.7 | 29.7 | 56.1 | 56.1 |
| 102 | 18.8 | \#N/A | 34.5 | \#N/A |
| 102 A | \#N/A | 6.2 | \#N/A | 9.1 |
| $102 B$ | \#N/A | 15.5 | \#N/A | 28.5 |
| 103 | 29.0 | 29.0 | 55.3 | 55.3 |
| Junction-3 | 47.8 | 50.7 | 89.7 | 92.7 |
| Reach-1 | 29.6 | 29.6 | 55.8 | 55.8 |
| 104 | 19.6 | 19.6 | 36.7 | 36.7 |
| Junction-1 | 93.1 | 96.0 | 177.0 | 180.1 |
| 201 | 3.4 | 3.4 | 6.3 | 6.3 |
| 202 | 6.6 | \#N/A | 12.3 | \#N/A |
| $202 A$ | \#N/A | 1.7 | \#N/A | 2.5 |
| $202 B$ | \#N/A | 5.5 | \#N/A | 10.2 |
| 203 | 3.8 | \#N/A | 7.2 | \#N/A |
| $203 A$ | \#N/A | 1.1 | \#N/A | 1.7 |
| $203 B$ | \#N/A | 3.5 | \#N/A | 6.7 |
| Junction-2 | 13.7 | 14.7 | 25.8 | 26.7 |

Note: Highlighted cells indicate an increase in peak flow due to planned improvements

To reduce peak flows at Junctions 2 and 3 two multi-purpose stormwater ponds were added as shown on Figure 5, Proposed Improvements. Each pond has storage for water quality in the form of an extended detention pond. The remaining pond capacity will be used to attenuate peak flows to at or less than under Existing Conditions. Table 5, Stormwater Ponds Stage-Storage-Discharge Inputs shows each proposed pond's design data for inclusion in the hydrology model.

Table 5. Stormwater Ponds Stage-Storage-Discharge Inputs

| Proposed Stormwater Pond \#1 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation | Area |  | Volume | Cumulative Volume |  | Peak Out-Flow |
| (ft) NAVD88 | $\left(\mathrm{ft}^{2}\right)$ | (Acres) | $\left(\mathrm{ft}^{3}\right)$ | $\left(\mathrm{ft}^{3}\right)$ | (AcreFeet) | (cfs) |
| 1087 | 3,416 | 0.078 | - | - | 0.000 | 0.0 |
| 1088 | 4,982 | 0.114 | 4,199 | 4,199 | 0.096 | 0.0 |
| 1089 | 6,826 | 0.157 | 5,904 | 10,103 | 0.232 | 0.0 |
| 1090 | 8,943 | 0.205 | 7,885 | 17,987 | 0.413 | 0.0 |
| 1090.5 | 10,140 | 0.233 | 4,771 | 22,758 | 0.522 | 0.5 |
| 1091 | 11,337 | 0.260 | 5,369 | 28,127 | 0.646 | 2.0 |
| 1092 | 14,284 | 0.328 | 12,811 | 40,938 | 0.940 | 6.0 |
| Proposed Stormwater Pond \#2 |  |  |  |  |  |  |
| Elevation | Area |  | Volume | Cumulative Volume |  | Peak Out-Flow |
| (ft) NAVD88 | $\left(\mathrm{ft}^{2}\right)$ | (Acres) | $\left(\mathrm{ft}^{3}\right)$ | $\left(\mathrm{ft}^{3}\right)$ | (AcreFeet) | (cfs) |
| 1046 | 8,064 | 0.185 | - | - | 0.000 | 0.0 |
| 1047 | 9,550 | 0.219 | 8,807 | 8,807 | 0.202 | 0.0 |
| 1048 | 11,097 | 0.255 | 10,324 | 19,131 | 0.439 | 0.1 |
| 1049 | 12,707 | 0.292 | 11,902 | 31,033 | 0.712 | 0.2 |
| 1050 | 14,377 | 0.330 | 13,542 | 44,575 | 1.023 | 0.3 |
| 1051 | 16,109 | 0.370 | 15,243 | 59,818 | 1.373 | 0.4 |



Figure 5. Proposed Improvements
The proposed conditions peak flows are shown in Table 6, Peak Flow Comparison (with detention). The peaks have been reduced at Junctions 2 and 3 to at or less than the existing conditions peak flows. The location of these ponds is based on locating them as near to the project location a possible to more efficiently reduce downstream peaks and provide water quality benefits.

The northerly pond (Pond \#1) should be located at the northeast end of the site as shown in Figure 5, Proposed Improvements, which will place it near the receiving water body for the shed. The location is also best suited to avoid encroachment into adjacent wetlands. A storm drain pipe from the northeast corner of the site will convey drainage to the pond and will cross an existing wetland. To avoid disturbance of the wetland, the storm drain pipe should be bored underneath the wetlands. The pond is intended to be placed in excavation such that earthen berms are avoided. Should earthen berms be required, such embankments will be engineered in consultation with a Geotechnical Engineer.

The southerly pond (Pond \#2) will be located down-hill from the site as shown. This location may be challenging from a constructability standpoint due to difficulties posed by excavating through rock, the remoteness of the location, and steep topography of the general area. As noted in Figure 5, Proposed Improvements, on-site underground proprietary systems are a viable alternative.

Table 6. Peak Flow Comparison (with detention)

| Results Comparison |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 10-Year |  | 100-Year |  |
| Hydrologic <br> Node | Existing | Proposed | Existing | Proposed |
| 101 | 29.7 | 29.7 | 56.1 | 56.1 |
| 102 | 18.8 | \#N/A | 34.5 | \#N/A |
| $102 A$ | \#N/A | 6.2 | \#N/A | 9.1 |
| $102 B$ | \#N/A | 15.5 | \#N/A | 28.5 |
| 103 | 29.0 | 29.0 | 55.3 | 55.3 |
| Junction-3 | 47.8 | 47.1 | 89.7 | 87.8 |
| Reach-1 | 29.6 | 29.6 | 55.8 | 55.8 |
| 104 | 19.6 | 19.6 | 36.7 | 36.7 |
| Junction-1 | 93.1 | 92.9 | 177.0 | 175.6 |
| 201 | 3.4 | 3.4 | 6.3 | 6.3 |
| 202 | 6.6 | \#N/A | 12.3 | \#N/A |
| $202 A$ | \#N/A | 1.7 | \#N/A | 2.5 |
| $202 B$ | \#N/A | 5.5 | \#N/A | 10.2 |
| 203 | 3.8 | \#N/A | 7.2 | \#N/A |
| $203 A$ | \#N/A | 1.1 | \#N/A | 1.7 |
| $203 B$ | \#N/A | 3.5 | \#N/A | 6.7 |
| Junction-2 | 13.7 | 12.5 | 25.8 | 23.4 |

## Hydraulics

To evaluate the existing SR 49 culvert crossing at the north end of the property a hydraulic model was developed using the Corps of Engineers' Hydraulic Engineering Center River Analysis System (HEC-RAS Version 6.3.1) software. A one-dimensional, steady state model was developed using the topographic information from the USGS. The existing culvert crossing of SR 49 is comprised of three 36 -inch by 22 -inch corrugated metal arch culverts as shown in Figure 6, Existing Culvert Crossing. This plan was provided by Caltrans as an As-Built Drawing.


Figure 6. Existing Culvert Crossing
The existing culverts have the capacity to pass a 10-year event without overtopping the road, however, a 100year event would overtop the highway as shown on Figure 7, 100-Year Hydraulic Profile.


Figure 7. 100-Year Hydraulic Profile

## Stormwater Quality

Post construction BMP's have been included in this study to treat stormwater runoff prior to discharging downstream. Two extended detention ponds were chosen to both treat runoff and attenuate peak flows for both the north and south drainage areas. These extended detention ponds capture the water quality volume based on the 85th percentile, 24 -hour storm event (Water Quality event). The $85^{\text {th }}$ percentile rainfall depth used in this analysis for a 24-hour storm is 0.90 -inches per the State of California Water Quality Control Board's water quality website. This rainfall amount is based on the following gauge results:

Placerville rain gauge 1.13-inches
Sonora rain gauge site is 1.01 -inches
Sacramento rain gauge is 0.64 -inches
Lodi gauge shows 0.59 -inches
To provide water quality treatment of runoff leaving the site the two, multi-purpose stormwater ponds proposed provide enough capacity to allow the water quality volume to infiltrate. This required volume is shown in Table 7, Required Water Quality Volumes.

If Option B for Stormwater Pond \#2 is the chosen option, it will be an underground detention system where be the post stormwater quality may be achieved via proprietary stormwater quality devices. The final construction of the ponds or proprietary systems should be located at or near those locations shown on Figure 5, Proposed Improvements.

Table 7. Required Water Quality Volumes

| Stormwater <br> Pond \# | Contributing <br> Catchment (s) | Water Quality <br> Runoff Volume |
| :---: | :---: | :---: |
|  |  | (Acre-Feet) |
| 1 | 102 A | 0.5 |
| 2 | 202 A and 203A | 0.2 |

## Conclusions

The development of this Casino project will increase the volume and peak flow of runoff from the site. Currently, the existing culvert crossing of SR 49 near the north end of the project boundary does not have the capacity to convey the 100-year peak flow without overtopping the road. The culvert crossing has the capacity to safely pass an approximately 50-year peak flow.

The increase in runoff due to this development can be mitigated with detention storage. A 0.90-acre-foot multipurpose stormwater pond just north of the Casino will attenuate peak, 100-year flows to less than existing conditions. A 1.20-acre-foot multi-purpose stormwater pond is proposed south of the project that will reduce peak flows to less than existing conditions, assuring that downstream impacts from the project are mitigated.

## APPENDIX D

## Report for Water and Waste Water

## TECHNICAL MEMORANDUM

TO:
Jai Singh, PE - RSC Engineering, Inc.
FROM: Mike Massaro, PE
DATE: December 14, 2023-REVISED
SUBJECT: Basis of Design Report for Water and Wastewater Treatment
PROJECT: Ione Band of Miwok Indian's Casino and Hotel Project

## I. Project Background

This project was first conceptualized in 2005-2007 and an Environmental Impact Statement (EIS) was prepared. The EIS evaluated 5 alternatives of a project to develop a casino, hotel, and event center on Tribal land. Appendix B of the 2007 EIS titled "Water and Wastewater Feasibility Study for the lone Casino and Hotel Final Report" was completed by HydroScience Engineers, Inc. in July of 2005. This memorandum builds upon the analysis, evaluation, and assumptions of this prior report. Appendix $B$ of the original EIS is attached for reference.

Based on 2023 changes for the Casino development and updated flow demands provided by Cuningham, BEN|EN has updated treatment calculations, sizing, and cost estimates for revised water treatment, storage, and wastewater treatment facilities for the project.

The potable water demand is estimated at 22,463 gpd. Note that well capacity is not affirmed as part of this evaluation. On-site wells are currently being evaluated and rehabilitated for production and this analysis assumes the necessary demands will be met with on-site wells. Note also that the original EIS evaluates the use of recycled water to offset irrigation demands and for potential use in casino and hotel for non-potable demands. Recycled water is not evaluated for use or potable water offset in this analysis. Although the effluent water quality of Membrane Bio Reactor (MBR) systems allows opportunities for reuse and maximizing the amount of treated effluent for re-use (landscape irrigation, fodder crops, construction water/dust control) decreases the demand for effluent storage and disposal.

Wastewater treatment and disposal demand is estimated at a daily flow of 36,315 gpd for preliminary design purposes and evaluation of treatment facilities. This flow is estimated from return sewer flow from the casino + filter backwash flow from the water treatment facilities.

## II. Water Treatment and Storage

Based on the flow estimate of potable water demand $(22,463 \mathrm{gpd})$ and the water quality data provided from the 2004 well assessment and we recommend an Anthracite/Green Sand Filter followed by a Reverse Osmosis (RO) membrane filter for raw water treatment. This will be followed by a Chlorine injection system ( NaOCl hypochlorite) ahead of the water tank storage. Hypochlorite dosing will also be used ahead of a greensand filter to improve efficiency of the filter and reduce filter fouling. It is important to note that due to a typical 60\% throughput flow for RO treatment ( $40 \%$ sent to reject/concentrate waste), the raw water required from the wells on site will be 37,438 gpd to achieve the 22,463 gpd demanded by the Casino. Therefore, on-site well(s) will need to produce 26 gpm .
A. Storage

Based on a potable daily demand of $22,463 \mathrm{gpd}$, we would recommend a steel water tank that holds 90,000 gallons to support the casino. This would provide 4 days of water storage to support fire flow demands if wells or treatment system were off-line for any reason. Tank would be 30 - ft in diameter and $19-\mathrm{ft}$ tall. This sizing assumes 2 -ft of freeboard in the tank and no unusable space at the tank bottom because the water system plumbed to the tank would be gravity fed from the tank.

## B. Treatment

While not specifically measured in the water quality analysis, most groundwater wells in the region require treatment for Iron and Manganese. Treating these constituents will require an Anthracite and Green Sand filter system. These are supplied as a pressure filter and for the estimated potable water demand, the filter would be 40 -inches in diameter and 72 -inches tall and have a filter loading rate of $3 \mathrm{gpm} / \mathrm{SF}$ of filter. 2004 water quality data demonstrated some elevated levels of Total Dissolved Solids which would need to be removed via membranes for potable standards. A reverse osmosis (RO) system will remove TDS although less expensive systems like micro-filtration (MF) membranes can sometimes be applied instead of the higher energy demand RO systems. Updated water quality data from the on-site wells will help address the consistency of high TDS raw water and assist in the coordination with membrane system vendors to source the most economically appropriate system.
We evaluated the water quality data provided in 2023 and the older well data from 2004 to assess treatment requirements. The data is summarized below.

Table 1 - Water Quality Summary - Analytes Requiring Treatment for Potable Use

| Required treatment (2005) | Additional analytes <br> requiring treatment (2023) | Analytes that required treatment in <br> 2005 but do not require treatment in <br> 2023 |
| :--- | :---: | :---: |
| Cadmium | Antimony | Barium |
| Calcium | Beryllium | Copper |
| Chloride | Thallium | Fluoride |
| Magnesium |  |  |
| Potassium |  |  |
| Silver |  |  |
| Sodium |  |  |
| Specific Conductance |  |  |
| Sulfate as SO4 |  |  |
| Total Alkalinity |  |  |
| TDS |  |  |
| Total Sulfides |  |  |
| Zinc |  |  |
| Hardness as CaCO3 |  |  |
| Bicarbonate as CaCO3 |  |  |

Potential vendors of anthracite/green sand filters and skid mounted membrane filtration systems are: Pure Water Guys, Crystal Quest, Lenntech, Pure Aqua, Inc, among others. They sell complete packaged systems.

Note that the packaged wastewater treatment plant (WWTP) should be sited adjacent to the Potable Water treatment area and storage tank so that the backwash and reject water from the Greensand filter and RO treatment can be disposed of via the WWTP.

## III. Wastewater Treatment and Disposal

The loading assumptions from the 2005 study (EIS Appendix B) are still valid for the updated Casino Project. The anticipated flow rate of 36,315 gpd is consistent with other Casino developments that have effectively utilized packaged Membrane Bioreactor (MBR) systems for treatment and reuse. See section 5.2.2 of EIS Appendix B (attached for reference).

Treatment sizing and disposal estimates have been updated for the 2023 project. We are recommending a bermed equalization storage pond for the treated wastewater effluent. The geometry of the pond is adjustable to site impacts and availability, but it will need to store 8.53 MG . The pond surface area will be 5 acres in area.

Additional area will be required for berm volume and ramp access into and out of the pond. Based on these calculations the maximum pond depth will be 5.3 feet deep. Typically, 2-feet of freeboard is required to prevent sloshing due to wind, so the berms will need to be 7.5 feet tall. Typically, the pond will be lined to prevent infiltration. However, due to the high quality of the MBR effluent the EPA may grant a waiver to leave the pond un-lined and some infiltration would reduce storage and disposal demands.

We are also recommending 4 acres of irrigation field to be installed adjacent to the flow equalization pond. This will create a disposal pathway via infiltration and evapotranspiration. A $350 \mathrm{ft} \times 500 \mathrm{ft}$ irrigation field is assumed. This field will be plumbed to the effluent piping and storage pond for disposal of wastewater effluent. No flow would be sent to the irrigation field from November (or start of rainy season) until March. The irrigation field will receive flow from April to October from the treatment plant and the seasonally stored equalization pond.

The cost of these facilities is primarily site civil earthwork, pond lining, and piping, valves, gates, and turnouts for irrigation ditches on the irrigation field. This approach and these sizes of facilities will avoid the cost of sprayer systems. Although spray irrigation systems could be added to improve evapotranspiration during the dryer months to improve disposal efficiency.

Construction cost for equivalent sized packaged MBR systems (30,000-50,000 gpd) can range from $\$ 3.5$ to $\$ 5.0 \mathrm{M}$ in 2023. However, this cost would include all controls, buildings, site development, storage tanks (equalization and effluent storage for re-use), and subsurface disposal systems.

The 2004 Geotechnical Report demonstrated a wide variability in infiltration rates, making the effectiveness of subsurface infiltration difficult to predict. Fractured rock in the area created these inconsistencies. Therefore, the previous study utilized mostly spray field and evapotranspiration as the primary disposal method. Wet weather seasonal storage is required, because irrigation fields and spray fields cannot be utilized within 24hours of rainfall events. Contractor will acquire multiple subcontracted WWTP bids from various suppliers of packaged MBR systems (i.e., Evoqua, ClearLogic MBR, Titan MBR, and Ovivo).

Note that water and wastewater systems will require full time maintenance operators for monitoring, maintenance, and compliance sampling depending on EPA requirements for the systems and disposal methods included in the project.

Appendices:
Appendix A - Preliminary Opinion of Probable Construction Cost - Water System
Appendix B - Water and Wastewater Feasibility Study for the Ione Casino and Hotel - Final Report, HSe 2005
Appendix C - Wastewater Water Balance and Storage Calculations

## CALCULATIONS

Job No. 23-114
Project Miwok Casino Development
Subject Preliminary Wastewater Storage and Disposal Calculations
Calc. by M. Massaro $\quad$ Date $\quad \frac{12 / 13 / 2023}{12 / 14 / 2023}$
Chkd. By D. Harden Date $\quad \underline{12 / 14 / 2023}$


Notes
based on typical annual water use
Plymouth, CA Weather Station Information
CIMIS

Total field Area $\left(\mathrm{ft}^{2}\right)$

> 174,240
4.00

Table 3: Assimilitive Capacity: irrigation field

notes: 1) $\quad \mathrm{K}_{\mathrm{c}}$ coefficients for old field FAO-56 Crop Coefficients by Richard Allen

ETo is potential evapotranspiration
ET is the product of $K c$ and $E T o$
Average annual recurrance distributed monthly
Irrigation demand is ET-rainfall
Max. allowable applied percolation during Dec-March is the conductivity of non tilled clay loam soils ( $4^{*} 10^{-6} \mathrm{~cm} / \mathrm{d}$ ), as a conservative estimate. ( $0.136 \mathrm{in} / \mathrm{d}$ )
Assimilitive capacity is the sum of irrigation demand and percolation.
Volume estimates of capacity are based on the assimilative capacity by the acreage available for irrigation

Table 4 - Flow Equalization Pond Sizing using Average Annual Precipitation

| Month | $\begin{gathered} \text { Est } \\ \text { Ww }^{1} \\ \text { MG } \end{gathered}$ | Field Disposal capacity MG | Difference ww vs Disposal MG | Rainfall Contribution MG | Carryover Vol <br> w/o evap <br> MG | Pond Evap Losses MG | Pond Vol w/ evap MG | Pond Vol <br> w/ evap <br> ac-ft | Pond <br> Depth <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | 1.1 | 0.75 | 0.38 | 0.75 | 2.77 | 0.20 | 1.84 | 5.64 | 1.2 |
| Feb | 1.0 | 0.45 | 0.57 | 0.69 | 4.03 | 0.27 | 2.82 | 8.67 | 1.8 |
| Mar | 1.1 | 0.33 | 0.80 | 0.64 | 5.47 | 0.41 | 3.85 | 11.82 | 2.4 |
| Apr | 1.1 | 0.33 | 0.76 | 0.33 | 6.56 | 0.59 | 4.35 | 13.35 | 2.7 |
| May | 1.1 | 0.33 | 0.80 | 0.18 | 7.54 | 0.76 | 4.57 | 14.03 | 2.9 |
| Jun | 1.1 | 0.33 | 0.76 | 0.04 | 8.34 | 0.96 | 4.41 | 13.55 | 2.8 |
| Jul | 1.1 | 0.33 | 0.80 | 0.00 | 9.14 | 1.02 | 4.19 | 12.88 | 2.6 |
| Aug | 1.1 | 0.50 | 0.63 | 0.00 | 9.77 | 0.93 | 3.89 | 11.95 | 2.4 |
| Sep | 1.1 | 0.74 | 0.35 | 0.07 | 0.00 | 0.65 | 0.00 | 0.00 | 0.0 |
| Oct | 1.1 | 1.00 | 0.13 | 0.23 | 0.36 | 0.42 | 0.00 | 0.00 | 0.0 |
| Nov | 1.1 | 1.07 | 0.01 | 0.48 | 0.85 | 0.22 | 0.27 | 0.83 | 0.2 |
| Dec | 1.1 | 1.01 | 0.12 | 0.68 | 1.65 | 0.16 | 0.91 | 2.79 | 0.6 |
| Totals | 13.3 | 7.14 |  | 4.07 |  | 6.58 |  |  |  |
|  |  |  |  |  |  | Maximum: | 4.57 | 14.03 | 2.86 |
|  |  |  |  |  |  |  | MG | ac-ft | $f$ ft |
|  |  |  |  |  |  |  | Vol | Vol | Depth |

Table 5 - Flow Equalization Pond Sizing using 100-year Precipitation on Pond

| Month | $\begin{gathered} \text { Est } \\ \text { WW }{ }^{1} \\ \text { MG } \end{gathered}$ | Field Disposal capacity MG | Difference ww vs Disposal MG | Rainfall Contribution MG | Carryover Vol w/o evap MG | Pond Evap Losses MG | Pond Vol w/ evap MG | Pond Vol w/ evap ac-ft | $\begin{aligned} & \text { Pond } \\ & \text { Depth } \\ & \mathrm{ft} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan | 1.1 | 0.33 | 0.80 | 1.12 | 6.24 | 0.20 | 5.24 | 16.10 | 3.3 |
| Feb | 1.0 | 0.33 | 0.69 | 1.04 | 7.97 | 0.27 | 6.70 | 20.57 | 4.2 |
| Mar | 1.1 | 0.33 | 0.80 | 0.96 | 9.73 | 0.41 | 8.05 | 24.70 | 5.0 |
| Apr | 1.1 | 0.50 | 0.59 | 0.49 | 10.80 | 0.59 | 8.53 | 26.19 | 5.3 |
| May | 1.1 | 0.74 | 0.39 | 0.26 | 11.45 | 0.76 | 8.43 | 25.87 | 5.3 |
| Jun | 1.1 | 1.00 | 0.09 | 0.06 | 11.61 | 0.96 | 7.62 | 23.39 | 4.8 |
| Jul | 1.1 | 1.07 | 0.05 | 0.00 | 11.66 | 1.02 | 6.65 | 20.42 | 4.2 |
| Aug | 1.1 | 1.01 | 0.12 | 0.00 | 11.78 | 0.93 | 5.84 | 17.94 | 3.7 |
| Sep | 1.1 | 0.75 | 0.34 | 0.10 | 0.00 | 0.65 | 0.00 | 0.00 | 0.0 |
| Oct | 1.1 | 0.45 | 0.68 | 0.35 | 1.02 | 0.42 | 0.61 | 1.87 | 0.4 |
| Nov | 1.1 | 0.33 | 0.76 | 0.71 | 2.50 | 0.22 | 1.86 | 5.72 | 1.2 |
| Dec | 1.1 | 0.33 | 0.80 | 1.02 | 4.32 | 0.16 | 3.52 | 10.82 | 2.2 |
| Totals | 13.3 | 7.14 |  | 6.11 |  | 6.58 |  |  |  |
|  |  |  |  |  |  | Maximum: | 8.53 | 26.19 | 5.35 |
|  |  |  |  |  |  |  | MG | ac-ft | ft |
|  |  |  |  |  |  |  | Vol | Vol | Depth |

Table 1: Rainfall and avg ET, by month: Plymouth, CA

| month | Avg rainfall <br> (in) | 100-yr rainfall <br> (in) | percent | ET <br> (in) |
| :---: | :---: | :---: | :---: | :---: |
| Jan | 5.50 | 8.25 | $18.33 \%$ | 1.50 |
| Feb | 5.10 | 7.65 | $17.00 \%$ | 2.06 |
| Mar | 4.70 | 7.05 | $15.67 \%$ | 3.09 |
| Apr | 2.40 | 3.60 | $8.00 \%$ | 4.45 |
| May | 1.30 | 1.95 | $4.33 \%$ | 5.68 |
| Jun | 0.30 | 0.45 | $1.00 \%$ | 7.21 |
| Jul | 0.00 | 0.00 | $0.00 \%$ | 7.66 |
| Aug | 0.00 | 0.00 | $0.00 \%$ | 6.97 |
| Sep | 0.50 | 0.75 | $1.67 \%$ | 4.85 |
| Oct | 1.70 | 2.55 | $5.67 \%$ | 3.13 |
| Nov | 3.50 | 5.25 | $11.67 \%$ | 1.66 |
| Dec | 5.00 | 7.50 | $16.67 \%$ | 1.19 |
| total | 30.0 | 45.00 | $100 \%$ | 49.45 |

100-yr Multiplier =
1.5

## APPENDIX E

Transportation Impact Study


# Transportation Impact Study Ione Casino Project 

Amador County

Prepared by:
Abrams Associates
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# Ione Casino Project Amador County 

## TRANSPORTATION IMPACT STUDY

## 1) INTRODUCTION

This traffic impact study describes the existing and future conditions for transportation with and without the proposed Ione Casino Project in Amador County. The project would include the following components which would be constructed on the Tribe's Reservation, which is currently held in federal trust:

1) Construction of a casino with 25,200 square feet of gaming area.
2) Demolition of the existing Shenandoah Inn, which has 46 guest rooms.

This study also describes the regulatory setting; the criterion used for determining the significance of environmental impacts; and summarizes potential environmental impacts and appropriate mitigation measures. This study has been conducted in accordance with the requirements and methodologies set forth by Amador County, the City of Plymouth, and Caltrans. This report has been prepared to assess off-reservation impacts of the project in accordance with Appendix B of the Tribe's Tribal-State Compact.

Summary of Required Mitigations and Recommended Improvement Measures - The following is a summary of the proposed mitigation measures to address the transportation impacts of the project. Based on a detailed analysis of traffic operations with and without each of the proposed mitigations, implementation of the following mitigation measures would reduce some of the project impacts to a less-than-significant level.

Impact \#1 Impacts to Intersection Operations - The project would result in a significant contribution (greater than 5 seconds delay) to the LOS operations at two intersections that would exceed the established standards under future weekday and Friday conditions:

1) State Route 16 at Latrobe Road (Intersection \#9)
2) Golden Chain Highway (SR 49) and the Project Entrance (Intersection \#6) The addition of traffic from the proposed project would result in an increase in delay of more than five seconds to these two intersections that are forecast to
exceed the established LOS standards. Please note that one of the impacted intersections (Intersection \#6) is within the City of Plymouth. The following mitigation measures would be forecast to reduce the impacts to a less-thansignificant level in all of the plus project scenarios.

## Mitigation Measures

MM 1 (a) State Route 16 at Latrobe Road - Payment of a proportionate share of the cost to install a traffic signal, meeting the County's requirements. Using Caltrans' methodology and the volume forecasts in this TIS, the estimated proportional share contribution from the project for this improvement would be 55\%.

MM 1 (b) Golden Chain Highway (SR 49) at Village Drive (the proposed project entrance) - Widening of Village Drive to allow for separate right and left turn lanes on the westbound approach to SR 49 (i.e., two lanes for traffic exiting the project at $S R$ 49). With this improvement the intersection would meet the established standards with the proposed casino. Using Caltrans' methodology and the volume forecasts in this TIS, the estimated proportional share contribution from the project for this improvement would be 81\%.

## Impact \#2 Impacts related to site access and circulation.

The current plan to provide access to the site via the northern intersection of SR 49 with Village Drive could result in safety impacts due to potential conflicts in the two-way left turn lane with left turns into Randolph Drive. It is our understanding that with the addition of traffic from the proposed project this off-set configuration with the two-way left turn lane may no longer be acceptable to Caltrans.

Regardless of the location. the LOS analysis indicates the project's intersection with SR 49 will exceed the LOS standards under cumulative conditions if the project exit has only one lane on its approach to SR 49. Therefore, under any of the above access alternatives the recommended mitigation for cumulative plus project conditions described previously, MM 1(b), would also need to be implemented. No other site circulation or access issues have been identified that would cause a traffic safety problem or any unusual traffic congestion or delay. Detailed LOS calculations for each of the project entrances under all scenarios are included in the technical appendix.

## Mitigation Measure

MM 2 (a) Golden Chain Highway (SR 49) at Village Drive (the proposed project entrance) - Relocate the project access to one of two other recommended locations:

1) Line up the project entrance with Randolph Street.
2) Design the project access to connect only to the other (southern) intersection of Village Drive with SR 49.

## 2) PROJECT DESCRIPTION

As noted above, the project would include the following traffic-generating components:

1) Construction of a casino with 25,200 square feet of gaming.
2) Demolition of the existing Shenandoah Inn, which has 46 guest rooms.

All access to the project is currently proposed to occur via the existing intersection of Village Drive (north) with SR 49. Figure 1 shows the project location and the surrounding roadway network. Figures 2 presents the site plan for the project.

## 3) EXISTING CONDITIONS

This section of the report describes the roadways, traffic conditions and other existing transportation characteristics in the vicinity of the project. The primary basis of the analysis is the peak hour level of service for the key intersections. The hours identified as the "peak" hours are generally between 7:15 a.m. and 8:15 a.m. and 4:00 p.m. and 5:00 p.m. for the transportation facilities described, based on the intersection turning movement counts collected for this analysis. These peak hours will be identified as the AM and PM peak hours. These volumes represent the conditions on a typical weekday (Tuesday through Thursday). An analysis of project impacts on Friday evening traffic conditions is presented in Section 4.8.

The peak hour of casino traffic generally occurs after the PM peak hour of adjacent street traffic but to be conservative the analysis assumes the peak hour of casino traffic combined with the peak hour street traffic in the afternoon (4:00 p.m. and 5:00 p.m.) It should be noted that the final traffic study prepared for the previous casino proposal clearly indicated the Friday plus project scenario was the essentially the worst-case scenario at all of the project study intersections. ${ }^{1}$ Although the casino would generate slightly higher volumes on a Saturday afternoon, the Saturday afternoon background traffic is so much lower than Friday afternoon traffic that Saturday conditions come out substantially better than Friday conditions in all cases.

[^1]Therefore, the Friday analysis is considered the worst-case scenario and no additional useful information about the potential for project impacts would be anticipated even if additional analysis of Saturday afternoon conditions was conducted.

### 3.1 Project Study Intersections

Figure 1 shows the location of the project study intersections included in the analysis. As mentioned above, all access to the site would be via the northern Village Drive intersection with SR 49. Eleven study intersections were analyzed in this study.

### 3.2 Traffic Analysis Scenarios

The study intersections were evaluated for the six scenarios described below:

- Scenario 1: Existing Conditions - Level of Service (LOS) based on the existing weekday peak hour volumes and existing intersection configurations.
- Scenario 2: Existing Plus Project Conditions - Existing traffic volumes plus the trips forecast to be generated by the proposed project.
- Scenario 3: Baseline (No Project) Conditions - The Baseline scenario is based on the existing volumes plus growth in background traffic (for two years) plus the traffic from all reasonably foreseeable developments that could substantially affect the volumes at the project study intersections.
- Scenario 4: Baseline Plus Project Conditions - This scenario is based on the Baseline traffic volumes plus the trips from the proposed project.
- Scenario 5: Cumulative Conditions - This scenario includes year 2040 cumulative volumes based on planned and approved projects and the Amador County Travel Demand Model.
- Scenario 6: Cumulative Plus Project Conditions - This scenario includes year 2040 cumulative volumes based on the Amador County Travel Demand Model plus the forecast trips from proposed project.





### 3.3 Existing Roadway Network

As discussed previously, the project location and the surrounding roadway network are illustrated in Figure 1. The following is a more detailed description of some of the main roadways in the area that could be affected by the project:

- State Route 49 - State Route is a north-south primarily two-lane road extending nearly 300 miles between SR 70 in Plumas County to SR 41 in Oakhurst. The route serves residential and retail development and lacks curb, gutter, and sidewalk near the project site. SR 49 has a posted speed of 45 mph . In the vicinity of the project site, SR 49 has a center two-way left turn lane.
- Jackson Highway (SR 16) - Jackson Highway (SR 16) is a major arterial that traverses in the east-west direction, providing connection between Folsom Boulevard in the City of Sacramento and SR 49 in Amador County. Jackson Highway has two 12foot travel lanes with 8 -foot paved shoulders in the vicinity of the project site. The speed limit along Jackson Highway is posted at 55 miles per hour (mph).
- State Route 88 - State Route 88 (SR 88) begins in San Joaquin County at SR 99 and terminates at the California/Nevada border. In the vicinity of the project site, SR 88 is a two-lane conventional highway and is classified as a principal arterial. The posted speed limit is 55 mph . SR 88 also has paved shoulders on each side. A segment of SR 88 passing through the communities of Lockeford and Clemens is designated as both SR 88 and SR 12. The posted speed limit in these areas ranges from 25 to 40 mph . There is also a center two-way left-turn lane along SR 88 in Lockeford.
- State Route 124 - State Route 124 (SR 124) is a 2-lane rural road extending from SR 88 south of Ione to SR 49. It is also known as Church Street in the City of Ione and Plymouth Highway north of the City of Ione. Outside of the City of lone, it has a posted speed limit that varies from 55 to 65 mph .
- Grant Line Road - Grant Line Road is a 2-lane thoroughfare which begins at State Route 99 (SR 99) and continues in a northeast direction into the County of Sacramento where it terminates at White Rock Road. It has a full access interchange at SR 99. In the vicinity of the project site, Grant Line Road has two 12-foot travel lanes with 6-foot paved shoulders and a posted speed limit of 55 mph . The facility generally lacks curbs, gutters, and sidewalks.
- Latrobe Road - Latrobe Road (Amador County) is a 2-lane roadway which begins at SR 16 in Amador County and continues north into El Dorado County where it terminates with US 50. Latrobe Road provides access to rural residential areas in Amador County. North of US 50, Latrobe Road is also known as El Dorado Hills

Boulevard. It has a full access interchange with US 50.

- Main Street - Main Street is a 2-lane arterial in the City of Plymouth. It has a posted speed limit of 25 mph . It is also known as Shenandoah Road east of SR 49. The roadway primarily serves residential and retail development.
- Randolph Drive - Randolph Drive is a 2-lane roadway which begins at SR 49 and continues east until its terminus with Randolph Court. The main project driveway will become the fourth leg of its intersection with SR 49.
- Empire Drive - Empire Street is a 2-lane collector which runs between SR 49 and Church Street in the City of Plymouth. It has a posted speed limit of 25 mph . The roadway primarily serves residential development.
- Poplar Street - Poplar Street is a 2-lane collector which generally lacks curbs, gutters, and sidewalks. The roadway primarily serves residential development. The posted speed limit is 25 mph .
- Miller Way - Miller Way is a local roadway in the City of Plymouth. It is an east-west roadway which extends west from SR 49. The roadway has a speed limit of 25 mph .


### 3.4 Intersection Analysis Methodology

Existing operational conditions at the eleven (11) study intersections have been evaluated according to the requirements set forth by the Amador County and City of Plymouth General Plans. Analysis of traffic operations was conducted using the $6^{\text {th }}$ Edition of the Highway Capacity Manual (HCM) Level of Service (LOS) methodology with Synchro software. ${ }^{2}$ Level of service is an expression, in the form of a scale, of the relationship between the capacity of an intersection (or roadway segment) to accommodate the volume of traffic moving through it at any given time.

The level of service scale describes traffic flow with six ratings ranging from $A$ to $F$, with " $A$ " indicating relatively free flow of traffic and "F" indicating stop-and-go traffic characterized by traffic jams. As the amount of traffic moving through a given intersection or roadway segment increases, the traffic flow conditions that motorists experience rapidly deteriorate as the capacity of the intersection or roadway segment is reached. Under such conditions, there is general instability in the traffic flow, which means that relatively small incidents (e.g., momentary engine stall) can cause considerable fluctuations in speeds and delays that lead to traffic congestion. This near-capacity situation is labeled level of service (LOS) E. Beyond LOS E, the intersection or roadway segment capacity has been exceeded, and arriving traffic will generally exceed the ability of the intersection to accommodate it.

[^2]For signalized intersections, The HCM methodology determines the capacity of each lane group approaching the intersection. The LOS is then based on average control delay (in seconds per vehicle) for the various movements within the intersection. A combined weighted average control delay and LOS are presented for the intersection. A summary of the HCM results and copies of the detailed HCM LOS calculations are included in the appendix to this report. Table 1 summarizes the relationship between LOS, average control delay, and the volume to capacity ratio at signalized intersections. Table 2 summarizes the relationship between LOS and average control delay at unsignalized intersections.

For unsignalized intersections (all-way stop controlled and two-way stop controlled) the average control delay and LOS operating conditions are calculated by approach (e.g., northbound) and by movement (e.g., northbound left-turn) for those movements that are subject to delay. In general, the operating conditions for unsignalized intersections are presented for the worst approach.

### 3.5 Roadway Segment Analysis Methodology

Amador County has designated the Amador County Transportation Commission (ACTC) as the agency responsible for monitoring the network of key roadways that carry the majority of the County's traffic. This network, the Congestion Management Plan (CMP) network, was created to monitor roadway performance in relation to established level-of-service (LOS) standards and recommend improvement when LOS is found to be deficient. The Highway Capacity Manual's (HCM) recommended practice for evaluation of traffic operations on urban streets involves calculating free-flow speeds of the roadway and assigning a LOS.

Since study roadways are rural roadways the average daily traffic (ADT) conditions have been used as the operations measure to evaluate traffic operations along the roadways, consistent with the requirements of Amador and Sacramento Counties. Tables presenting the volume thresholds for road segment LOS in Amador County and Sacramento County that are applicable for the study roadway network are included in the technical appendix to this report.

Level of service is an expression, in the form of a scale, of the relationship between the capacity of a roadway segment to accommodate the volume of traffic moving through it at any given time. The level of service scale describes traffic flow with six ratings ranging from $A$ to $F$, with "A" indicating relatively free flow of traffic and " $F$ " indicating stop-and-go traffic characterized by traffic jams. As the amount of traffic moving through a given roadway segment increases, the traffic flow conditions that motorists experience rapidly deteriorate as the capacity of the roadway segment is reached.

| TABLE 1 <br> Signalized intersection Level of service definitions |  |  |  |
| :---: | :---: | :---: | :---: |
| Level of Service | Description of Operations | Average Delay (sec/veh) | Volume to Capacity Ratio |
| A | Insignificant Delays: No approach phase is fully used and no vehicle waits longer than one red indication. | $\leq 10$ | < 0.60 |
| B | Minimal Delays: An occasional approach phase is fully used. Drivers begin to feel restricted. | > 10 to 20 | > 0.61 to 0.70 |
| C | Acceptable Delays: Major approach phase may become fully used. Most drivers feel somewhat restricted. | > 20 to 35 | > 0.71 to 0.80 |
| D | Tolerable Delays: Drivers may wait through no more than one red indication. Queues may develop but dissipate rapidly without excessive delays. | > 35 to 55 | > 0.81 to 0.90 |
| E | Significant Delays: Volumes approaching capacity. Vehicles may wait through several signal cycles and long vehicle queues from upstream. | > 55 to 80 | > 0.91 to 1.00 |
| F | Excessive Delays: Represents conditions at capacity, with extremely long delays. Queues may block upstream intersections. | $>80$ | > 1.00 |
| SOURCES: $6^{\text {th }}$ Edition of the Highway Capacity Manual, Transportation Research Board, 2016. |  |  |  |


| TABLE 2 <br> UNSIGNALIZED INTERSECTION LEVEL OF SERVICE DEFINITIONS |  |  |
| :---: | :---: | :---: |
| Level of Service | Description of Operations | Average Delay (seconds/vehicle) |
| A | No delay for stop-controlled approaches. | 0 to 10 |
| B | Operations with minor delays. | $>10$ to 15 |
| C | Operations with moderate delays. | $>15$ to 25 |
| D | Operations with some delays. | $>25$ to 35 |
| E | Operations with high delays and long queues. | $>35$ to 50 |
| F | Operation with extreme congestion, with very high delays and long queues unacceptable to most drivers. | > 50 |
| SOURCE: 6 $^{\text {th }}$ Edition of the Highway Capacity Manual, Transportation Research Board, 2016. |  |  |

### 3.6 Existing Intersection Capacity Conditions (Scenario 1)

The existing intersection geometry at each of the project study intersections can be seen in Figure 3 and the existing traffic volumes at each are presented in Figure 4. Traffic counts at the study intersections were conducted in May of 2023 at times when local schools were in session. Table 3 summarizes the associated LOS computation results for the existing weekday AM and PM peak hour conditions. Please note that the corresponding LOS analysis calculation sheets are presented in the appendix to this report. As shown in Table 3, all of the project study intersections currently have acceptable conditions (LOS D or better) during the weekday AM and PM peak hours, with the exception of Jackson Road (SR 16) at Grant Line Road, which would operate at LOS E in the AM peak hour and LOS in the PM peak hour. See Section 3.8 for a description of the applicable intersection thresholds.

### 3.7 Pedestrian and Bicycle Facilities

Bicycle and pedestrian facilities in the project study area are currently very limited with no bike lanes or sidewalks provided in the vicinity of the project. Bicycle paths, lanes and routes are typical examples of bicycle transportation facilities, which are defined by Caltrans as being in one of the four classes:

Class I - Provides a completely separated facility designed for the exclusive use of bicyclists and pedestrians with crossing points minimized.
Class II - Provides a restricted right-of-way designated lane for the exclusive or semi-exclusive use of bicycles with through travel by motor vehicles or pedestrians prohibited, but with vehicle parking and cross-flows by pedestrians and motorists permitted.
Class III - Provides a route designated by signs or permanent markings and shared with pedestrians and motorists.
Class IV - Provides an adjacent bike lane or bikeway that is physically separated from motor vehicle traffic.

Field observations indicate that walking and bicycling activity is limited in the immediate vicinity of the proposed project site. This is primarily due to the lack of existing bicycle and pedestrian traffic generators in the vicinity of the project site. However, there is a lack of curbs, gutters, and sidewalks along SR 49 to accommodate pedestrian activity. On most of the roadways in the study area, bicyclists must ride in the roadway and share the travel lane with vehicular traffic.

### 3.7 Transit Service

Bus Transit - Bus transit service in the project area is provided by Amador Transit. Amador Transit operates local bus route 3 within the City of Plymouth. The route operates twice a day with stops near the project site Monday through Friday from about 8:30 AM to 4:00 PM. Limited Saturday service is also offered. The routes provide connections to regional transit via intercity routes 1,2 , and 7 . The nearest bus stops to the project are located adjacent to the site at the intersection of Village Drive at SR 49.





[^3]TABLE 3
EXISTING INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | PEAK HOUR | EXISting |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | LOS |
| 1 | GOLDEN CHAIN HWY (SR-49) \& MILLER WAY |  | Side Street Stop | AM | 9.0 | A |
|  |  | PM |  | 9.1 | A |
| 2 | GOLDEN CHAIN HWY (SR-49) \& MAIN STREET | Roundabout | AM | 4.4 | A |
|  |  |  | PM | 4.9 | A |
| 3 | GOLDEN CHAIN HWY (SR-49) \& POPLAR STREET | Side Street Stop | AM | 10.0 | B |
|  |  |  | PM | 10.1 | B |
| 4 | GOLDEN CHAIN HWY (SR-49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | AM | 15.9 | C |
|  |  |  | PM | 14.8 | B |
| 5 | GOLDEN CHAIN HWY (SR-49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | AM | 12.1 | B |
|  |  |  | PM | 13.0 | B |
| 6 | GOLDEN CHAIN HIGHWAY (SR-49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street Stop | AM | 13.5 | B |
|  |  |  | PM | 15.7 | C |
| 7 | GOLDEN CHAIN HIGHWAY (SR-49) \& SR-16 | Signalized | AM | 11.9 | B |
|  |  |  | PM | 11.9 | B |
| 8 | SR-16 \& PLYMOUTH HIGHWAY (SR-124) | Side Street Stop | AM | 12.6 | B |
|  |  |  | PM | 14.5 | B |
| 9 | SR-16 \& LATROBE ROAD | Side Street Stop | AM | 15.2 | C |
|  |  |  | PM | 19.7 | C |
| 10 | JACKSON ROAD (SR-16) \& IONE ROAD | Side Street Stop | AM | 15.2 | C |
|  |  |  | PM | 17.4 | C |
| 11 | JACKSON ROAD (SR-16) \& GRANT LINE ROAD | Signalized | AM | 57.9 | E |
|  |  |  | PM | 77.5 | E |

SOURCE: Abrams Associates, 2023
NOTE: Delay results are presented in terms of seconds per vehicle.

### 3.8 Standards and Objectives

Existing policies, laws and regulations that apply to the proposed project are summarized below.
Tribal-State Compact - The Tribal-State Compact Between the State of California and the lone Band of Miwok Indians specifies that a Mitigated Negative Declaration shall include: "a description of proposed mitigation measures included in the Project to reduce the potential Significant Effects on the Off-Reservation Environment to a less-than-significant level; and The Tribe's commitment to enter into an enforceable binding letter agreement with the State under which the Tribe shall agree to perform the required mitigation."

Caltrans - The California Department of Transportation (Caltrans) has jurisdiction over State highways. Therefore, Caltrans controls all construction, modification, and maintenance of State highways, such as U.S. 101. Any improvements to these roadways would require Caltrans' approval.

Amador County General Plan - The Transportation and Circulation Element included in the Amador County General Plan was prepared pursuant to Section 65302(b) of the California Government Code. The Transportation and Circulation Element addresses the location and
extent of existing and planned transportation routes, terminals, and other local public utilities and facilities. The General Plan identifies roadway and transit goals and policies that have been adopted to ensure that the transportation system of the County will have adequate capacity to serve planned growth. These goals and policies are intended to provide a plan and implementation measures for an integrated, multi-modal transportation system that will safely and efficiently meet the transportation needs of all economic and social segments of the County.

City of Plymouth General Plan - The Circulation Element included in the City of Plymouth General also identifies roadway and transit goals and policies that have been adopted to ensure that the transportation system of the City will continue to have adequate capacity to serve planned growth.

Significance Criteria - For the purposes of this analysis a project would have a significant impact if it would:

- Conflict with an applicable program, plan, ordinance or policy establishing measures of effectiveness for the performance of addressing the circulation system, including transit, roadways, bicycle lanes and pedestrian facilities/paths?

The goal of Amador County is to maintain a Level of Service (LOS) C during the peak hours, while the goal of the City of Plymouth and Sacramento County is to maintain a Level of Service (LOS) D during the peak hours. The County does not have plans, ordinances, or policies establishing measures of effectiveness for the performance of other parts of its circulation system. The applicable measures of effectiveness are summarized below:

Signalized Intersections - Project-related operational impacts on the signalized study intersections in the Amador County are considered significant if project-related traffic causes the Level of Service (LOS) rating to deteriorate from LOS C to LOS D, E or F. In addition, in Amador County project impacts are also considered significant if a roadway or signalized intersection already exceeds the standards without project trips, and the project causes the average delay to increase by five seconds or more. Project-related operational impacts on signalized study intersections in the Sacramento County are considered significant if project-related traffic causes the Level of Service (LOS) rating to deteriorate from LOS D to LOS E, or F. In Sacramento County project impacts are also considered significant if a roadway or signalized intersection already exceeds the standards without project trips, and the project causes the volume to capacity (V/C) ratio to increase by more that 0.05 .

Unsignalized Intersections - Project-related operational impacts on unsignalized intersections in Amador County are considered significant if project generated traffic causes a movement/approach to deteriorate from LOS C or better to LOS D, E or F. In Sacramento County impacts are considered significant if project generated traffic causes a movement/approach to deteriorate from LOS D or better to LOS E or F. For unsignalized intersections where the LOS would already exceed Amador County or

Sacramento County standards it is considered a significant impact if the project increases the delay by more than 5 seconds.

- Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the off-reservation circulation system, taking into account all modes of transportation including mass transit and nonmotorized travel and relevant components of the circulation system, including, but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit?
- Conflict with an applicable congestion management program, including, but not limited to, level of service standards and travel demand measures, or other standards established by the county congestion management agency for designated offreservation roads or highways?
- Substantially increase hazards to an off-reservation design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)?
- Result in inadequate emergency access for off-reservation responders?


## 4) TRANSPORTATION IMPACT ANALYSIS

### 4.1 Project Trip Generation

Casino Trip Generation - The peak-hour trip generation of the proposed casino was reviewed based on information published in Institute of Transportation Engineers (ITE) Trip Generation Manual (Eleventh Edition, 2021). The trip generation forecasts include all traffic in and out of the site including patrons, employees, vendors, and deliveries. The trip generation forecasts are presented below in Table 4.

TABLE 4
PROJECT TRIP GENERATION CALCULATIONS

| Land Use | Size | ADT | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Indian Casino Trip Rates Trips per Square Feet |  | 98.21 | 1.78 | 1.64 | 3.42 | 3.10 | 3.64 | 6.74 |
| Proposed Casino Expansion Trip Generation | $\begin{aligned} & \text { 25,200 } \\ & \text { sq. ft. } \end{aligned}$ | 2,475 | 45 | 41 | 86 | 78 | 92 | 170 |
| ITE Hotel Trip Rates - Trips per Room |  | 7.99 | 0.26 | 0.20 | 0.46 | 0.30 | 0.29 | 0.59 |
| Shenandoah Inn Trip Generation (To be demolished) | 46 rooms | 368 | 12 | 9 | 21 | 14 | 13 | 27 |
| Net New Project Trip Generation |  | 2,108 | 33 | 32 | 65 | 64 | 79 | 143 |

As described below, more recent trip generation data is available from surveys of existing Indian casinos, and this data was used to estimate the traffic that would be produced by the project. The ITE Trip Generation Manual is generally the standard reference from which to determine trip generation rates. However, the rates for a casino included in the latest edition of the ITE Trip Generation Manual are based on surveys of six casino/video lottery establishments taken in South Dakota in the 1990's. The square footages of the surveyed facilities ranged from 600 to 2,400 square feet. Based on preliminary calculations and a comparison of this rate with other studies (described below) it was found that use of the ITE rate produced results that did not compare with the expected traffic of the proposed project. This was verified based on trip generation surveys conducted at the Graton Resort \& Casino.

The approach used for establishing trip generation rates for the casino was to investigate trip generation characteristics at other similar casinos based on the results of trip generation surveys and validate the results with traffic counts taken at other existing casinos. For this project additional data on casino trip generation rates were obtained from the transportation
impact analysis prepared for the Tejon Casino in Kern County. ${ }^{3}$ The trip generation rates were based on the average of the traffic surveys conducted at three similar Indian casinos as part of the Tejon Casino Transportation Impact Analysis. This document includes extensive discussions on the research performed to determine an appropriate trip generation rate for Indian gaming facilities and on the actually developed trip rates for weekday daily, AM and PM peak of the street, as well as Saturday peak hour of the generator conditions. A review of other more recent casino traffic impact studies indicates this data can still be considered conservative. Traffic from the existing 46-room Shenandoah Inn (to be demolished) was subtracted from the casino trip generation. During the normal weekday commute peak hours the project is estimated to generate a total of approximately 65 AM peak hour trips ( 33 inbound and 32 outbound) and 143 PM peak hour trips (64 inbound and 78 outbound).

### 4.2 Project Trip Distribution

The trip distribution assumptions have been based on the project's proximity to the access freeway and other key travel routes in Amador County, the existing directional split at nearby intersections, and the overall land use patterns in the area. Figure 5 shows the project trips that would be added at the study intersections.

### 4.3 Existing Plus Project Traffic Capacity Conditions (Scenario 2)

This scenario evaluates the existing conditions with the addition of traffic from the proposed project. The traffic volumes for each of the study intersections for Existing Plus Project conditions are shown in Figure 6. The capacity calculations for the Existing Plus Project scenario are shown in Table 5. The corresponding LOS analysis calculation sheets are presented in the appendix to this report. The proposed project access would be via Village Drive at Intersection \#6. Village Drive is currently has one lane in each direction with side street stop control at its intersection with State Route 49 (Golden Chain Highway). Village Drive currently has 15 foot lanes in the vicinity of State Route 49. Based on the existing and forecast volumes, Section 301.1. of Caltrans' Highway Design Manual specifies that the minimum lane width for Village Drive is 11 feet and the minimum lane width for State Route 49 is 12 feet.

As shown in Table 5, all of the project study intersections would continue to have acceptable conditions (LOS D or better) during the weekday AM and PM peak hours with the exception all of the project study intersections currently have acceptable conditions (LOS D or better) during the weekday AM and PM peak hours, with the exception of Jackson Road (SR 16) at Grant Line Road and also the main project entrance intersection (Village Drive) with State Route 49. The intersection of Jackson Road (SR 16) and Grant Line Road is forecast to exceed the LOS standards regardless of whether or not the proposed project is implemented and the project would not increase the average delay by more than five seconds per vehicle.

[^4]



FIGURE 6B | EXISTING PLUS PROJECT WEEKDAY AM(PM) PEAK HOUR TRAFFIC VOLUMES TRANSPORTATION IMPACT STUDY
Ione Casino Project
Amador County

TABLE 5
EXISTING PLUS PROJECT INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | PEAK HOUR | EXISTING |  | EXISTING PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | LOS | Delay | LOS |
| 1 | GOLDEN CHAIN HWY (SR-49) \& MILLER WAY |  | $\begin{gathered} \text { Side Street } \\ \text { Stop } \\ \hline \end{gathered}$ | AM | 9.0 | A | 9.0 | A |
|  |  | PM |  | 9.1 | A | 9.2 | A |
| 2 | GOLDEN CHAIN HWY (SR-49) \& MAIN STREET | Roundabout | AM | 4.4 | A | 4.4 | A |
|  |  |  | PM | 4.9 | A | 5.1 | A |
| 3 | GOLDEN CHAIN HWY (SR-49) \& POPLAR STREET | Side Street Stop | AM | 10.0 | B | 10.1 | B |
|  |  |  | PM | 10.1 | B | 10.2 | B |
| 4 | GOLDEN CHAIN HWY (SR-49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | AM | 15.9 | C | 16.2 | C |
|  |  |  | PM | 14.8 | B | 15.4 | C |
| 5 | GOLDEN CHAIN HWY (SR-49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | AM | 12.1 | B | 12.3 | B |
|  |  |  | PM | 13.0 | B | 13.4 | B |
| 6 | GOLDEN CHAIN HIGHWAY (SR-49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | $\begin{gathered} \hline \text { Side Street } \\ \text { Stop } \\ \hline \end{gathered}$ | AM | 13.5 | B | 14.5 | B |
|  |  |  | PM | 15.7 | C | 18.1 | C |
| 7 | GOLDEN CHAIN HIGHWAY (SR-49) \& SR-16 | Signalized | AM | 11.9 | B | 11.9 | B |
|  |  |  | PM | 11.9 | B | 12.0 | B |
| 8 | SR-16 \& PLYMOUTH HIGHWAY (SR-124) | $\begin{gathered} \hline \text { Side Street } \\ \text { Stop } \\ \hline \end{gathered}$ | AM | 12.6 | B | 12.8 | B |
|  |  |  | PM | 14.5 | B | 15.5 | C |
| 9 | SR-16 \& LATROBE ROAD | $\begin{gathered} \text { Side Street } \\ \text { Stop } \\ \hline \end{gathered}$ | AM | 15.2 | C | 15.7 | C |
|  |  |  | PM | 19.7 | C | 22.1 | C |
| 10 | JACKSON ROAD (SR-16) \& IONE ROAD | Side Street Stop | AM | 15.2 | C | 15.6 | C |
|  |  |  | PM | 17.4 | C | 18.6 | C |
| 11 | JACKSON ROAD (SR-16) \& GRANT LINE ROAD | Signalized | AM | 57.9 | E | 59.0 | E |
|  |  |  | PM | 77.5 | E | >80.0 | F |

SOURCE: Abrams Associates, 2023
NOTE: Delay results are presented in terms of seconds per vehicle.

### 4.4 Baseline Traffic Capacity Conditions (Scenario 3)

The Baseline scenario evaluates the existing conditions with the addition of traffic from reasonably foreseeable projects in the area and general baseline growth in traffic. For this analysis the baseline volumes were developed based on the assumption that the project completion date would be 2025 with a 1\% per year growth in background traffic plus the addition of traffic from approved projects. The trip generation for the approved and/or reasonably foreseeable projects was derived from the Putnam Ranch Draft Transportation Analysis Report. ${ }^{4}$ The five projects include Putnam Ranch, Zinfandel Ridge, Shenandoah Ridge, the Greilich Ranch Subdivision, and the 49er RV Park Expansion. The traffic volumes for each of the study intersections for the Baseline scenario are shown in Figure 7. Table 6 summarizes the associated LOS computation results for the Baseline weekday AM and PM peak hour conditions. As shown in Table 6, all of the study intersections would continue to have acceptable conditions under the Baseline scenario during the weekday AM and PM peak hours, with the exception of Jackson
Road (SR 16) at Grant Line Road which would operate at LOS E in the AM and PM peak hours.

[^5]


TABLE 6
bASELINE PLUS PROJECT INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | PEAK HOUR | BASELINE |  | BASELINE PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | LOS | Delay | LOS |
| 1 | GOLDEN CHAIN HWY (SR-49) \& MILLER WAY |  | Side Street Stop | AM | 9.3 | A | 9.3 | A |
|  |  | PM |  | 9.4 | A | 9.5 | A |
| 2 | GOLDEN CHAIN HWY (SR-49) \& MAIN STREET | Roundabout | AM | 4.9 | A | 5.0 | A |
|  |  |  | PM | 5.7 | A | 5.9 | A |
| 3 | GOLDEN CHAIN HWY (SR-49) \& POPLAR STREET | Side Street Stop | AM | 10.6 | B | 10.7 | B |
|  |  |  | PM | 10.9 | B | 11.0 | B |
| 4 | GOLDEN CHAIN HWY (SR-49) \& PACIFIC STREET / EMPIRE STREET | $\begin{aligned} & \text { Side Street } \\ & \text { Stop } \end{aligned}$ | AM | 19.5 | C | 20.0 | C |
|  |  |  | PM | 18.2 | C | 19.0 | C |
| 5 | GOLDEN CHAIN HWY (SR-49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | AM | 14.5 | B | 14.8 | B |
|  |  |  | PM | 16.8 | C | 17.5 | C |
| 6 | GOLDEN CHAIN HIGHWAY (SR-49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street | AM | 18.0 | C | 19.6 | C |
|  |  |  | PM | 24.1 | C | 32.4 | D |
| 7 | GOLDEN CHAIN HIGHWAY (SR-49) \& SR-16 | Signalized | AM | 19.2 | B | 19.6 | B |
|  |  |  | PM | 19.7 | B | 20.2 | C |
| 8 | SR-16 \& PLYMOUTH HIGHWAY (SR-124) | Side StreetStop | AM | 13.8 | B | 14.1 | B |
|  |  |  | PM | 17.2 | C | 18.6 | C |
| 9 | SR-16 \& LATROBE ROAD | Side Street Stop | AM | 17.8 | C | 18.6 | C |
|  |  |  | PM | 29.2 | D | 34.7 | D |
| 10 | JACKSON ROAD (SR-16) \& IONE ROAD | Side Street Stop | AM | 16.9 | C | 17.4 | C |
|  |  |  | PM | 20.3 | C | 21.7 | C |
| 11 | JACKSON ROAD (SR-16) \& GRANT LINE ROAD | Signalized | AM | 68.1 | E | 69.7 | E |
|  |  |  | PM | >80.0 | F | >80.0 | F |

SOURCE: Abrams Associates, 2020
NOTE: Delay results are presented in terms of seconds per vehicle.

### 4.5 Baseline Plus Project Traffic Capacity Conditions (Scenario 4)

The Baseline plus proposed project traffic forecasts were developed by adding traffic from the project to the baseline traffic volumes. The traffic volumes for each of the study intersections for the Baseline Plus Project scenario are shown in Figure 8. Table 6 summarizes the LOS results for the Baseline and Baseline Plus Project weekday AM and PM peak hour conditions. The corresponding LOS analysis calculation sheets are presented in the appendix to this report. As shown in Table 6, all of the study intersections would continue to have acceptable conditions under the Baseline Plus Project scenario during the weekday AM and PM peak hours, with the exception of Jackson Road (SR 16) at Grant Line Road. The intersection of Jackson Road (SR 16) and Grant Line Road is forecast to exceed the LOS standards regardless of whether or not the proposed project is implemented and the project would not increase the average delay by more than five seconds per vehicle. Mitigations to improve the operations at these intersections are discussed in Section 5.



### 4.6 Cumulative Traffic Capacity Conditions (Scenario 5)

For the cumulative conditions, the intersection traffic volumes were based on the existing turning movements plus incremental growth of $0.5 \%$ per year in background traffic based on the Amador County Travel Demand Model. In addition to background growth, this scenario includes traffic from the following five projects: Putnam Ranch, Zinfandel Ridge, Shenandoah Ridge, the Greilich Ranch Subdivision, and the 49er RV Park Expansion. This scenario also includes the planned widening of Grant Line Road to four lanes. Figure 9 presents the cumulative build-out traffic volumes for the project study intersections. Table 7 summarizes the LOS results for the Cumulative (Year 2040) traffic conditions at each of the project study intersections. As shown on this table, the project study intersections would be forecast to continue to have acceptable conditions during the weekday AM and PM peak commute hours, with the exception of the intersection of SR 16 with Latrobe Road. There are planned left turn lanes identified for this intersection in the Amador County Regional Traffic Mitigation Fee Project List. However, even assuming the additional left turn lanes this intersection is still forecast to operate at LOS E in the PM peak hour.

TABLE 7
CUMULATIVE PLUS PROJECT INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | PEAK HOUR | CUMULATIVE |  | CUMULATIVE PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | LOS | Delay | LOS |
| 1 | GOLDEN CHAIN HWY (SR-49) \& MILLER WAY |  | Side Street Stop | AM | 9.3 | A | 9.4 | A |
|  |  | PM |  | 9.5 | A | 9.6 | A |
| 2 | GOLDEN CHAIN HWY (SR-49) \& MAIN STREET | Roundabout | AM | 5.1 | A | 5.2 | A |
|  |  |  | PM | 6.0 | A | 6.2 | A |
| 3 | GOLDEN CHAIN HWY (SR-49) \& POPLAR STREET | Side Street Stop | AM | 10.9 | B | 11.0 | B |
|  |  |  | PM | 11.1 | B | 11.3 | B |
| 4 | GOLDEN CHAIN HWY (SR-49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | AM | 21.5 | C | 22.1 | C |
|  |  |  | PM | 19.9 | C | 20.9 | C |
| 5 | GOLDEN CHAIN HWY (SR-49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | AM | 15.6 | C | 15.9 | C |
|  |  |  | PM | 18.4 | C | 19.4 | C |
| 6 | GOLDEN CHAIN HIGHWAY (SR-49) \& VILLAGE DRIVE | Side Street Stop | AM | 19.8 | C | 21.6 | C |
|  |  |  | PM | 27.9 | D | 40.0 | E |
| 7 | GOLDEN CHAIN HIGHWAY (SR-49) \& SR-16 | Signalized | AM | 20.4 | C | 20.9 | C |
|  |  |  | PM | 21.1 | C | 21.8 | C |
| 8 | SR-16 \& PLYMOUTH HIGHWAY (SR-124) | Side Street Stop | AM | 14.8 | B | 15.1 | C |
|  |  |  | PM | 19.0 | C | 21.0 | C |
| 9 | SR-16 \& LATROBE ROAD | Side Street Stop | AM | 19.7 | C | 20.6 | C |
|  |  |  | PM | 38.6 | E | 48.4 | E |
| 10 | JACKSON ROAD (SR-16) \& IONE ROAD | Side Street Stop | AM | 18.7 | C | 19.3 | C |
|  |  |  | PM | 23.3 | C | 25.2 | D |
| 11 | JACKSON ROAD (SR-16) \& GRANT LINE ROAD | Signalized | AM | 25.5 | C | 25.7 | C |
|  |  |  | PM | 24.5 | C | 25.0 | C |

SOURCE: Abrams Associates, 2023
NOTE: Delay results are presented in terms of seconds per vehicle.



[^6]

FIGURE 10A | CUMULATIVE PLUS PROJECT WEEKDAY AM(PM) PEAK HOUR TRAFFIC VOLUMES TRANSPORTATION IMPACT STUDY


### 4.7 Cumulative Plus Project Traffic Capacity Conditions (Scenario 6)

Table 7 summarizes the LOS results for the Cumulative Plus Project (Year 2040) traffic conditions at each of the project study intersection. Figure 10 presents the cumulative build-out traffic volumes including the traffic from the proposed project. As shown on this table, all of the signalized study intersections would continue to have acceptable conditions during the weekday peak hours, with the exception of the intersection of SR 16 with Latrobe Road and also Golden Chain Highway (SR 49) with Village Drive (the proposed project entrance). Mitigations to improve the operations at these intersections are discussed in Section 5.

### 4.8 Friday Evening Cumulative Traffic Capacity Conditions

Traffic counts at all of the project study intersections were conducted on Friday, May $12^{\text {th }}, 2023$. Table 8 summarizes the associated LOS computation results for cumulative Friday PM peak hour conditions. Please note that the corresponding LOS analysis calculation sheets for all analysis scenarios are presented in the appendix to this report. For this analysis the Friday evening cumulative and cumulative plus project conditions are presented in Table 8. As shown in Table 8, all of the project study intersections would continue to have acceptable operations (LOS D or better) under cumulative plus project conditions during the Friday PM peak hours except for the intersection of SR 16 with Latrobe Road and also the intersection of Golden Chain Highway (SR 49) with Village Drive (the proposed project entrance). Mitigations to improve the operations at these intersections are discussed in Section 5.

### 4.9 Roadway Segment Capacity Conditions

The average daily traffic (ADT) along with the capacity and worst-case Cumulative LOS (with and without the project) is shown in Table 9. The resulting volume to capacity (V/C) ratios with and without the proposed project and the resulting project change for the two segments exceeding the standards are shown in Table 10. The LOS standards were not exceeded on any segments in the existing segment analysis, which was based on 24 -hour traffic counts that were conducted on each roadway segment in May of 2023. As shown in Table 9, all of the study segments are forecast to continue to have acceptable operations under cumulative conditions with the exception of the segments of SR 16 from Stonehouse Road to Dillard Road and from Dillard Road to Grant Line Road. Please note these roadway segments are forecast to exceed the LOS standard (LOS D) regardless of whether or not the proposed project is implemented. As shown in Table 10, the maximum increase in the V/C ratio on either of the two roadway segments exceeding the standards was 0.03 , which is below the established standard of significance, which is an increase in the V/C ratio of 0.05 or more. Therefore, there would be no significant project impacts on any study roadway segments under cumulative plus project conditions.

TABLE 8
FRIDAY EVENING CUMULATIVE PLUS PROJECT INTERSECTION LEVEL OF SERVICE CONDITIONS

| INTERSECTION |  | CONTROL | CUMULATIVE |  | CUMULATIVE PLUS PROJECT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay | LOS | Delay | LOS |
| 1 | GOLDEN CHAIN HWY (SR-49) \& MILLER WAY |  | Side Street Stop | 9.9 | A | 10.1 | B |
| 2 | GOLDEN CHAIN HWY (SR-49) \& MAIN STREET | Roundabout | 7.2 | A | 7.6 | A |
| 3 | GOLDEN CHAIN HWY (SR-49) \& POPLAR STREET | Side Street Stop | 12.3 | B | 12.7 | B |
| 4 | GOLDEN CHAIN HWY (SR-49) \& PACIFIC STREET / EMPIRE STREET | Side Street Stop | 15.9 | C | 16.9 | C |
| 5 | GOLDEN CHAIN HWY (SR-49) \& 49ER VILLAGE / EMPIRE STREET | Side Street Stop | 23.4 | C | 26.1 | D |
| 6 | GOLDEN CHAIN HIGHWAY (SR-49) \& RANDOLPH DRIVE / VILLAGE DRIVE (THE PROJECT ENTRANCE) | Side Street Stop | 39.4 | E | > 50.0 | F |
| 7 | GOLDEN CHAIN HIGHWAY (SR-49) \& SR-16 | Signalized | 23.5 | C | 25.6 | C |
| 8 | SR-16 \& PLYMOUTH HIGHWAY (SR-124) | Side Street Stop | 19.5 | C | 23.6 | C |
| 9 | SR-16 \& LATROBE ROAD | Side Street Stop | > 50.0 | F | > 50.0 | F |
| 10 | JACKSON ROAD (SR-16) \& IONE ROAD | Side Street Stop | 23.6 | C | 27.2 | D |
| 11 | JACKSON ROAD (SR-16) \& GRANT LINE ROAD | Signalized | 24.7 | C | 25.7 | C |

SOURCE: Abrams Associates, 2023
NOTE: Delay results are presented in terms of seconds per vehicle.

### 4.10 Vehicle Miles Traveled

One performance measure that can be used to quantify the transportation impacts of a project is vehicle miles traveled (VMT). This section presents an analysis of the extent of the VMT-related transportation impacts caused by the Project. OPR recommends that VMT thresholds for residential and employment-based land use projects be set at fifteen percent below the baseline VMT/capita or VMT/employee. ${ }^{5}$ The Project is not located in a Transit Priority Area and, subject to County approval, would not otherwise be screened out from VMT analysis because of its location in a relatively high VMT generating area.

[^7]TABLE 9
CUMULATIVE PLUS PROJECT ROADWAY SEGMENT
LEVEL OF SERVICE CONDITIONS

| From | To | Location | Classification | Capacity | Impact Threshold | Cumulative ADT | $\begin{gathered} \text { CU+PR } \\ \text { ADT } \\ \hline \end{gathered}$ | CU+PR LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Village Drive (SR-49) | SR-16 | Amador | Arterial w/clmb lane | 22,200 | D | 12,253 | 13,738 | B |
| SR-49 | SR-124 | Amador | Class I Arterial | 16,900 | C | 14,707 | 16,007 | B |
| SR-124 | Latrobe Road | Amador | Class I Arterial | 16,900 | c | 12,530 | 13,302 | B |
| Old Sacramento Road | Ione Road | Amador | Class I Arterial | 16,900 | c | 8,000 | 8,557 | B |
| Stonehouse Road | Dillard Road | Sacramento | 2 Lane Arterial | 18,000 | D | 18,049 | 18,607 | D |
| Dillard Road | Grant Line Road | Sacramento | 2 Lane Arterial | 18,000 | D | 19,410 | 19,968 | D |

TABLE 10
CUMULATIVE CONDITIONS ROADWAY SEGMENT VIC RATIO ANALYSIS

| SEGMENT | CUMULATIVE | CUMULATIVE <br> +PROJECT | PROJECT <br> CHANGE |  |
| :---: | :---: | :---: | :---: | :---: |
| Stonehouse Road to Dillard Road | 18,049 | 0.90 | 18,607 | 0.93 |
| Dillard Road to Grant Line Road | 19,410 | 0.97 | 19,968 | 1.00 |

For this analysis, the California Statewide Travel Demand Model (CSTDM) was used. The model calculates VMT based on the number of vehicles multiplied by the typical distance traveled by each vehicle originating from or driving to a certain area. The volume of traffic and distance traveled depends on mix of land use types, density, and location as well as the existing and planned transportation system, including availability of public transportation. The model divides areas within the County into transportation analysis zones, or TAZs, which are used for transportation analysis and other planning purposes. It should be noted that the conclusions would be expected to be the same using the Amador County Transportation Commission's Travel Demand Model due to the project's location on SR 49 directly adjacent to the city limits of one of Amador County's five unincorporated Cities.

Near-Term Plus Project VMT Analysis - Based on the CSTDM Travel Demand Model the County's average VMT per employee is estimated to be 17.9 miles. The employees of the proposed project would be expected to have similar VMT to existing employees within the TAZ where the project is located, and in other surrounding TAZ's with similar land uses. The VMT per employee estimated by the CSTDM Travel Model for the project area would therefore be assumed represent the approximate VMT per employee that would be generated by the proposed project as well. The project site is located in TAZ 3003. Table 11 summarizes the existing VMT per employee for the project and provides a comparison to the County average VMT per employee. As seen in Table 11, the proposed project is forecast to have an average VMT per employee of 13.2 miles. Data from the CSTDM model indicates the project would not have a significant impact on VMT in the County.

TABLE 11
NEAR-TERM PLUS PROJECT VMT RESULTS

| Scenario | Project Average <br> VMT Per Employee | VMT Impact <br> Threshold $^{1}$ | Impact? |
| :---: | :---: | :---: | :---: |
| 2023 Plus Project | 13.2 miles | 17.9 miles | No |

NOTE: ${ }^{1}$ The existing plus project VMT impact threshold for commercial projects in Amador County is a VMT per employee that is no higher than the Countywide average VMT per employee which is 17.9 miles.

Cumulative Plus Project VMT Analysis - Since the project was not found to have a significant impact on VMT in the near-term scenario, a detailed evaluation of the project's cumulative VMT impacts was not conducted. The cumulative analysis is for determining if the Countywide VMT increases or decreases with the proposed project, relative to the VMT generated that would otherwise be generated by full General Plan buildout. Based on the data described above, the project's cumulative VMT impacts would also be assumed to be less-than-significant.

### 4.11 Transit Impacts

The project would not result in degradation of the level of service (or a significant increase in delay) on any roadway segments currently being utilized by bus transit in the area and, as such, no significant impacts to bus transit are expected. The proposed project is not be expected to significantly impact the operating capacity any existing Amador Transit bus routes. The proposed project could potentially help support existing bus services with additional transit ridership and would not conflict with any transit plans or goals of the County or Amador Transit. Although the proposed project does have the potential to increase patronage on bus lines in the area, no significant effects on transit capacity are anticipated given that the additional ridership would be added primarily in the non-peak directions. As a result, the project would not be expected to result in any significant impacts to bus transit service in the area.

### 4.12 Pedestrians, Bicycles and Non-Motorized Vehicular Travel

The County does not have level of service standards for pedestrian or bicycle facilities. Nevertheless, use of existing facilities by the users of the project would not be expected to overcrowd those facilities or decrease their performance or safety. The project will add some pedestrians and bicyclists in the area but the volumes added would not be expected to significantly impact any existing facilities. In relation to the existing conditions, the proposed project would not cause substantial changes to the pedestrian or bicycle traffic in the area and would not significantly impact or require changes to the design of any existing bicycle or pedestrian facilities. However, consistent with the County General Plan, the project could be asked to contribute to pedestrian and bicycle improvement measures in the project vicinity.

### 4.13 Site Access and Circulation

Based on the analysis of the proposed project no on-site circulation issues have been identified that would cause a traffic safety problem or any unusual traffic congestion or delay. However, the current plan to provide access to the site via the northern intersection of SR 49 with Village Drive could potentially result in safety impacts due to potential conflicts in the two-way left turn lane with left turns into Randolph Drive. This is an existing safety issue due to the off-set of the two approaches but it currently operates acceptably because of the low volume of left turns into the two side streets. With the higher left turn volumes from the proposed project this configuration could have increased left turn conflicts in the center two-way left-turn with an increased potential for head-on collisions. It is recommended that the project access be relocated to one of two other locations:

1) Line up the project entrance with Randolph Street.
2) Design the project access to connect only to the other (southern) intersection of Village Drive with SR 49.

At any of these locations the LOS analysis indicates the project's intersection with SR 49 will exceed the LOS standards under cumulative conditions if the project exit has only one lane on its approach to SR 49. Therefore, under any of the above access alternatives a recommended mitigation for cumulative plus project conditions will be to provide separate right and left turn lanes at the project exit (i.e., a two-lane approach).

### 4.14 Parking

The proposed project would provide an adequate supply of off-street parking based on the County's requirements. The project is currently proposing to meet the County's parking requirements and based on a review of the proposed parking plan there would be no significant parking impacts expected to the surrounding properties.

## 5) MITIGATION

The following is a summary of the proposed mitigation measures to address the transportation impacts of the project. Based on a detailed analysis of traffic operations with and without each of the proposed mitigations, implementation of the following mitigation measures would reduce some of the project impacts to a less-than-significant level.

## Impact \#1 Impacts to intersection operations - The project would result in a significant contribution (greater than 5 seconds delay) to the LOS operations at two intersections that would exceed the established standards under future weekday and Friday conditions:

1) State Route 16 at Latrobe Road (Intersection \#9)
2) Golden Chain Highway (SR 49) and the Project Entrance (Intersection \#6)

The addition of traffic from the proposed project would result in an increase in delay of more than five seconds to these two intersections that are forecast to exceed the established LOS standards. Please note that one of the impacted intersections (Intersection \#6) is within the City of Plymouth. The following mitigation measures would be forecast to reduce the impacts to a less-thansignificant level in all of the plus project scenarios.

## Mitigation Measures

MM 1 (a) State Route 16 at Latrobe Road - Payment of a proportionate share of the cost to install a traffic signal, meeting the County's requirements. Using Caltrans' methodology and the volume forecasts in this TIS, the estimated proportional share contribution from the project for this improvement would be 55\%.

MM 1 (b) Golden Chain Highway (SR 49) at Village Drive (the proposed project entrance) - Widening of Village Drive to allow for separate right and left turn lanes on the westbound approach to SR 49 (i.e., two lanes for traffic exiting the project at $S R$ 49). With this improvement the intersection would meet the established standards with the proposed casino. Using Caltrans' methodology and the volume forecasts in this TIS, the estimated proportional share contribution from the project for this improvement would be 81\%.

## Impact \#2 Impacts related to site access and circulation.

The current plan to provide access to the site via the northern intersection of SR 49 with Village Drive could result in safety impacts due to potential conflicts in the two-way left turn lane with left turns into Randolph Drive. It is our understanding that with the addition of traffic from the proposed project this off-set configuration with the two-way left turn lane may no longer be acceptable to Caltrans.

Regardless of the location. the LOS analysis indicates the project's intersection with SR 49 will exceed the LOS standards under cumulative conditions if the project exit has only one lane on its approach to SR 49. Therefore, under any of the above access alternatives the recommended mitigation for cumulative plus project conditions described previously, MM 1(b), would also need to be implemented. No other site circulation or access issues have been identified that would cause a traffic safety problem or any unusual traffic congestion or delay. Detailed LOS calculations for each of the project entrances under all scenarios are included in the technical appendix.
Mitigation Measure

MM 2 (a) Golden Chain Highway (SR 49) at Village Drive (the proposed project entrance) - Relocate the project access to one of two other recommended locations:

1) Line up the project entrance with Randolph Street.
2) Design the project access to connect only to the other (southern) intersection of Village Drive with SR 49.

## Impact \#3 Impacts related to conflicts with adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities, or potential decreases to the performance or safety of such facilities.

The project would not result in degradation of the level of service (or a significant increase in delay) on any roadway segments currently being utilized by bus transit in the area and would not increase ridership beyond existing capacity. As such, no significant impacts to bus transit are expected. In addition, the project would not significantly impact or change the design of any existing transportation facility or create any new safety problems in the area. Therefore, based on the County's significance criteria the project's impacts on alternative transportation would be considered less than significant and no mitigations would be required.

## Mitigation Measures

None required.

## Impact \#4 Demolition and construction activities associated with the proposed project would result in an increase in traffic to and from the site and could lead to unsafe conditions near the project site.

The increase in traffic as a result of demolition and construction activities associated with the proposed project has been quantified assuming a worst-case single phase construction period of 24 months.

## Heavy Equipment

Approximately 15 truck trips per day are estimated throughout the demolition and construction of the proposed project. Heavy equipment transport to and from the site could cause traffic impacts in the vicinity of the project site during construction. The project would implement a Traffic Control Plan to address this truck traffic.

The requirements within the Traffic Control Plan will include, but are not limited to, the following: truck drivers would be notified of and required to use the most direct routes; all site ingress and egress would occur only at the main driveways to the project site and construction activities may require installation of temporary traffic signals; specifically designated travel routes for large vehicles would be monitored and controlled by flaggers for large construction vehicle ingress and egress; warning signs indicating frequent truck entry and exit would be posted on State Route 49; and any debris and mud on nearby streets caused by trucks would be monitored daily and may require instituting a street cleaning program. In addition, the ten loads of heavy equipment being hauled to and from the site each month would be short-term and temporary.

## Employees

The weekday work is expected to begin around 7:00 AM and end around 4:00 PM. The construction worker arrival peak would occur between 6:30 AM and 7:30 AM, and the departure peak would occur between 4:00 PM and 5:00 PM. These peak hours are slightly before the countywide commute peaks. It should be noted that the number of trips generated during construction would not only be temporary, but would also be substantially less than the proposed project at buildout. Based on estimates of the number of construction workers, the project could require parking for up to 100 vehicles during the peak construction period. Additionally, deliveries, visits, and other activities may generate peak non-worker parking demand of 20 to 30 trucks and automobiles per day. Therefore, up to 130 vehicle parking spaces may be required during the peak construction period for the construction employees. Because the construction of the project can be staged so that employee parking demand is met by using on-site parking, the impacts of
construction-related employee traffic and parking are considered less-thansignificant.

## Construction Material Import/Export

The project would also require removal of existing debris as well as the importation of construction material, including raw materials for the building pads, the buildings, the parking area, and landscaping. During the maximum peak construction period, it is estimated material import and export could generate approximately 10 truck trips per day.

## Traffic Control Plan

The Traffic Control Plan would indicate how parking for construction workers would be provided during construction on adjacent land currently held in trust by the Tribe to ensure a safe flow of traffic in the project area during construction. This analysis assumed construction of the entire project in one phase to identify the potential worst-case traffic effects. If the project is built in phases over time, the effects of each phase will be the same or less. Therefore, the demolition and construction activities associated with the proposed project or its individual phases would not lead to noticeable congestion in the vicinity of the site or the perception of decreased traffic safety resulting in a less-than-significant impact.

## Mitigation Measures

None required.

## Impact \#5 Impacts regarding emergency vehicle access on and surrounding the proposed project site.

Sufficient emergency access is determined by factors such as number of access points, roadway width, and proximity to fire stations. The land use plan for the proposed project includes the main entrance on SR 49 and will include a secondary emergency vehicle access. All lane widths within the project would meet the minimum width that can accommodate an emergency vehicle; therefore, the width of the internal roadways would be adequate. In addition, with the proposed mitigations the addition of project traffic would not result in any significant changes to emergency vehicle response times in the area. Therefore, development of the project is expected to have less-than-significant impacts regarding emergency vehicle access.

## Mitigation Measures

None required.


# Transportation Impact Study Technical Appendix Ione Casino Project 

Amador County

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# Appendix Table of Contents 

1.) Accident Summary (5 Years)
2.) Warrants
3.) HCM 6th Edition Level of Service (LOS) Results

| Ione Casino Project Amador County |  | Collision Data2022-2017 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CASE ID |  |  | PRIMARY RD | SECONDARY RD |  |  |  | TYPE OF COLLISION | COLLISION SEVERITY |  |  | PCF VIOLATION CATEGORY | MOTOR VEHICLE INVOLVED WITH |  |
| 2022 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91883294 | 20220923 | 1203 | SR-49 | MAIN STREET | 00 | Y | Clear | Rear End | Injury (Other Visible) | 0 | 2 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |
| 91886196 | 20220927 | 625 | SR-49 | MAIN STREET | 00 | Y | Clear | Broadside | Property Damage Only | 0 | 0 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91955641 | 20221201 | 1010 | SR-49 NORTH | MAIN STREET | 40 N | N | Cloudy | Rear End | Property Damage Only | 0 | 0 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91740420 | 20220324 | 930 | SR-49 | SR-16 | 00 | Y | Clear | Overturned | Property Damage Only | 0 | 0 | Unsafe Speed | Non-Collision | 0 |
| 91927190 | 20221117 | 1650 | SR-49 | SR-16 | 230 S | N | Clear | Hit Object | Injury (Severe) | 0 | 1 | Wrong Side of Road | Fixed Object | 0 |
| 91956582 | 20221220 | 1405 | SR-16 | SR-49 | 00 | Y | Clear | Rear End | Injury (Other Visible) | 0 | 2 | Unsafe Speed | Other Motor Vehicle | 0 |
| 91788240 | 20220525 | 830 | SR-16 | SR-124 | 00 | Y | Clear | Broadside | Injury (Other Visible) | 0 | 1 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91847769 | 20220822 | 820 | SR-16 | SR-124 | 00 | Y | Clear | Broadside | Injury (Complaint of Pain) | 0 | 2 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91905261 | 20221022 | 2145 | SR-16 | SR-124 | 135 W | N | Clear | Hit Object | Injury (Severe) | 0 | 1 | DUI | \#N/A | Y |
| 91833440 | 20220731 | 1230 | SR-16 | LATROBE RD | 00 | Y | Clear | Rear End | Injury (Other Visible) | 0 | 2 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91958784 | 20221227 | 520 | SR-16 | IONE RD | 00 | Y | Cloudy | Broadside | Property Damage Only | 0 | 0 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91694200 | 20220205 | 1045 | SR-16 | GRANT LINE RD | 45 E | N | Clear | Rear End | Property Damage Only | 0 | 0 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |
| 91762539 | 20220423 | 1725 | SR-16 | GRANTLINE RD. | 150 E | N | Clear | Rear End | Property Damage Only | 0 | 0 | Unsafe Speed | Other Motor Vehicle | 0 |
| 91787975 | 20220525 | 1130 | SR-16 | GRANT LINE RD. | 30 E | N | Clear | Rear End | Property Damage Only | 0 | 0 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |




| Ione Casino Project Amador County |  |  | Collision Data2022-2017 |  |  |  |  |  |  |  |  | PCF VIOLATION CATEGORY | MOTOR VEHICLE INVOLVED WITH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CASE ID |  |  | PRIMARY RD | SECONDARY RD |  |  |  | TYPE OF COLLISION | COLLISION SEVERITY |  |  |  |  |  |
| 2019 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91109706 | 20191018 | 1428 | SR-49 | MILLER WAY | 00 | Y | Clear | Broadside | Injury (Complaint of Pain) | 0 | 2 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 90938675 | 20190224 | 520 | SR-16 E/B TO SR-49 SSR-16 |  | 200 S | N | Cloudy | Hit Object | Injury (Other Visible) | 0 | 1 | DUI | Fixed Object | Y |
| 91009343 | 20190607 | 540 | SR-49 | SR-16 | 18 S | N | Clear | Overturned | Property Damage Only | 0 | 0 | Unsafe Speed | Non-Collision | 0 |
| 91097715 | 20191011 | 600 | SR-16 | SR-49 | 00 | Y | Clear | Broadside | Property Damage Only | 0 | 0 | Traffic Signals and Signs | Other Motor Vehicle | 0 |
| 91112971 | 20191030 | 1520 | SR-16 | SR-49 | 00 | Y | Clear | Broadside | Property Damage Only | 0 | 0 | Traffic Signals and Signs | Other Motor Vehicle | 0 |
| 91153180 | 20191224 | 1120 | SR-49 | SR-16 | 60 S | N | Cloudy | Rear End | Injury (Complaint of Pain) | 0 | 1 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |
| 90954069 | 20190319 | 1045 | SR-16 (JACKS | IONE RD | 32 W | N | Cloudy | Broadside | Injury (Severe) | 0 | 1 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 90954333 | 20190320 | 630 | IONE RD | SR-16 | 00 | Y | Cloudy | Broadside | Injury (Complaint of Pain) | 0 | 1 | Automobile Right of Way | Other Motor Vehicle | 0 |
| 91137157 | 20191127 | 1700 | SR-16 | IONE RD | 150 E | N | Cloudy | Hit Object | Injury (Complaint of Pain) | 0 | 1 | Improper Turning | Fixed Object | 0 |
| 91097483 | 20191006 | 1830 | SR-16 | GRANT LINE RD | 50 W | N | Clear | Rear End | Property Damage Only | 0 | 0 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |
| 91114761 | 20191026 | 745 | SR-16 | GRANT LINE RD | 75 W | N | Clear | Rear End | Injury (Complaint of Pain) | 0 | 1 | Unsafe Starting or Backing | Other Motor Vehicle | 0 |
| 91121608 | 20191109 | 1335 | SR-16 | GRANT LINE RD | 00 | Y | Clear | Sideswipe | Property Damage Only | 0 | 0 | Traffic Signals and Signs | Other Motor Vehicle | 0 |
| 91142876 | 20191210 | 1910 | SR-16 | GRANT LINE RD | 50 W | N | Cloudy | Rear End | Property Damage Only | 0 | 0 | DUI | Other Motor Vehicle | Y |



## PEAK HOUR VOLUME WARRANT <br> (Urban Areas)



MAJOR STREET—TOTAL OF BOTH APPROACHES—
VEHICLES PER HOUR (VPH)

* note:

150 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR-STREET APPROACH WITH TWO OR MORE LANES AND 100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR-STREET APPROACH WITH ONE LANE.

SOURCE:
MUTCD, CHAPTER 4
(FIGURE 4C-3)
\#6 - GOLDEN CHAIN HIGHWAY (SR-49) \& VILLAGE DRIVE - CUMULATIVE PLUS PROJECT Ione Casino Project



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 4.4 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 68 | 240 | 207 | 106 |
| Demand Flow Rate, veh/h | 69 | 244 | 211 | 108 |
| Vehicles Circulating, veh/h | 251 | 114 | 42 | 241 |
| Vehicles Exiting, veh/h | 98 | 139 | 278 | 117 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.0 | 4.7 | 4.1 | 4.3 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 69 | 244 | 211 | 108 |
| Cap Entry Lane, veh/h | 1068 | 1228 | 1322 | 1079 |
| Entry HV Adj Factor | 0.979 | 0.982 | 0.983 | 0.984 |
| Flow Entry, veh/h | 68 | 240 | 207 | 106 |
| Cap Entry, veh/h | 1045 | 1207 | 1299 | 1062 |
| VIC Ratio | 0.065 | 0.199 | 0.160 | 0.100 |
| Control Delay, s/veh | 4.0 | 4.7 | 4.1 | 4.3 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 0 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement EBL | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Traffic Vol, veh/h | 3 | 0 | 82 | 3 | 1 | 1 | 78 | 203 | 0 | 1 | 267 | 3 |  |
| Future Vol, veh/h | 3 | 0 | 82 | 3 | 1 | 1 | 78 | 203 | 0 | 1 | 267 | 3 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control S | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 3 | 0 | 89 | 3 | 1 | 1 | 85 | 221 | 0 | 1 | 290 | 3 |  |


| Major/Minor | Minor2 | Minor1 |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 686 | 685 | 292 | 729 | 686 | 221 | 293 | 0 | 0 | 221 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Stage 1 | 294 | 294 | - | 391 | 391 | - | - | - | - | - | - |







## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\boldsymbol{\beta}$ |  |  | 个 | a | $\mathbf{7}$ |
| Traffic Vol, veh/h | 301 | 29 | 88 | 367 | 20 | 81 |
| Future Vol, veh/h | 301 | 29 | 88 | 367 | 20 | 81 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 327 | 32 | 96 | 399 | 22 | 88 |




| Major/Minor | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 451 | 0 | - | 0 | 562 | 365 |
| Stage 1 | - | - | - | - | 365 | - |
| Stage 2 | - | - | - | - | 197 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1109 | - |  | - | 488 | 680 |
| Stage 1 | - | - | - | - | 702 | - |
| Stage 2 | - | - | - | - | 836 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1109 | - | - | - | 488 | 680 |
| Mov Cap-2 Maneuver | - | - | - | - | 488 | - |
| Stage 1 | - | - | - | - | 702 | - |
| Stage 2 | - | - | - | - | 836 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  |  |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 15.2 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | T | WBR | SBLn1 |
| Capacity (veh/h) |  | 1109 | - | - | - | 491 |
| HCM Lane V/C Ratio |  | - | - | - | - | 0.281 |
| HCM Control Delay (s) |  | 0 | - | - | - | 15.2 |
| HCM Lane LOS |  | A | - | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 1.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  | 1 | 个 | r | $\mathbf{7}$ |
| Traffic Vol, veh/h | 183 | 110 | 4 | 293 | 113 | 2 |
| Future Vol, veh/h | 183 | 110 | 4 | 293 | 113 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 199 | 120 | 4 | 318 | 123 | 2 |



|  | $\rangle$ | $\rightarrow$ |  | $\dagger$ |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\square}$ |  | ${ }^{*}$ | $\uparrow$ |  |  | ${ }_{4}$ |  |  | 4 |  |
| Traffic Volume (veh/h) | 47 | 295 | 2 | 57 | 631 | 41 | 3 | 285 | 37 | 26 | 230 | 34 |
| Future Volume (veh/h) | 47 | 295 | 2 | 57 | 631 | 41 | 3 | 285 | 37 | 26 | 230 | 34 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 51 | 321 | 2 | 62 | 686 | 45 | 3 | 310 | 40 | 28 | 250 | 37 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 66 | 759 | 5 | 80 | 724 | 48 | 3 | 331 | 43 | 30 | 268 | 40 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.05 | 0.42 | 0.42 | 0.21 | 0.21 | 0.21 | 0.19 | 0.19 | 0.19 |
| Sat Flow, veh/h | 1781 | 1857 | 12 | 1781 | 1736 | 114 | 16 | 1609 | 208 | 162 | 1447 | 214 |
| Grp Volume(v), veh/h | 51 | 0 | 323 | 62 | 0 | 731 | 353 | 0 | 0 | 315 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1868 | 1781 | 0 | 1850 | 1832 | 0 | 0 | 1824 | 0 | 0 |
| Q Serve(g_s), s | 3.3 | 0.0 | 14.3 | 4.0 | 0.0 | 44.2 | 22.0 | 0.0 | 0.0 | 19.8 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 3.3 | 0.0 | 14.3 | 4.0 | 0.0 | 44.2 | 22.0 | 0.0 | 0.0 | 19.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 0.01 |  | 0.11 | 0.09 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 66 | 0 | 764 | 80 | 0 | 772 | 377 | 0 | 0 | 338 | 0 | 0 |
| V/C Ratio(X) | 0.78 | 0.00 | 0.42 | 0.77 | 0.00 | 0.95 | 0.94 | 0.00 | 0.00 | 0.93 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 81 | 0 | 764 | 189 | 0 | 817 | 377 | 0 | 0 | 338 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 55.5 | 0.0 | 24.5 | 54.9 | 0.0 | 32.6 | 45.4 | 0.0 | 0.0 | 46.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 30.6 | 0.0 | 0.4 | 14.5 | 0.0 | 19.3 | 30.5 | 0.0 | 0.0 | 32.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.0 | 0.0 | 6.4 | 2.1 | 0.0 | 23.4 | 13.1 | 0.0 | 0.0 | 11.9 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 86.0 | 0.0 | 24.9 | 69.3 | 0.0 | 51.9 | 75.9 | 0.0 | 0.0 | 78.8 | 0.0 | 0.0 |
| LnGrp LOS | F | A | C | E | A | D | E | A | A | E | A | A |
| Approach Vol, veh/h |  | 374 |  |  | 793 |  |  | 353 |  |  | 315 |  |
| Approach Delay, s/veh |  | 33.2 |  |  | 53.2 |  |  | 75.9 |  |  | 78.8 |  |
| Approach LOS |  | C |  |  | D |  |  | E |  |  | E |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 9.7 | 52.0 |  | 26.0 | 8.8 | 53.0 |  | 28.4 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.3 | 44.3 |  | 21.5 | 5.3 | 51.3 |  | 23.9 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.0 | 16.3 |  | 21.8 | 5.3 | 46.2 |  | 24.0 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 2.0 |  | 0.0 | 0.0 | 2.2 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 57.9 |  |  |  |  |  |  |  |  |  |
|  |  |  | E |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 4.9 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 93 | 210 | 339 | 156 |
| Demand Flow Rate, veh/h | 95 | 214 | 346 | 159 |
| Vehicles Circulating, veh/h | 285 | 155 | 80 | 224 |
| Vehicles Exiting, veh/h | 97 | 271 | 300 | 145 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.4 | 4.7 | 5.3 | 4.6 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 95 | 214 | 346 | 159 |
| Cap Entry Lane, veh/h | 1032 | 1178 | 1272 | 1098 |
| Entry HV Adj Factor | 0.978 | 0.981 | 0.979 | 0.984 |
| Flow Entry, veh/h | 93 | 210 | 339 | 156 |
| Cap Entry, veh/h | 1009 | 1156 | 1245 | 1081 |
| VIC Ratio | 0.092 | 0.182 | 0.272 | 0.145 |
| Control Delay, s/veh | 4.4 | 4.7 | 5.3 | 4.6 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |










## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | $\mathbf{4}$ | t | $\mathbf{7}$ |
| Traffic Vol, veh/h | 444 | 32 | 81 | 338 | 22 | 109 |
| Future Vol, veh/h | 444 | 32 | 81 | 338 | 22 | 109 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 483 | 35 | 88 | 367 | 24 | 118 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  |  | F |  | M |  |
| Traffic Vol, veh/h | 1 |  | 194 | 160 | 191 | 1 |
| Future Vol, veh/h | 1 | 298 | 194 | 160 | 191 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 324 | 211 | 174 | 208 | 1 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | A | I | $\mathbf{7}$ |
| Traffic Vol, veh/h | 315 | 161 | 1 | 219 | 125 | 1 |
| Future Vol, veh/h | 315 | 161 | 1 | 219 | 125 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 342 | 175 | 1 | 238 | 136 | 1 |


| Major/Minor | Major1 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Major2 |  | Minor1 |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 517 | 0 | 670 | 430 |
| $\quad$ Stage 1 | - | - | - | - | 430 | - |
| $\quad$ Stage 2 | - | - | - | - | 240 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | -2.218 | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | - | - | 1049 | - | 422 | 625 |
| $\quad$ Stage 1 | - | - | - | - | 656 | - |
| Stage 2 | - | - | - | - | 800 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1049 | - | 422 | 625 |
| Mov Cap-2 Maneuver | - | - | - | - | 422 | - |
| Stage 1 | - | - | - | - | 656 | - |
| Stage 2 | - | - | - | - | 799 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 17.4 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 422 | 625 | - | -1049 | - |  |
| HCM Lane V/C Ratio | 0.322 | 0.002 | - | -0.001 | - |  |
| HCM Control Delay (s) | 17.5 | 10.8 | - | - | 8.4 | - |
| HCM Lane LOS | C | B | - | - | A | - |
| HCM 95th \%tile Q(veh) | 1.4 | 0 | - | - | 0 | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F |  | 7 | F |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 34 | 613 | 6 | 62 | 412 | 35 | 6 | 298 | 87 | 43 | 288 | 45 |
| Future Volume (veh/h) | 34 | 613 | 6 | 62 | 412 | 35 | 6 | 298 | 87 | 43 | 288 | 45 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 37 | 666 | 7 | 67 | 448 | 38 | 7 | 324 | 95 | 47 | 313 | 49 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 53 | 693 | 7 | 82 | 666 | 56 | 7 | 304 | 89 | 43 | 286 | 45 |
| Arrive On Green | 0.03 | 0.37 | 0.37 | 0.05 | 0.39 | 0.39 | 0.22 | 0.22 | 0.22 | 0.21 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1781 | 1847 | 19 | 1781 | 1700 | 144 | 30 | 1367 | 401 | 209 | 1393 | 218 |
| Grp Volume(v), veh/h | 37 | 0 | 673 | 67 | 0 | 486 | 426 | 0 | 0 | 409 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 0 | 1844 | 1797 | 0 | 0 | 1821 | 0 | 0 |
| Q Serve(g_s), s | 2.5 | 0.0 | 42.0 | 4.4 | 0.0 | 25.9 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.5 | 0.0 | 42.0 | 4.4 | 0.0 | 25.9 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.02 |  | 0.22 | 0.11 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 53 | 0 | 700 | 82 | 0 | 722 | 399 | 0 | 0 | 374 | 0 | 0 |
| V/C Ratio(X) | 0.70 | 0.00 | 0.96 | 0.82 | 0.00 | 0.67 | 1.07 | 0.00 | 0.00 | 1.09 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 0 | 713 | 82 | 0 | 722 | 399 | 0 | 0 | 374 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.3 | 0.0 | 36.4 | 56.3 | 0.0 | 30.0 | 46.3 | 0.0 | 0.0 | 47.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 15.5 | 0.0 | 24.3 | 44.6 | 0.0 | 2.5 | 63.8 | 0.0 | 0.0 | 73.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.3 | 0.0 | 23.5 | 3.0 | 0.0 | 11.9 | 18.8 | 0.0 | 0.0 | 18.7 | 0.0 | 0.0 |

Unsig. Movement Delay, s/veh

| LnGrp Delay (d),s/veh | 72.8 | 0.0 | 60.8 | 101.0 | 0.0 | 32.4 | 110.1 | 0.0 | 0.0 | 121.2 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | E | A | E | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 710 |  |  | 553 |  |  | 426 |  | 409 |  |  |
| Approach Delay, s/veh |  | 61.4 |  |  | 40.7 |  |  | 110.1 |  | 121.2 |  |  |
| Approach LOS | E |  |  | D |  |  | F |  |  | F |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 10.0 | 49.2 | 29.0 | 8.0 | 51.2 | 31.0 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 5.5 | 45.5 | 24.5 | 5.1 | 45.9 | 26.5 |
| Max Q Clear Time (g_c+11), s | 6.4 | 44.0 | 26.5 | 4.5 | 27.9 | 28.5 |
| Green Ext Time (p_C), s | 0.0 | 0.7 | 0.0 | 0.0 | 3.0 | 0.0 |

Intersection Summary
HCM 6th Ctrl Delay 77.5

HCM 6th LOS E

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y |  |  | 4 | F |  |
| Traffic Vol, veh/h | 5 | 21 | 10 | 107 | 77 | 1 |
| Future Vol, veh/h | 5 | 21 | 10 | 107 | 77 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 23 | 11 | 116 | 84 | 1 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 4.4 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 68 | 241 | 215 | 114 |
| Demand Flow Rate, veh/h | 69 | 245 | 219 | 116 |
| Vehicles Circulating, veh/h | 260 | 121 | 42 | 242 |
| Vehicles Exiting, veh/h | 98 | 140 | 287 | 124 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.0 | 4.8 | 4.1 | 4.3 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 69 | 245 | 219 | 116 |
| Cap Entry Lane, veh/h | 1058 | 1220 | 1322 | 1078 |
| Entry HV Adj Factor | 0.979 | 0.982 | 0.983 | 0.984 |
| Flow Entry, veh/h | 68 | 241 | 215 | 114 |
| Cap Entry, veh/h | 1036 | 1198 | 1299 | 1061 |
| V/C Ratio | 0.065 | 0.201 | 0.166 | 0.108 |
| Control Delay, s/veh | 4.0 | 4.8 | 4.1 | 4.3 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 0 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |










## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{7}$ |  |  | A | l | $\mathbf{7}$ |
| Traffic Vol, veh/h | 314 | 29 | 96 | 380 | 20 | 89 |
| Future Vol, veh/h | 314 | 29 | 96 | 380 | 20 | 89 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 341 | 32 | 104 | 413 | 22 | 97 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | 1 |  | Mr |  |
| Traffic Vol, veh/h | 0 | 190 | 266 | 162 | 128 | 3 |
| Future Vol, veh/h | 0 | 190 | 266 | 162 | 128 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 207 | 289 | 176 | 139 | 3 |


| Major/Minor M | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 465 | 0 | - | 0 | 584 | 377 |
| Stage 1 | - | - | - | - | 377 | - |
| Stage 2 | - | - | - | - | 207 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1096 | - | - | - | 474 | 670 |
| Stage 1 | - | - | - | - | 694 | - |
| Stage 2 | - | - | - | - | 828 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1096 | - | - | - | 474 | 670 |
| Mov Cap-2 Maneuver | - | - | - | - | 474 | - |
| Stage 1 | - | - | - | - | 694 | - |
| Stage 2 | - | - | - | - | 828 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | B |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 15.7 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL EBT WBT WBRSBLn1 |  |  |  |  |
| Capacity (veh/h) |  | 1096 | - | - - | - | 477 |
| HCM Lane V/C Ratio |  | - | - | - | - | 0.299 |
| HCM Control Delay (s) |  | 0 | - | - | - | 15.7 |
| HCM Lane LOS |  | A | - | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 1.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | 4 | 1 | $\mathbf{T}$ |
| Traffic Vol, veh/h | 192 | 110 | 4 | 302 | 113 | 2 |
| Future Vol, veh/h | 192 | 110 | 4 | 302 | 113 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 209 | 120 | 4 | 328 | 123 | 2 |



|  | $\rangle$ | $\rightarrow$ |  | $\dagger$ |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |  | ¢ |  |  | 4 |  |
| Traffic Volume (veh/h) | 47 | 302 | 2 | 58 | 638 | 42 | 3 | 285 | 38 | 27 | 230 | 34 |
| Future Volume (veh/h) | 47 | 302 | 2 | 58 | 638 | 42 | 3 | 285 | 38 | 27 | 230 | 34 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 51 | 328 | 2 | 63 | 693 | 46 | 3 | 310 | 41 | 29 | 250 | 37 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 66 | 763 | 5 | 81 | 728 | 48 | 3 | 328 | 43 | 31 | 266 | 39 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.05 | 0.42 | 0.42 | 0.20 | 0.20 | 0.20 | 0.18 | 0.18 | 0.18 |
| Sat Flow, veh/h | 1781 | 1857 | 11 | 1781 | 1735 | 115 | 16 | 1604 | 212 | 167 | 1443 | 214 |
| Grp Volume(v), veh/h | 51 | 0 | 330 | 63 | 0 | 739 | 354 | 0 | 0 | 316 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1868 | 1781 | 0 | 1850 | 1831 | 0 | 0 | 1824 | 0 | 0 |
| Q Serve(g_s), s | 3.3 | 0.0 | 14.7 | 4.1 | 0.0 | 45.0 | 22.2 | 0.0 | 0.0 | 20.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 3.3 | 0.0 | 14.7 | 4.1 | 0.0 | 45.0 | 22.2 | 0.0 | 0.0 | 20.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 0.01 |  | 0.12 | 0.09 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 66 | 0 | 768 | 81 | 0 | 777 | 375 | 0 | 0 | 336 | 0 | 0 |
| V/C Ratio(X) | 0.78 | 0.00 | 0.43 | 0.77 | 0.00 | 0.95 | 0.94 | 0.00 | 0.00 | 0.94 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 81 | 0 | 768 | 188 | 0 | 813 | 375 | 0 | 0 | 336 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 55.7 | 0.0 | 24.6 | 55.1 | 0.0 | 32.7 | 45.7 | 0.0 | 0.0 | 47.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 30.9 | 0.0 | 0.4 | 14.3 | 0.0 | 20.2 | 32.3 | 0.0 | 0.0 | 33.9 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.1 | 0.0 | 6.6 | 2.2 | 0.0 | 23.9 | 13.4 | 0.0 | 0.0 | 12.2 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 86.6 | 0.0 | 25.0 | 69.4 | 0.0 | 52.9 | 78.0 | 0.0 | 0.0 | 80.9 | 0.0 | 0.0 |
| LnGrp LOS | F | A | C | E | A | D | E | A | A | F | A | A |
| Approach Vol, veh/h |  | 381 |  |  | 802 |  |  | 354 |  |  | 316 |  |
| Approach Delay, s/veh |  | 33.2 |  |  | 54.2 |  |  | 78.0 |  |  | 80.9 |  |
| Approach LOS |  | C |  |  | D |  |  | E |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 9.8 | 52.5 |  | 26.0 | 8.8 | 53.5 |  | 28.4 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.3 | 44.3 |  | 21.5 | 5.3 | 51.3 |  | 23.9 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.1 | 16.7 |  | 22.0 | 5.3 | 47.0 |  | 24.2 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 2.1 |  | 0.0 | 0.0 | 2.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 59.0 |  |  |  |  |  |  |  |  |  |
|  |  |  | E |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | 4 | b |  |
| Traffic Vol, veh/h | 2 | 24 | 61 | 136 | 165 | 7 |
| Future Vol, veh/h | 2 | 24 | 61 | 136 | 165 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 26 | 66 | 148 | 179 | 8 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.9 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 115 | 264 | 447 | 205 |
| Demand Flow Rate, veh/h | 117 | 270 | 457 | 208 |
| Vehicles Circulating, veh/h | 381 | 238 | 84 | 286 |
| Vehicles Exiting, veh/h | 113 | 303 | 414 | 221 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.1 | 5.8 | 6.3 | 5.5 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | ---: | :---: | ---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR |  |  |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 4.976 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 208 |
| Entry Flow, veh/h | 117 | 270 | 457 | 1031 |
| Cap Entry Lane, veh/h | 936 | 1082 | 1267 | 0.983 |
| Entry HV Adj Factor | 0.982 | 0.977 | 2.979 | 105 |
| Flow Entry, veh/h | 115 | 264 | 447 | 0.202 |
| Cap Entry, veh/h | 919 | 1058 | 1240 | 5.5 |
| V/C Ratio | 0.125 | 0.249 | 0.361 | A |
| Control Delay, s/veh | 5.1 | 5.8 | 6.3 | 1 |
| LOS | A | 1 | 2 |  |
| 95th \%tile Queue, veh | 0 | 1 | 2 |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | -1 | $\uparrow$ |  |
| Traffic Vol, veh/h | 0 | 37 | 34 | 405 | 379 | 1 |
| Future Vol, veh/h | 0 | 37 | 34 | 405 | 379 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 40 | 37 | 440 | 412 | 1 |










## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | A | 1 | 「 |
| Traffic Vol, veh/h | 562 | 33 | 117 | 416 | 22 | 154 |
| Future Vol, veh/h | 562 | 33 | 117 | 416 | 22 | 154 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 611 | 36 | 127 | 452 | 24 | 167 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 7.9 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\mathbf{4}$ | F |  | M |  |
| Traffic Vol, veh/h | 1 | 372 | 245 | 187 | 236 | 1 |
| Future Vol, veh/h | 1 | 372 | 245 | 187 | 236 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 404 | 266 | 203 | 257 | 1 |




| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor1 |  |  |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 601 | 0 | 807 | 512 |
| $\quad$ Stage 1 | - | - | - | - | 512 | - |
| Stage 2 | - | - | - | - | 295 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 976 | - | 351 | 562 |
| $\quad$ Stage 1 | - | - | - | - | 602 | - |
| Stage 2 | - | - | - | - | 755 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 976 | - | 351 | 562 |
| Mov Cap-2 Maneuver | - | - | - | - | 351 | - |
| Stage 1 | - | - | - | - | 602 | - |
| Stage 2 | - | - | - | - | 754 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 21.7 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 351 | 562 | - | - | 976 | - |
| HCM Lane V/C Ratio | 0.396 | 0.002 | - | -0.001 | - |  |
| HCM Control Delay (s) | 21.8 | 11.4 | - | - | 8.7 | - |
| HCM Lane LOS | C | B | - | - | A | - |
| HCM 95th \%tile Q(veh) | 1.8 | 0 | - | - | 0 | - |


|  | $\rangle$ | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\square}$ |  | \% | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 35 | 674 | 6 | 73 | 454 | 39 | 6 | 304 | 104 | 48 | 294 | 46 |
| Future Volume (veh/h) | 35 | 674 | 6 | 73 | 454 | 39 | 6 | 304 | 104 | 48 | 294 | 46 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 38 | 733 | 7 | 79 | 493 | 42 | 7 | 330 | 113 | 52 | 320 | 50 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 53 | 701 | 7 | 82 | 671 | 57 | 6 | 290 | 99 | 46 | 282 | 44 |
| Arrive On Green | 0.03 | 0.38 | 0.38 | 0.05 | 0.40 | 0.40 | 0.22 | 0.22 | 0.22 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1850 | 18 | 1781 | 1700 | 145 | 28 | 1311 | 449 | 224 | 1380 | 216 |
| Grp Volume(v), veh/h | 38 | 0 | 740 | 79 | 0 | 535 | 450 | 0 | 0 | 422 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 0 | 1844 | 1788 | 0 | 0 | 1820 | 0 | 0 |
| Q Serve(g_s), s | 2.5 | 0.0 | 45.5 | 5.3 | 0.0 | 29.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.5 | 0.0 | 45.5 | 5.3 | 0.0 | 29.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.02 |  | 0.25 | 0.12 |  | 0.12 |
| Lane Grp Cap (c), veh/h | 53 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| V/C Ratio(X) | 0.71 | 0.00 | 1.05 | 0.97 | 0.00 | 0.73 | 1.14 | 0.00 | 0.00 | 1.14 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.7 | 0.0 | 37.3 | 57.2 | 0.0 | 30.9 | 46.8 | 0.0 | 0.0 | 47.8 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 16.3 | 0.0 | 46.2 | 88.5 | 0.0 | 3.9 | 89.1 | 0.0 | 0.0 | 88.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 0.0 | 29.4 | 4.4 | 0.0 | 13.8 | 21.5 | 0.0 | 0.0 | 20.2 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 74.0 | 0.0 | 83.5 | 145.6 | 0.0 | 34.8 | 135.8 | 0.0 | 0.0 | 136.6 | 0.0 | 0.0 |
| LnGrp LOS | E | A | F | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 778 |  |  | 614 |  |  | 450 |  |  | 422 |  |
| Approach Delay, s/veh |  | 83.0 |  |  | 49.0 |  |  | 135.8 |  |  | 136.6 |  |
| Approach LOS |  | F |  |  | D |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 10.0 | 50.0 |  | 29.0 | 8.1 | 51.9 |  | 31.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.5 | 45.5 |  | 24.5 | 5.1 | 45.9 |  | 26.5 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.3 | 47.5 |  | 26.5 | 4.5 | 31.7 |  | 28.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 |  | 0.0 | 0.0 | 3.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 94.3 |  |  |  |  |  |  |  |  |  |
|  |  |  | F |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | 4 | F |  |
| Traffic Vol, veh/h | 11 | 71 | 16 | 119 | 75 | 2 |
| Future Vol, veh/h | 11 | 71 | 16 | 119 | 75 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 77 | 17 | 129 | 82 | 2 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 4.9 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 79 | 258 | 285 | 168 |
| Demand Flow Rate, veh/h | 81 | 262 | 291 | 171 |
| Vehicles Circulating, veh/h | 329 | 156 | 55 | 274 |
| Vehicles Exiting, veh/h | 116 | 190 | 355 | 144 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.5 | 5.1 | 4.7 | 5.0 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 81 | 262 | 291 | 171 |
| Cap Entry Lane, veh/h | 987 | 1177 | 1305 | 1043 |
| Entry HV Adj Factor | 0.981 | 0.983 | 0.979 | 0.984 |
| Flow Entry, veh/h | 79 | 258 | 285 | 168 |
| Cap Entry, veh/h | 967 | 1157 | 1277 | 1027 |
| VIC Ratio | 0.082 | 0.223 | 0.223 | 0.164 |
| Control Delay, s/veh | 4.5 | 5.1 | 4.7 | 5.0 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |







| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 0.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 /}$ | $\uparrow$ |  |  | $\uparrow$ |  | ${ }^{7}$ | 4 | 「゙ | ${ }^{7}$ | 4 | 「 |
| Traffic Vol，veh／h | 1 | 1 | 1 | 3 | 0 | 14 | 4 | 338 | 3 | 19 | 542 | 7 |
| Future Vol，veh／h | 1 | 1 | 1 | 3 | 0 | 14 | 4 | 338 | 3 | 19 | 542 | 7 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | － | － | Stop | － | － | None | － | － | None | － | － | None |
| Storage Length | 0 | － | 40 | － | － | － | 100 | － | 200 | 100 | － | 100 |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 1 | 1 | 3 | 0 | 15 | 4 | 367 | 3 | 21 | 589 | 8 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1 /}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 |  | $\uparrow$ | 「 |  | \＆ |  |
| Traffic Volume（veh／h） | 4 | 169 | 247 | 274 | 263 | 3 | 302 | 4 | 164 | 7 | 12 | 11 |
| Future Volume（veh／h） | 4 | 169 | 247 | 274 | 263 | 3 | 302 | 4 | 164 | 7 | 12 | 11 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 4 | 174 | 0 | 282 | 271 | 3 | 311 | 4 | 0 | 8 | 13 | 12 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 10 | 270 |  | 361 | 639 | 546 | 423 | 5 |  | 16 | 25 | 23 |
| Arrive On Green | 0.01 | 0.15 | 0.00 | 0.20 | 0.34 | 0.34 | 0.24 | 0.24 | 0.00 | 0.04 | 0.04 | 0.04 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1760 | 23 | 1572 | 421 | 684 | 631 |
| Grp Volume（v），veh／h | 4 | 174 | 0 | 282 | 271 | 3 | 315 | 0 | 0 | 33 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1782 | 0 | 1572 | 1736 | 0 | 0 |
| Q Serve（g＿s），s | 0.1 | 4.3 | 0.0 | 7.3 | 5.4 | 0.1 | 7.9 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.1 | 4.3 | 0.0 | 7.3 | 5.4 | 0.1 | 7.9 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.24 |  | 0.36 |
| Lane Grp Cap（c），veh／h | 10 | 270 |  | 361 | 639 | 546 | 429 | 0 |  | 64 | 0 | 0 |
| V／C Ratio（X） | 0.42 | 0.64 |  | 0.78 | 0.42 | 0.01 | 0.73 | 0.00 |  | 0.51 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 184 | 845 |  | 1079 | 1786 | 1526 | 1199 | 0 |  | 647 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 23.9 | 19.5 | 0.0 | 18.2 | 12.2 | 10.4 | 16.9 | 0.0 | 0.0 | 22.8 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 26.1 | 2.6 | 0.0 | 3.7 | 0.4 | 0.0 | 2.5 | 0.0 | 0.0 | 6.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.1 | 1.8 | 0.0 | 3.0 | 2.0 | 0.0 | 3.1 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 50.0 | 22.0 | 0.0 | 21.9 | 12.6 | 10.4 | 19.4 | 0.0 | 0.0 | 29.0 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | B | A |  | C | A | A |
| Approach Vol，veh／h |  | 178 |  |  | 556 |  |  | 315 |  |  | 33 |  |
| Approach Delay，s／veh |  | 22.7 |  |  | 17.3 |  |  | 19.4 |  |  | 29.0 |  |
| Approach LOS |  | C |  |  | B |  |  | B |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 14.4 | 11.5 | 6.3 | 4.8 | 21.1 | 16.1 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 29.5 | 22.0 | 18.0 | 5.0 | 46.5 | 32.5 |
| Max Q Clear Time（g＿c＋11），s | 9.3 | 6.3 | 2.9 | 2.1 | 7.4 | 9.9 |
| Green Ext Time（p＿c），s | 0.8 | 0.8 | 0.1 | 0.0 | 1.7 | 1.9 |

## Intersection Summary

| HCM 6th Ctrl Delay | 19.2 |
| :--- | ---: |
| HCM 6th LOS | B |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{7}$ |  |  | A | l | $\mathbf{7}$ |
| Traffic Vol, veh/h | 330 | 30 | 116 | 460 | 20 | 90 |
| Future Vol, veh/h | 330 | 30 | 116 | 460 | 20 | 90 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 359 | 33 | 126 | 500 | 22 | 98 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 0 | 199 | 313 | 196 | 135 | 3 |
| Future Vol, veh/h | 0 | 199 | 313 | 196 | 135 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 216 | 340 | 213 | 147 | 3 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 553 | 0 | - | 0 | 663 | 447 |
| $\quad$ Stage 1 | - | - | - | - | 447 | - |
| Stage 2 | - | - | - | - | 216 | - |
| Critical Hdwy | 4.12 | - | - | -6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | -5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1017 | - | - | - | 426 | 612 |
| $\quad$ Stage 1 | - | - | - | - | 644 | - |
| $\quad$ Stage 2 | - | - | - | - | 820 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1017 | - | - | - | 426 | 612 |
| Mov Cap-2 Maneuver | - | - | - | - | 426 | - |
| Stage 1 | - | - | - | - | 644 | - |
| Stage 2 | - | - | - | - | 820 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 17.8 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1017 | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | 4 | T | $\mathbf{T}$ |
| Traffic Vol, veh/h | 201 | 112 | 4 | 350 | 115 | 2 |
| Future Vol, veh/h | 201 | 112 | 4 | 350 | 115 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 218 | 122 | 4 | 380 | 125 | 2 |



|  | $\rangle$ |  |  | $\checkmark$ | 4 |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | ${ }^{7}$ | $\uparrow$ |  |  | \$ |  |  | \$ |  |
| Traffic Volume (veh/h) | 48 | 310 | 2 | 70 | 680 | 45 | 3 | 291 | 42 | 28 | 235 | 35 |
| Future Volume (veh/h) | 48 | 310 | 2 | 70 | 680 | 45 | 3 | 291 | 42 | 28 | 235 | 35 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 52 | 337 | 2 | 76 | 739 | 49 | 3 | 316 | 46 | 30 | 255 | 38 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 67 | 768 | 5 | 97 | 747 | 50 | 3 | 317 | 46 | 31 | 260 | 39 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.05 | 0.43 | 0.43 | 0.20 | 0.20 | 0.20 | 0.18 | 0.18 | 0.18 |
| Sat Flow, veh/h | 1781 | 1857 | 11 | 1781 | 1735 | 115 | 15 | 1583 | 230 | 169 | 1439 | 215 |
| Grp Volume(v), veh/h | 52 | 0 | 339 | 76 | 0 | 788 | 365 | 0 | 0 | 323 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1868 | 1781 | 0 | 1850 | 1828 | 0 | 0 | 1823 | 0 | 0 |
| Q Serve(g_s), s | 3.4 | 0.0 | 15.5 | 5.0 | 0.0 | 50.4 | 23.8 | 0.0 | 0.0 | 21.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 3.4 | 0.0 | 15.5 | 5.0 | 0.0 | 50.4 | 23.8 | 0.0 | 0.0 | 21.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 0.01 |  | 0.13 | 0.09 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 67 | 0 | 772 | 97 | 0 | 796 | 367 | 0 | 0 | 329 | 0 | 0 |
| VIC Ratio(X) | 0.78 | 0.00 | 0.44 | 0.78 | 0.00 | 0.99 | 1.00 | 0.00 | 0.00 | 0.98 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 79 | 0 | 772 | 184 | 0 | 796 | 367 | 0 | 0 | 329 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 56.9 | 0.0 | 25.0 | 55.6 | 0.0 | 33.7 | 47.6 | 0.0 | 0.0 | 48.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 32.7 | 0.0 | 0.4 | 12.7 | 0.0 | 29.2 | 45.7 | 0.0 | 0.0 | 44.6 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.2 | 0.0 | 6.9 | 2.6 | 0.0 | 28.4 | 15.4 | 0.0 | 0.0 | 13.6 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 89.6 | 0.0 | 25.4 | 68.3 | 0.0 | 62.9 | 93.3 | 0.0 | 0.0 | 93.2 | 0.0 | 0.0 |
| LnGrp LOS | F | A | C | E | A | E | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 391 |  |  | 864 |  |  | 365 |  |  | 323 |  |
| Approach Delay, s/veh |  | 34.0 |  |  | 63.4 |  |  | 93.3 |  |  | 93.2 |  |
| Approach LOS |  | C |  |  | E |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 11.0 | 53.8 |  | 26.0 | 9.0 | 55.8 |  | 28.4 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.3 | 44.3 |  | 21.5 | 5.3 | 51.3 |  | 23.9 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.0 | 17.5 |  | 23.0 | 5.4 | 52.4 |  | 25.8 |  |  |  |  |
| Green Ext Time (p_c), s | 0.1 | 2.1 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 68.1 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | 4 | F |  |
| Traffic Vol, veh/h | 2 | 24 | 61 | 118 | 150 | 7 |
| Future Vol, veh/h | 2 | 24 | 61 | 118 | 150 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 26 | 66 | 128 | 163 | 8 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.7 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 114 | 263 | 425 | 189 |
| Demand Flow Rate, veh/h | 116 | 269 | 433 | 192 |
| Vehicles Circulating, veh/h | 364 | 217 | 84 | 284 |
| Vehicles Exiting, veh/h | 112 | 300 | 396 | 201 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.0 | 5.6 | 6.1 | 5.3 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 116 | 269 | 433 | 192 |
| Cap Entry Lane, veh/h | 952 | 1106 | 1267 | 1033 |
| Entry HV Adj Factor | 0.982 | 0.977 | 0.981 | 0.984 |
| Flow Entry, veh/h | 114 | 263 | 425 | 189 |
| Cap Entry, veh/h | 935 | 1081 | 1243 | 1016 |
| VIC Ratio | 0.122 | 0.243 | 0.342 | 0.186 |
| Control Delay, s/veh | 5.0 | 5.6 | 6.1 | 5.3 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | 4 | F |  | 4 | 「' |  | \& |  |
| Traffic Volume (veh/h) | 15 | 291 | 373 | 215 | 209 | 7 | 266 | 12 | 243 | 6 | 8 | 7 |
| Future Volume (veh/h) | 15 | 291 | 373 | 215 | 209 | 7 | 266 | 12 | 243 | 6 | 8 | 7 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 16 | 300 | 0 | 222 | 215 | 8 | 274 | 13 | 0 | 7 | 9 | 8 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 36 | 418 |  | 289 | 684 | 584 | 373 | 18 |  | 14 | 19 | 16 |
| Arrive On Green | 0.02 | 0.23 | 0.00 | 0.16 | 0.37 | 0.37 | 0.22 | 0.22 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow, veh/h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1704 | 81 | 1572 | 508 | 653 | 580 |
| Grp Volume(v), veh/h | 16 | 300 | 0 | 222 | 215 | 8 | 287 | 0 | 0 | 24 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1785 | 0 | 1572 | 1741 | 0 | 0 |
| Q Serve(g_s), s | 0.4 | 7.4 | 0.0 | 5.9 | 4.1 | 0.2 | 7.4 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.4 | 7.4 | 0.0 | 5.9 | 4.1 | 0.2 | 7.4 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.95 |  | 1.00 | 0.29 |  | 0.33 |
| Lane Grp Cap(c), veh/h | 36 | 418 |  | 289 | 684 | 584 | 390 | 0 |  | 49 | 0 | 0 |
| V/C Ratio(X) | 0.45 | 0.72 |  | 0.77 | 0.31 | 0.01 | 0.74 | 0.00 |  | 0.49 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 195 | 1202 |  | 840 | 1881 | 1607 | 1030 | 0 |  | 634 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 23.9 | 17.7 | 0.0 | 19.8 | 11.1 | 9.9 | 18.0 | 0.0 | 0.0 | 23.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 8.7 | 2.3 | 0.0 | 4.3 | 0.3 | 0.0 | 2.7 | 0.0 | 0.0 | 7.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.3 | 3.0 | 0.0 | 2.5 | 1.5 | 0.0 | 3.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 32.6 | 20.0 | 0.0 | 24.1 | 11.4 | 9.9 | 20.7 | 0.0 | 0.0 | 30.8 | 0.0 | 0.0 |
| LnGrp LOS | C | C |  | C | B | A | C | A |  | C | A | A |
| Approach Vol, veh/h |  | 316 |  |  | 445 |  |  | 287 |  |  | 24 |  |
| Approach Delay, s/veh |  | 20.7 |  |  | 17.7 |  |  | 20.7 |  |  | 30.8 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 12.6 | 15.6 | 5.9 | 5.5 | 22.7 | 15.3 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time (g_c+11), s | 7.9 | 9.4 | 2.7 | 2.4 | 6.1 | 9.4 |
| Green Ext Time (p_c), s | 0.5 | 1.8 | 0.0 | 0.0 | 1.4 | 1.6 |

## Intersection Summary

| HCM 6th Ctrl Delay | 19.7 |
| :--- | ---: |
| HCM 6th LOS | B |

## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | A | 1 | 「 |
| Traffic Vol, veh/h | 538 | 33 | 97 | 386 | 22 | 137 |
| Future Vol, veh/h | 538 | 33 | 97 | 386 | 22 | 137 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 585 | 36 | 105 | 420 | 24 | 149 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\mathbf{F}$ |  | M |  |
| Traffic Vol, veh/h | 1 | 355 | 223 | 179 | 229 | 1 |
| Future Vol, veh/h | 1 | 355 | 223 | 179 | 229 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 386 | 242 | 195 | 249 | 1 |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 437 | 0 | - | 0 | 728 | 340 |  |
| Stage 1 | - | - | - | - | 340 | - |  |
| Stage 2 | - | - | - | - | 388 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | 1123 | - | - | - | 390 | 702 |  |
| $\quad$ Stage 1 | - | - | - | - | 721 | - |  |
| Stage 2 | - | - | - | - | 686 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1123 | - | - | - | 390 | 702 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 390 | - |  |
| Stage 1 | - | - | - | - | 720 | - |  |
| Stage 2 | - | - | - | - | 686 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 29.2 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1123 | - | - | - | 391 |
| HCM Lane V/C Ratio | 0.001 | - | - | -0.639 |  |
| HCM Control Delay (s) | 8.2 | 0 | - | - | 29.2 |
| HCM Lane LOS | A | A | - | - | D |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 4.3 |



| Major/Minor | Major1 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Major2 |  | Minor1 |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 582 | 0 | 765 | 493 |
| $\quad$ Stage 1 | - | - | - | - | 493 | - |
| Stage 2 | - | - | - | - | 272 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | - | - | 992 | - | 371 | 576 |
| $\quad$ Stage 1 | - | - | - | - | 614 | - |
| Stage 2 | - | - | - | - | 774 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 992 | - | 371 | 576 |
| Mov Cap-2 Maneuver | - | - | - | - | 371 | - |
| Stage 1 | - | - | - | - | 614 | - |
| Stage 2 | - | - | - | - | 773 | - |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F |  | ${ }^{7}$ | F |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 35 | 660 | 6 | 70 | 437 | 37 | 6 | 304 | 102 | 47 | 294 | 46 |
| Future Volume (veh/h) | 35 | 660 | 6 | 70 | 437 | 37 | 6 | 304 | 102 | 47 | 294 | 46 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 38 | 717 | 7 | 76 | 475 | 40 | 7 | 330 | 111 | 51 | 320 | 50 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 53 | 701 | 7 | 82 | 672 | 57 | 6 | 291 | 98 | 45 | 283 | 44 |
| Arrive On Green | 0.03 | 0.38 | 0.38 | 0.05 | 0.40 | 0.40 | 0.22 | 0.22 | 0.22 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1849 | 18 | 1781 | 1701 | 143 | 28 | 1318 | 443 | 221 | 1384 | 216 |
| Grp Volume(v), veh/h | 38 | 0 | 724 | 76 | 0 | 515 | 448 | 0 | 0 | 421 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 0 | 1845 | 1789 | 0 | 0 | 1820 | 0 | 0 |
| Q Serve(g_s), s | 2.5 | 0.0 | 45.5 | 5.1 | 0.0 | 28.1 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.5 | 0.0 | 45.5 | 5.1 | 0.0 | 28.1 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.02 |  | 0.25 | 0.12 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 53 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| V/C Ratio(X) | 0.71 | 0.00 | 1.02 | 0.93 | 0.00 | 0.71 | 1.13 | 0.00 | 0.00 | 1.13 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.7 | 0.0 | 37.3 | 57.1 | 0.0 | 30.5 | 46.8 | 0.0 | 0.0 | 47.8 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 16.3 | 0.0 | 39.7 | 76.5 | 0.0 | 3.1 | 87.0 | 0.0 | 0.0 | 87.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 0.0 | 28.1 | 4.0 | 0.0 | 13.0 | 21.2 | 0.0 | 0.0 | 20.1 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 74.0 | 0.0 | 76.9 | 133.6 | 0.0 | 33.6 | 133.7 | 0.0 | 0.0 | 135.6 | 0.0 | 0.0 |
| LnGrp LOS | E | A | F | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 762 |  |  | 591 |  |  | 448 |  |  | 421 |  |
| Approach Delay, s/veh |  | 76.8 |  |  | 46.5 |  |  | 133.7 |  |  | 135.6 |  |
| Approach LOS |  | E |  |  | D |  |  | F |  |  | F |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 10.0 | 50.0 | 29.0 | 8.1 | 51.9 | 31.0 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 5.5 | 45.5 | 24.5 | 5.1 | 45.9 | 26.5 |
| Max Q Clear Time (g_c+11), s | 7.1 | 47.5 | 26.5 | 4.5 | 30.1 | 28.5 |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 0.0 | 3.0 | 0.0 |

## Intersection Summary

HCM 6th Ctrl Delay 91.3

HCM 6th LOS F

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  | 1 | 个 | 言 |  |
| Traffic Vol, veh/h | 11 | 71 | 16 | 126 | 83 | 2 |
| Future Vol, veh/h | 11 | 71 | 16 | 126 | 83 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 77 | 17 | 137 | 90 | 2 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.0 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 79 | 259 | 293 | 177 |
| Demand Flow Rate, veh/h | 81 | 263 | 299 | 180 |
| Vehicles Circulating, veh/h | 339 | 163 | 55 | 275 |
| Vehicles Exiting, veh/h | 116 | 191 | 365 | 151 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.5 | 5.2 | 4.8 | 5.1 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR |  | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 2.600 |
| Follow-Up Headway, s | 2.609 | 2.609 | 4.609 | 4.976 |
| Critical Headway, s | 4.976 | 4.976 | 180 |  |
| Entry Flow, veh/h | 81 | 263 | 299 | 1042 |
| Cap Entry Lane, veh/h | 977 | 1169 | 1305 | 0.984 |
| Entry HV Adj Factor | 0.981 | 0.984 | 0.979 | 177 |
| Flow Entry, veh/h | 79 | 259 | 293 | 1025 |
| Cap Entry, veh/h | 958 | 1149 | 1277 | 0.173 |
| V/C Ratio | 0.083 | 0.225 | 0.229 | A |
| Control Delay, s/veh | 4.5 | 5.2 | 4.8 | A |
| LOS | A | 1 | 1 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | $\uparrow$ | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 2 | 29 | 19 | 285 | 319 | 3 |
| Future Vol, veh/h | 2 | 29 | 19 | 285 | 319 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 32 | 21 | 310 | 347 | 3 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | \% | * | $\uparrow$ | F |  | $\uparrow$ | 「 |  | ¢ |  |
| Traffic Volume (veh/h) | 4 | 190 | 247 | 277 | 284 | 3 | 302 | 4 | 167 | 7 | 12 | 11 |
| Future Volume (veh/h) | 4 | 190 | 247 | 277 | 284 | 3 | 302 | 4 | 167 | 7 | 12 | 11 |
| Initial $Q(Q b)$, veh | , | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 4 | 196 | 0 | 286 | 293 | 3 | 311 | 4 | 0 | 8 | 13 | 12 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 10 | 292 |  | 363 | 663 | 567 | 420 | 5 |  | 15 | 25 | 23 |
| Arrive On Green | 0.01 | 0.16 | 0.00 | 0.21 | 0.36 | 0.36 | 0.24 | 0.24 | 0.00 | 0.04 | 0.04 | 0.04 |
| Sat Flow, veh/h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1760 | 23 | 1572 | 421 | 684 | 631 |
| Grp Volume(v), veh/h | 4 | 196 | 0 | 286 | 293 | 3 | 315 | 0 | 0 | 33 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1782 | 0 | 1572 | 1736 | 0 | 0 |
| Q Serve(g_s), s | 0.1 | 5.0 | 0.0 | 7.6 | 6.0 | 0.1 | 8.1 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.1 | 5.0 | 0.0 | 7.6 | 6.0 | 0.1 | 8.1 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.24 |  | 0.36 |
| Lane Grp Cap(c), veh/h | 10 | 292 |  | 363 | 663 | 567 | 426 | 0 |  | 64 | 0 | 0 |
| V/C Ratio(X) | 0.42 | 0.67 |  | 0.79 | 0.44 | 0.01 | 0.74 | 0.00 |  | 0.52 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 179 | 820 |  | 1047 | 1733 | 1480 | 1163 | 0 |  | 627 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 24.7 | 19.8 | 0.0 | 18.7 | 12.2 | 10.3 | 17.5 | 0.0 | 0.0 | 23.5 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 26.1 | 2.7 | 0.0 | 3.8 | 0.5 | 0.0 | 2.5 | 0.0 | 0.0 | 6.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 2.1 | 0.0 | 3.1 | 2.2 | 0.0 | 3.2 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 50.8 | 22.5 | 0.0 | 22.5 | 12.7 | 10.3 | 20.1 | 0.0 | 0.0 | 29.9 | 0.0 | 0.0 |


| LnGrp LOS | D | C | C | B | B | C | A | C |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Vol, veh/h | 200 | 582 |  | 315 | A |  |  |  |
| Approach Delay, s/veh | 23.0 | 17.5 |  | 20.1 | 33 |  |  |  |
| Approach LOS | C |  | B |  | C | 29.9 |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 14.7 | 12.3 | 6.3 | 4.8 | 22.3 | 16.4 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$, s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 29.5 | 22.0 | 18.0 | 5.0 | 46.5 | 32.5 |
| Max Q Clear Time (g_c+11), s | 9.6 | 7.0 | 2.9 | 2.1 | 8.0 | 10.1 |
| Green Ext Time (p_c), s | 0.8 | 0.9 | 0.1 | 0.0 | 1.9 | 1.9 |

## Intersection Summary

| HCM 6th Ctrl Delay | 19.6 |
| :--- | ---: |
| HCM 6th LOS | $B$ |

## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | A | l | $\mathbf{7}$ |
| Traffic Vol, veh/h | 343 | 30 | 124 | 473 | 20 | 98 |
| Future Vol, veh/h | 343 | 30 | 124 | 473 | 20 | 98 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 373 | 33 | 135 | 514 | 22 | 107 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 0 | 208 | 322 | 200 | 139 | 3 |
| Future Vol, veh/h | 0 | 208 | 322 | 200 | 139 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 226 | 350 | 217 | 151 | 3 |


| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 567 | 0 | - | 0 | 685 | 459 |  |
| $\quad$ Stage 1 | - | - | - | - | 459 | - |  |
| Stage 2 | - | - | - | - | 226 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1005 | - | - | - | 414 | 602 |  |
| $\quad$ Stage 1 | - | - | - | - | 636 | - |  |
| Stage 2 | - | - | - | - | 812 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1005 | - | - | - | 414 | 602 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 414 | - |  |
| Stage 1 | - | - | - | - | 636 | - |  |
| Stage 2 | - | - | - | - | 812 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 18.6 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1005 | - | - | - | 417 |
| HCM Lane V/C Ratio | - | - | - | - | 0.37 |
| HCM Control Delay (s) | 0 | - | - | -18.6 |  |
| HCM Lane LOS | A | - | - | - | C |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 1.7 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | 4 | T | $\mathbf{T}$ |
| Traffic Vol, veh/h | 210 | 112 | 4 | 359 | 115 | 2 |
| Future Vol, veh/h | 210 | 112 | 4 | 359 | 115 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 228 | 122 | 4 | 390 | 125 | 2 |



|  | $\rangle$ |  |  | $\dagger$ |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{}$ |  | ${ }^{7}$ | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 48 | 317 | 2 | 71 | 687 | 46 | 3 | 291 | 43 | 29 | 235 | 35 |
| Future Volume (veh/h) | 48 | 317 | 2 | 71 | 687 | 46 | 3 | 291 | 43 | 29 | 235 | 35 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 52 | 345 | 2 | 77 | 747 | 50 | 3 | 316 | 47 | 32 | 255 | 38 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 67 | 767 | 4 | 98 | 746 | 50 | 3 | 316 | 47 | 32 | 258 | 38 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.06 | 0.43 | 0.43 | 0.20 | 0.20 | 0.20 | 0.18 | 0.18 | 0.18 |
| Sat Flow, veh/h | 1781 | 1858 | 11 | 1781 | 1733 | 116 | 15 | 1578 | 235 | 179 | 1430 | 213 |
| Grp Volume(v), veh/h | 52 | 0 | 347 | 77 | 0 | 797 | 366 | 0 | 0 | 325 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1868 | 1781 | 0 | 1849 | 1827 | 0 | 0 | 1823 | 0 | 0 |
| Q Serve(g_s), s | 3.4 | 0.0 | 16.0 | 5.1 | 0.0 | 51.3 | 23.9 | 0.0 | 0.0 | 21.2 | 0.0 | 0.0 |
| Cycle Q Clear (g_c), s | 3.4 | 0.0 | 16.0 | 5.1 | 0.0 | 51.3 | 23.9 | 0.0 | 0.0 | 21.2 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 0.01 |  | 0.13 | 0.10 |  | 0.12 |
| Lane Grp Cap (c), veh/h | 67 | 0 | 771 | 98 | 0 | 796 | 366 | 0 | 0 | 329 | 0 | 0 |
| V/C Ratio(X) | 0.78 | 0.00 | 0.45 | 0.78 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 79 | 0 | 771 | 184 | 0 | 796 | 366 | 0 | 0 | 329 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 56.9 | 0.0 | 25.2 | 55.6 | 0.0 | 33.9 | 47.6 | 0.0 | 0.0 | 48.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 32.7 | 0.0 | 0.4 | 12.6 | 0.0 | 32.2 | 46.6 | 0.0 | 0.0 | 46.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 2.2 | 0.0 | 7.1 | 2.6 | 0.0 | 29.4 | 15.5 | 0.0 | 0.0 | 13.8 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 89.6 | 0.0 | 25.6 | 68.2 | 0.0 | 66.1 | 94.3 | 0.0 | 0.0 | 95.0 | 0.0 | 0.0 |
| LnGrp LOS | F | A | C | E | A | F | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 399 |  |  | 874 |  |  | 366 |  |  | 325 |  |
| Approach Delay, s/veh |  | 34.0 |  |  | 66.3 |  |  | 94.3 |  |  | 95.0 |  |
| Approach LOS |  | C |  |  | E |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 11.1 | 53.7 |  | 26.0 | 9.0 | 55.8 |  | 28.4 |  |  |  |  |
| Change Period ( $Y+R \mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.3 | 44.3 |  | 21.5 | 5.3 | 51.3 |  | 23.9 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.1 | 18.0 |  | 23.2 | 5.4 | 53.3 |  | 25.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.1 | 2.2 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 69.7 |  |  |  |  |  |  |  |  |  |
|  |  |  | E |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | A | F |  |
| Traffic Vol, veh/h | 2 | 24 | 61 | 136 | 165 | 7 |
| Future Vol, veh/h | 2 | 24 | 61 | 136 | 165 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 26 | 66 | 148 | 179 | 8 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.9 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 115 | 264 | 447 | 205 |
| Demand Flow Rate, veh/h | 117 | 270 | 457 | 208 |
| Vehicles Circulating, veh/h | 381 | 238 | 84 | 286 |
| Vehicles Exiting, veh/h | 113 | 303 | 414 | 221 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.1 | 5.8 | 6.3 | 5.5 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR |  |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 4.909 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 208 |
| Entry Flow, veh/h | 117 | 270 | 457 | 1031 |
| Cap Entry Lane, veh/h | 936 | 1082 | 1267 | 0.983 |
| Entry HV Adj Factor | 0.982 | 0.977 | 0.979 | 205 |
| Flow Entry, veh/h | 115 | 264 | 447 | 1014 |
| Cap Entry, veh/h | 919 | 1058 | 1240 | 0.202 |
| V/C Ratio | 0.125 | 0.249 | 0.361 | 5 |
| Control Delay, s/veh | 5.1 | 5.8 | 6.3 | A |
| LOS | A | 1 | 2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | $\uparrow$ | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 0 | 37 | 34 | 405 | 379 | 1 |
| Future Vol, veh/h | 0 | 37 | 34 | 405 | 379 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 40 | 37 | 440 | 412 | 1 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 4 | 「 | ＊ | 4 | 「 |  | $\uparrow$ | 「 |  | ¢ |  |
| Traffic Volume（veh／h） | 15 | 332 | 373 | 222 | 259 | 7 | 266 | 12 | 249 | 6 | 8 | 7 |
| Future Volume（veh／h） | 15 | 332 | 373 | 222 | 259 | 7 | 266 | 12 | 249 | 6 | 8 | 7 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 16 | 342 | 0 | 229 | 267 | 8 | 274 | 13 | 0 | 7 | 9 | 8 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 35 | 458 |  | 295 | 730 | 624 | 367 | 17 |  | 14 | 18 | 16 |
| Arrive On Green | 0.02 | 0.25 | 0.00 | 0.17 | 0.39 | 0.39 | 0.22 | 0.22 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1704 | 81 | 1572 | 508 | 653 | 580 |
| Grp Volume（v），veh／h | 16 | 342 | 0 | 229 | 267 | 8 | 287 | 0 | 0 | 24 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1785 | 0 | 1572 | 1741 | 0 | 0 |
| Q Serve（g＿s），s | 0.5 | 8.9 | 0.0 | 6.5 | 5.3 | 0.2 | 7.9 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.5 | 8.9 | 0.0 | 6.5 | 5.3 | 0.2 | 7.9 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.95 |  | 1.00 | 0.29 |  | 0.33 |
| Lane Grp Cap（c），veh／h | 35 | 458 |  | 295 | 730 | 624 | 385 | 0 |  | 49 | 0 | 0 |
| V／C Ratio（X） | 0.45 | 0.75 |  | 0.78 | 0.37 | 0.01 | 0.75 | 0.00 |  | 0.49 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 183 | 1132 |  | 791 | 1772 | 1513 | 970 | 0 |  | 597 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 25.4 | 18.3 | 0.0 | 20.9 | 11.3 | 9.7 | 19.2 | 0.0 | 0.0 | 25.1 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 8.8 | 2.5 | 0.0 | 4.4 | 0.3 | 0.0 | 2.9 | 0.0 | 0.0 | 7.4 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.3 | 3.7 | 0.0 | 2.8 | 1.9 | 0.0 | 3.2 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 34.2 | 20.7 | 0.0 | 25.4 | 11.6 | 9.7 | 22.1 | 0.0 | 0.0 | 32.5 | 0.0 | 0.0 |
| LnGrp LOS | C | C |  | C | B | A | C | A |  | C | A | A |
| Approach Vol，veh／h |  | 358 |  |  | 504 |  |  | 287 |  |  | 24 |  |
| Approach Delay，s／veh |  | 21.3 |  |  | 17.8 |  |  | 22.1 |  |  | 32.5 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 13.2 | 17.4 | 6.0 | 5.5 | 25.1 | 15.8 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 8.5 | 10.9 | 2.7 | 2.5 | 7.3 | 9.9 |
| Green Ext Time（p＿c），s | 0.6 | 2.0 | 0.0 | 0.0 | 1.7 | 1.6 |

## Intersection Summary

| HCM 6th Ctrl Delay | 20.2 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | A | 1 | 「 |
| Traffic Vol, veh/h | 562 | 33 | 117 | 416 | 22 | 154 |
| Future Vol, veh/h | 562 | 33 | 117 | 416 | 22 | 154 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 611 | 36 | 127 | 452 | 24 | 167 |



| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 7.9 |  |  |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations |  | ${ }_{*} 1$ | 个 |  | M |  |  |
| Traffic Vol, veh/h | 1 | 372 | 245 | 187 | 236 | 1 |  |
| Future Vol, veh/h | 1 | 372 | 245 | 187 | 236 | 1 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - | - |
| Grade, \% | - | 0 | 0 | - | 0 | - | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 404 | 266 | 203 | 257 | 1 |  |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 469 | 0 | - | 0 | 774 | 368 |
| Stage 1 | - | - | - | - | 368 | - |
| Stage 2 | - | - | - | - | 406 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1093 | - | - | - | 367 | 677 |
| Stage 1 | - | - | - | - | 700 | - |
| Stage 2 | - | - | - | - | 673 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1093 | - | - | - | 367 | 677 |
| Mov Cap-2 Maneuver | - | - | - | - | 367 | - |
| Stage 1 | - | - | - | - | 699 | - |
| Stage 2 | - | - | - | - | 673 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 34.7 |  |
| HCM LOS |  |  |  |  | D |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1093 | - | - | - | 368 |
| HCM Lane V/C Ratio |  | 0.001 | - | - | - | 0.7 |
| HCM Control Delay (s) |  | 8.3 | 0 | - | - | 34.7 |
| HCM Lane LOS |  | A | A | - | - | D |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 5.1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | 4 | T | $\mathbf{T}$ |
| Traffic Vol, veh/h | 389 | 164 | 1 | 270 | 128 | 1 |
| Future Vol, veh/h | 389 | 164 | 1 | 270 | 128 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 423 | 178 | 1 | 293 | 139 | 1 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor1 |  |  |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 601 | 0 | 807 | 512 |
| $\quad$ Stage 1 | - | - | - | - | 512 | - |
| Stage 2 | - | - | - | - | 295 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 976 | - | 351 | 562 |
| $\quad$ Stage 1 | - | - | - | - | 602 | - |
| Stage 2 | - | - | - | - | 755 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 976 | - | 351 | 562 |
| Mov Cap-2 Maneuver | - | - | - | - | 351 | - |
| Stage 1 | - | - | - | - | 602 | - |
| Stage 2 | - | - | - | - | 754 | - |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 21.7 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 351 | 562 | - | - | 976 | - |
| HCM Lane V/C Ratio | 0.396 | 0.002 | - | -0.001 | - |  |
| HCM Control Delay (s) | 21.8 | 11.4 | - | - | 8.7 | - |
| HCM Lane LOS | C | B | - | - | A | - |
| HCM 95th \%tile Q(veh) | 1.8 | 0 | - | - | 0 | - |


|  | $\rangle$ | $\rightarrow$ |  | 7 |  |  | 4 | $\uparrow$ |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\square}$ |  | * | $\uparrow$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 35 | 674 | 6 | 73 | 454 | 39 | 6 | 304 | 104 | 48 | 294 | 46 |
| Future Volume (veh/h) | 35 | 674 | 6 | 73 | 454 | 39 | 6 | 304 | 104 | 48 | 294 | 46 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 38 | 733 | 7 | 79 | 493 | 42 | 7 | 330 | 113 | 52 | 320 | 50 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 53 | 701 | 7 | 82 | 671 | 57 | 6 | 290 | 99 | 46 | 282 | 44 |
| Arrive On Green | 0.03 | 0.38 | 0.38 | 0.05 | 0.40 | 0.40 | 0.22 | 0.22 | 0.22 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1850 | 18 | 1781 | 1700 | 145 | 28 | 1311 | 449 | 224 | 1380 | 216 |
| Grp Volume(v), veh/h | 38 | 0 | 740 | 79 | 0 | 535 | 450 | 0 | 0 | 422 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1867 | 1781 | 0 | 1844 | 1788 | 0 | 0 | 1820 | 0 | 0 |
| Q Serve(g_s), s | 2.5 | 0.0 | 45.5 | 5.3 | 0.0 | 29.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.5 | 0.0 | 45.5 | 5.3 | 0.0 | 29.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.02 |  | 0.25 | 0.12 |  | 0.12 |
| Lane Grp Cap(c), veh/h | 53 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| V/C Ratio(X) | 0.71 | 0.00 | 1.05 | 0.97 | 0.00 | 0.73 | 1.14 | 0.00 | 0.00 | 1.14 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 0 | 708 | 82 | 0 | 729 | 395 | 0 | 0 | 372 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.7 | 0.0 | 37.3 | 57.2 | 0.0 | 30.9 | 46.8 | 0.0 | 0.0 | 47.8 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 16.3 | 0.0 | 46.2 | 88.5 | 0.0 | 3.9 | 89.1 | 0.0 | 0.0 | 88.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 0.0 | 29.4 | 4.4 | 0.0 | 13.8 | 21.5 | 0.0 | 0.0 | 20.2 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 74.0 | 0.0 | 83.5 | 145.6 | 0.0 | 34.8 | 135.8 | 0.0 | 0.0 | 136.6 | 0.0 | 0.0 |
| LnGrp LOS | E | A | F | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 778 |  |  | 614 |  |  | 450 |  |  | 422 |  |
| Approach Delay, s/veh |  | 83.0 |  |  | 49.0 |  |  | 135.8 |  |  | 136.6 |  |
| Approach LOS |  | F |  |  | D |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 10.0 | 50.0 |  | 29.0 | 8.1 | 51.9 |  | 31.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.5 | 45.5 |  | 24.5 | 5.1 | 45.9 |  | 26.5 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.3 | 47.5 |  | 26.5 | 4.5 | 31.7 |  | 28.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 |  | 0.0 | 0.0 | 3.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 94.3 |  |  |  |  |  |  |  |  |  |
|  |  |  | F |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | 4 | b |  |
| Traffic Vol, veh/h | 12 | 77 | 17 | 128 | 81 | 2 |
| Future Vol, veh/h | 12 | 77 | 17 | 128 | 81 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 84 | 18 | 139 | 88 | 2 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.1 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 85 | 279 | 307 | 182 |
| Demand Flow Rate, veh/h | 87 | 284 | 313 | 185 |
| Vehicles Circulating, veh/h | 355 | 168 | 59 | 297 |
| Vehicles Exiting, veh/h | 127 | 204 | 383 | 155 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.7 | 5.4 | 4.9 | 5.3 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 87 | 284 | 313 | 185 |
| Cap Entry Lane, veh/h | 961 | 1163 | 1299 | 1019 |
| Entry HV Adj Factor | 0.982 | 0.981 | 0.980 | 0.984 |
| Flow Entry, veh/h | 85 | 279 | 307 | 182 |
| Cap Entry, veh/h | 943 | 1140 | 1273 | 1003 |
| VIC Ratio | 0.091 | 0.244 | 0.241 | 0.182 |
| Control Delay, s/veh | 4.7 | 5.4 | 4.9 | 5.3 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ |  |  | ¢ |  |  | $\dagger$ |  |  |
| Traffic Vol, veh/h | 3 | 0 | 92 | 3 | 1 | 1 | 87 | 304 | 0 | , | 374 | 4 |  |
| Future Vol, veh/h | 3 | 0 | 92 | 3 | 1 | 1 | 87 | 304 | 0 | 1 | 374 | 4 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 3 | 0 | 100 | 3 | 1 | 1 | 95 | 330 | 0 | 1 | 407 | 4 |  |







| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | 「 | 7 | 4 | F |  | $\uparrow$ | F |  | \$ |  |
| Traffic Volume (veh/h) | 4 | 182 | 266 | 295 | 283 | 3 | 325 | 4 | 177 | 8 | 13 | 12 |
| Future Volume (veh/h) | 4 | 182 | 266 | 295 | 283 | 3 | 325 | 4 | 177 | 8 | 13 | 12 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 4 | 188 | 0 | 304 | 292 | 3 | 335 | 4 | 0 | 9 | 14 | 13 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 10 | 278 |  | 380 | 667 | 570 | 443 | 5 |  | 17 | 26 | 24 |
| Arrive On Green | 0.01 | 0.15 | 0.00 | 0.22 | 0.36 | 0.36 | 0.25 | 0.25 | 0.00 | 0.04 | 0.04 | 0.04 |
| Sat Flow, veh/h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1761 | 21 | 1572 | 434 | 675 | 627 |
| Grp Volume(v), veh/h | 4 | 188 | 0 | 304 | 292 | 3 | 339 | 0 | 0 | 36 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1782 | 0 | 1572 | 1736 | 0 | 0 |
| Q Serve(g_s), s | 0.1 | 5.0 | 0.0 | 8.5 | 6.3 | 0.1 | 9.2 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.1 | 5.0 | 0.0 | 8.5 | 6.3 | 0.1 | 9.2 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.25 |  | 0.36 |
| Lane Grp Cap(c), veh/h | 10 | 278 |  | 380 | 667 | 570 | 449 | 0 |  | 68 | 0 | 0 |
| V/C Ratio(X) | 0.42 | 0.68 |  | 0.80 | 0.44 | 0.01 | 0.76 | 0.00 |  | 0.53 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 170 | 781 |  | 998 | 1651 | 1410 | 1108 | 0 |  | 598 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 25.9 | 21.0 | 0.0 | 19.4 | 12.7 | 10.7 | 18.1 | 0.0 | 0.0 | 24.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 26.2 | 2.9 | 0.0 | 3.9 | 0.5 | 0.0 | 2.6 | 0.0 | 0.0 | 6.4 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 2.2 | 0.0 | 3.5 | 2.3 | 0.0 | 3.7 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 52.1 | 23.9 | 0.0 | 23.4 | 13.2 | 10.7 | 20.7 | 0.0 | 0.0 | 31.0 | 0.0 | 0.0 |


| LnGrp LOS | D | C | C | B | B | C | A | C |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Vol, veh/h | 192 | 599 |  | 339 | A |  |  |  |
| Approach Delay, s/veh | 24.5 | 18.3 |  | 20.7 | 31.0 |  |  |  |
| Approach LOS | C | B |  | C | C |  |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 15.7 | 12.3 | 6.5 | 4.8 | 23.3 | 17.7 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 29.5 | 22.0 | 18.0 | 5.0 | 46.5 | 32.5 |
| Max Q Clear Time (g_c+11), s | 10.5 | 7.0 | 3.1 | 2.1 | 8.3 | 11.2 |
| Green Ext Time (p_c), s | 0.9 | 0.8 | 0.1 | 0.0 | 1.9 | 2.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 20.4 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  | 1 | 个 | t | $\mathbf{7}$ |
| Traffic Vol, veh/h | 356 | 32 | 125 | 496 | 22 | 97 |
| Future Vol, veh/h | 356 | 32 | 125 | 496 | 22 | 97 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 387 | 35 | 136 | 539 | 24 | 105 |




| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 595 | 0 | - | 0 | 714 | 481 |  |
| Stage 1 | - | - | - | - | 481 | - |  |
| Stage 2 | - | - | - | - | 233 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 981 | - | - | - | 398 | 585 |  |
| $\quad$ Stage 1 | - | - | - | - | 622 | - |  |
| Stage 2 | - | - | - | - | 806 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 981 | - | - | - | 398 | 585 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 398 | - |  |
| Stage 1 | - | - | - | - | 622 | - |  |
| Stage 2 | - | - | - | - | 806 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 19.7 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 981 | - | - | - | 398 | 585 |
| HCM Lane V/C Ratio | - | - | - | -0.396 | 0.006 |  |
| HCM Control Delay (s) | 0 | - | - | - | 19.9 | 11.2 |
| HCM Lane LOS | A | - | - | - | C | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 1.9 | 0 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  | 1 | 4 | T | $\mathbf{7}$ |
| Traffic Vol, veh/h | 217 | 121 | 4 | 377 | 124 | 2 |
| Future Vol, veh/h | 217 | 121 | 4 | 377 | 124 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 236 | 132 | 4 | 410 | 135 | 2 |



|  | $\rangle$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  | ${ }_{7}$ | ¢个 | 「 | ${ }_{1}$ | 个个 | 「 |
| Traffic Volume（veh／h） | 52 | 334 | 2 | 75 | 733 | 48 | 3 | 314 | 45 | 30 | 253 | 38 |
| Future Volume（veh／h） | 52 | 334 | 2 | 75 | 733 | 48 | 3 | 314 | 45 | 30 | 253 | 38 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 57 | 363 | 2 | 82 | 797 | 52 | 3 | 341 | 49 | 33 | 275 | 41 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 81 | 946 | 5 | 107 | 909 | 59 | 114 | 487 | 217 | 114 | 487 | 217 |
| Arrive On Green | 0.05 | 0.51 | 0.51 | 0.06 | 0.52 | 0.52 | 0.06 | 0.14 | 0.14 | 0.06 | 0.14 | 0.14 |
| Sat Flow，veh／h | 1781 | 1858 | 10 | 1781 | 1737 | 113 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 57 | 0 | 365 | 82 | 0 | 849 | 3 | 341 | 49 | 33 | 275 | 41 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1869 | 1781 | 0 | 1850 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 2.5 | 0.0 | 9.3 | 3.5 | 0.0 | 31.6 | 0.1 | 7.2 | 2.2 | 1.4 | 5.7 | 1.8 |
| Cycle Q Clear（g＿c），s | 2.5 | 0.0 | 9.3 | 3.5 | 0.0 | 31.6 | 0.1 | 7.2 | 2.2 | 1.4 | 5.7 | 1.8 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 81 | 0 | 951 | 107 | 0 | 968 | 114 | 487 | 217 | 114 | 487 | 217 |
| V／C Ratio（X） | 0.70 | 0.00 | 0.38 | 0.77 | 0.00 | 0.88 | 0.03 | 0.70 | 0.23 | 0.29 | 0.56 | 0.19 |
| Avail Cap（c＿a），veh／h | 125 | 0 | 1273 | 280 | 0 | 1422 | 410 | 832 | 371 | 412 | 836 | 373 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 36.8 | 0.0 | 11.7 | 36.2 | 0.0 | 16.4 | 34.3 | 32.2 | 30.0 | 34.9 | 31.6 | 29.9 |
| Incr Delay（d2），s／veh | 10.6 | 0.0 | 0.3 | 11.0 | 0.0 | 4.5 | 0.1 | 1.8 | 0.5 | 1.4 | 1.0 | 0.4 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.3 | 0.0 | 3.6 | 1.8 | 0.0 | 12.9 | 0.1 | 3.1 | 0.8 | 0.6 | 2.4 | 0.7 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 47.4 | 0.0 | 12.0 | 47.2 | 0.0 | 20.9 | 34.4 | 34.0 | 30.6 | 36.3 | 32.6 | 30.3 |
| LnGrp LOS | D | A | B | D | A | C | C | C | C | D | C | C |
| Approach Vol，veh／h |  | 422 |  |  | 931 |  |  | 393 |  |  | 349 |  |
| Approach Delay，s／veh |  | 16.8 |  |  | 23.2 |  |  | 33.6 |  |  | 32.7 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 9.2 | 44.3 | 9.5 | 15.2 | 8.1 | 45.4 | 9.5 | 15.2 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 12.3 | 53.3 | 18.0 | 18.4 | 5.5 | 60.1 | 18.1 | 18.3 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 5.5 | 11.3 | 2.1 | 7.7 | 4.5 | 33.6 | 3.4 | 9.2 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.1 | 2.5 | 0.0 | 1.3 | 0.0 | 7.3 | 0.0 | 1.6 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 25.5 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y |  |  | 4 | b |  |
| Traffic Vol, veh/h | 2 | 26 | 66 | 127 | 162 | 8 |
| Future Vol, veh/h | 2 | 26 | 66 | 127 | 162 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 28 | 72 | 138 | 176 | 9 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 6.0 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 123 | 284 | 457 | 202 |
| Demand Flow Rate, veh/h | 125 | 290 | 466 | 205 |
| Vehicles Circulating, veh/h | 390 | 233 | 91 | 306 |
| Vehicles Exiting, veh/h | 121 | 324 | 424 | 217 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.2 | 5.9 | 6.5 | 5.6 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 125 | 290 | 466 | 205 |
| Cap Entry Lane, veh/h | 927 | 1088 | 1258 | 1010 |
| Entry HV Adj Factor | 0.982 | 0.979 | 0.980 | 0.984 |
| Flow Entry, veh/h | 123 | 284 | 457 | 202 |
| Cap Entry, veh/h | 911 | 1065 | 1232 | 993 |
| VIC Ratio | 0.135 | 0.267 | 0.371 | 0.203 |
| Control Delay, s/veh | 5.2 | 5.9 | 6.5 | 5.6 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | $\uparrow$ | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 0 | 40 | 37 | 414 | 390 | 1 |
| Future Vol, veh/h | 0 | 40 | 37 | 414 | 390 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 43 | 40 | 450 | 424 | 1 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | \＄ |  |
| Traffic Volume（veh／h） | 16 | 314 | 402 | 232 | 225 | 8 | 287 | 13 | 262 | 6 | 9 | 8 |
| Future Volume（veh／h） | 16 | 314 | 402 | 232 | 225 | 8 | 287 | 13 | 262 | 6 | 9 | 8 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 17 | 324 | 0 | 239 | 232 | 9 | 296 | 14 | 0 | 7 | 10 | 9 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 37 | 435 |  | 305 | 716 | 611 | 390 | 18 |  | 14 | 20 | 18 |
| Arrive On Green | 0.02 | 0.23 | 0.00 | 0.17 | 0.39 | 0.39 | 0.23 | 0.23 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1705 | 81 | 1572 | 468 | 669 | 602 |
| Grp Volume（v），veh／h | 17 | 324 | 0 | 239 | 232 | 9 | 310 | 0 | 0 | 26 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1785 | 0 | 1572 | 1739 | 0 | 0 |
| Q Serve（g＿s），s | 0.5 | 8.7 | 0.0 | 7.0 | 4.7 | 0.2 | 8.7 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.5 | 8.7 | 0.0 | 7.0 | 4.7 | 0.2 | 8.7 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.95 |  | 1.00 | 0.27 |  | 0.35 |
| Lane Grp Cap（c），veh／h | 37 | 435 |  | 305 | 716 | 611 | 409 | 0 |  | 52 | 0 | 0 |
| V／C Ratio（X） | 0.46 | 0.75 |  | 0.78 | 0.32 | 0.01 | 0.76 | 0.00 |  | 0.50 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 179 | 1103 |  | 772 | 1727 | 1475 | 945 | 0 |  | 581 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 26.0 | 19.1 | 0.0 | 21.3 | 11.6 | 10.2 | 19.4 | 0.0 | 0.0 | 25.7 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 8.5 | 2.6 | 0.0 | 4.4 | 0.3 | 0.0 | 2.9 | 0.0 | 0.0 | 7.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.3 | 3.7 | 0.0 | 3.0 | 1.7 | 0.1 | 3.6 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 34.6 | 21.7 | 0.0 | 25.8 | 11.9 | 10.2 | 22.3 | 0.0 | 0.0 | 32.9 | 0.0 | 0.0 |
| LnGrp LOS | C | C |  | C | B | B | C | A |  | C | A | A |
| Approach Vol，veh／h |  | 341 |  |  | 480 |  |  | 310 |  |  | 26 |  |
| Approach Delay，s／veh |  | 22.3 |  |  | 18.8 |  |  | 22.3 |  |  | 32.9 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 13.8 | 17.1 | 6.1 | 5.6 | 25.3 | 16.8 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 9.0 | 10.7 | 2.8 | 2.5 | 6.7 | 10.7 |
| Green Ext Time（p＿c），s | 0.6 | 1.9 | 0.1 | 0.0 | 1.5 | 1.7 |

## Intersection Summary

| HCM 6th Ctrl Delay | 21.1 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  |  | 4 | i | $\mathbf{T}$ |
| Traffic Vol, veh/h | 580 | 36 | 105 | 416 | 24 | 148 |
| Future Vol, veh/h | 580 | 36 | 105 | 416 | 24 | 148 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 630 | 39 | 114 | 452 | 26 | 161 |



| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 9 |  |  |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations | ${ }^{7}$ | 4 | $\uparrow$ |  | ${ }^{7}$ | 「 |  |
| Traffic Vol, veh/h | 1 | 383 | 240 | 193 | 247 | 1 | 1 |
| Future Vol, veh/h | 1 | 383 | 240 | 193 | 247 | 1 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | 200 | - | - | - | 100 | 0 | 0 |
| Veh in Median Storage, \# | \# - | 0 | 0 | - | 0 |  | - |
| Grade, \% | - | 0 | 0 | - | 0 | - | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 416 | 261 | 210 | 268 | 1 | 1 |





| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ |  | 7 | $\hat{\beta}$ |  | 7 | 个 $\uparrow$ | 「 | 7 | 个 $\uparrow$ | F |
| Traffic Volume（veh／h） | 38 | 711 | 6 | 75 | 471 | 40 | 6 | 328 | 110 | 51 | 317 | 50 |
| Future Volume（veh／h） | 38 | 711 | 6 | 75 | 471 | 40 | 6 | 328 | 110 | 51 | 317 | 50 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 41 | 773 | 7 | 82 | 512 | 43 | 7 | 357 | 120 | 55 | 345 | 54 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 68 | 895 | 8 | 106 | 859 | 72 | 120 | 523 | 233 | 120 | 523 | 233 |
| Arrive On Green | 0.04 | 0.48 | 0.48 | 0.06 | 0.50 | 0.50 | 0.07 | 0.15 | 0.15 | 0.07 | 0.15 | 0.15 |
| Sat Flow，veh／h | 1781 | 1851 | 17 | 1781 | 1702 | 143 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 41 | 0 | 780 | 82 | 0 | 555 | 7 | 357 | 120 | 55 | 345 | 54 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1867 | 1781 | 0 | 1845 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.7 | 0.0 | 27.5 | 3.4 | 0.0 | 15.8 | 0.3 | 7.1 | 5.2 | 2.2 | 6.8 | 2.2 |
| Cycle Q Clear（g＿c），s | 1.7 | 0.0 | 27.5 | 3.4 | 0.0 | 15.8 | 0.3 | 7.1 | 5.2 | 2.2 | 6.8 | 2.2 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 68 | 0 | 903 | 106 | 0 | 931 | 120 | 523 | 233 | 120 | 523 | 233 |
| V／C Ratio（X） | 0.60 | 0.00 | 0.86 | 0.77 | 0.00 | 0.60 | 0.06 | 0.68 | 0.51 | 0.46 | 0.66 | 0.23 |
| Avail Cap（c＿a），veh／h | 170 | 0 | 1421 | 218 | 0 | 1453 | 432 | 876 | 391 | 434 | 881 | 393 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 35.1 | 0.0 | 17.0 | 34.4 | 0.0 | 13.0 | 32.4 | 30.0 | 29.2 | 33.3 | 29.9 | 28.0 |
| Incr Delay（d2），s／veh | 8.1 | 0.0 | 3.5 | 11.3 | 0.0 | 0.6 | 0.2 | 1.6 | 1.8 | 2.7 | 1.4 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.9 | 0.0 | 11.3 | 1.8 | 0.0 | 6.0 | 0.1 | 3.0 | 2.0 | 1.0 | 2.9 | 0.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |


| LnGrp Delay（d），s／veh | 43.2 | 0.0 | 20.5 | 45.7 | 0.0 | 13.6 | 32.6 | 31.6 | 31.0 | 36.0 | 31.3 | 28.5 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | D | A | C | D | A | B | C | C | C | D | C | C |
| Approach Vol，veh／h |  | 821 |  |  | 637 |  |  | 484 |  | 4 | 454 |  |
| Approach Delay，s／veh |  | 21.6 |  |  | 17.8 |  |  | 31.5 |  | 31.6 |  |  |
| Approach LOS |  | C |  |  | B |  |  | C |  | C |  |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 8.9 | 40.4 | 9.5 | 15.4 | 7.4 | 42.0 | 9.5 | 15.4 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 9.1 | 56.5 | 18.0 | 18.4 | 7.1 | 58.5 | 18.1 | 18.3 |
| Max Q Clear Time（g＿c＋11），s | 5.4 | 29.5 | 2.3 | 8.8 | 3.7 | 17.8 | 4.2 | 9.1 |
| Green Ext Time（p＿c），s | 0.0 | 6.4 | 0.0 | 1.6 | 0.0 | 4.2 | 0.1 | 1.8 |

## Intersection Summary

HCM 6th Ctrl Delay 24.5
HCM 6th LOS

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | 4 | b |  |
| Traffic Vol, veh/h | 12 | 77 | 17 | 135 | 89 | 2 |
| Future Vol, veh/h | 12 | 77 | 17 | 135 | 89 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 13 | 84 | 18 | 147 | 97 | 2 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 5.2 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 85 | 280 | 316 | 191 |
| Demand Flow Rate, veh/h | 87 | 285 | 323 | 194 |
| Vehicles Circulating, veh/h | 365 | 177 | 59 | 298 |
| Vehicles Exiting, veh/h | 127 | 205 | 393 | 164 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.7 | 5.5 | 5.0 | 5.4 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 87 | 285 | 323 | 194 |
| Cap Entry Lane, veh/h | 951 | 1152 | 1299 | 1018 |
| Entry HV Adj Factor | 0.982 | 0.981 | 0.980 | 0.984 |
| Flow Entry, veh/h | 85 | 280 | 316 | 191 |
| Cap Entry, veh/h | 933 | 1130 | 1273 | 1002 |
| VIC Ratio | 0.091 | 0.247 | 0.249 | 0.191 |
| Control Delay, s/veh | 4.7 | 5.5 | 5.0 | 5.4 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 0 | 1 | 1 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | -1 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 2 | 31 | 20 | 307 | 343 | 3 |
| Future Vol, veh/h | 2 | 31 | 20 | 307 | 343 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 34 | 22 | 334 | 373 | 3 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement EBL | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |  | ¢ |  |  |
| Traffic Vol, veh/h | 3 | 0 | 92 | 3 | 1 | 1 | 87 | 312 | 0 | 1 | 383 | 4 |  |
| Future Vol, veh/h | 3 | 0 | 92 | 3 | 1 | 1 | 87 | 312 | 0 | 1 | 383 | 4 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control S | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized |  | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length |  | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# |  | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% |  | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% |  | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow |  | 0 | 100 | 3 | 1 | 1 | 95 | 339 | 0 | 1 | 416 | 4 |  |







| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | $\uparrow$ |  |
| Traffic Volume（veh／h） | 4 | 203 | 266 | 298 | 304 | 3 | 325 | 4 | 180 | 8 | 13 | 12 |
| Future Volume（veh／h） | 4 | 203 | 266 | 298 | 304 | 3 | 325 | 4 | 180 | 8 | 13 | 12 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 4 | 209 | 0 | 307 | 313 | 3 | 335 | 4 | 0 | 9 | 14 | 13 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 10 | 298 |  | 381 | 689 | 589 | 440 | 5 |  | 17 | 26 | 24 |
| Arrive On Green | 0.01 | 0.16 | 0.00 | 0.22 | 0.37 | 0.37 | 0.25 | 0.25 | 0.00 | 0.04 | 0.04 | 0.04 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1761 | 21 | 1572 | 434 | 675 | 627 |
| Grp Volume（v），veh／h |  | 209 | 0 | 307 | 313 | 3 | 339 | 0 | 0 | 36 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1782 | 0 | 1572 | 1736 | 0 | 0 |
| Q Serve（g＿s），s | 0.1 | 5.7 | 0.0 | 8.9 | 6.9 | 0.1 | 9.5 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.1 | 5.7 | 0.0 | 8.9 | 6.9 | 0.1 | 9.5 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.25 |  | 0.36 |
| Lane Grp Cap（c），veh／h | 10 | 298 |  | 381 | 689 | 589 | 446 | 0 |  | 67 | 0 | 0 |
| V／C Ratio（X） | 0.42 | 0.70 |  | 0.80 | 0.45 | 0.01 | 0.76 | 0.00 |  | 0.54 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 166 | 759 |  | 969 | 1604 | 1370 | 1077 | 0 |  | 581 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 26.7 | 21.3 | 0.0 | 20.0 | 12.8 | 10.6 | 18.7 | 0.0 | 0.0 | 25.4 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 26.3 | 3.0 | 0.0 | 4.0 | 0.5 | 0.0 | 2.7 | 0.0 | 0.0 | 6.5 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.1 | 2.5 | 0.0 | 3.7 | 2.5 | 0.0 | 3.8 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 52.9 | 24.3 | 0.0 | 24.0 | 13.3 | 10.7 | 21.4 | 0.0 | 0.0 | 31.9 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | C | A |  | C | A | A |
| Approach Vol，veh／h |  | 213 |  |  | 623 |  |  | 339 |  |  | 36 |  |
| Approach Delay，s／veh |  | 24.9 |  |  | 18.6 |  |  | 21.4 |  |  | 31.9 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 16.1 | 13.2 | 6.6 | 4.8 | 24.5 | 17.9 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 29.5 | 22.0 | 18.0 | 5.0 | 46.5 | 32.5 |
| Max Q Clear Time（g＿c＋11），s | 10.9 | 7.7 | 3.1 | 2.1 | 8.9 | 11.5 |
| Green Ext Time（p＿c），s | 0.9 | 0.9 | 0.1 | 0.0 | 2.0 | 2.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 20.9 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{7}$ |  |  | A | 1 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 369 | 32 | 133 | 509 | 22 | 105 |
| Future Vol, veh/h | 369 | 32 | 133 | 509 | 22 | 105 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 401 | 35 | 145 | 553 | 24 | 114 |




| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 610 | 0 | - | 0 | 735 | 493 |  |
| $\quad$ Stage 1 | - | - | - | - | 493 | - |  |
| Stage 2 | - | - | - | - | 242 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 969 | - | - | - | 387 | 576 |  |
| $\quad$ Stage 1 | - | - | - | - | 614 | - |  |
| Stage 2 | - | - | - | - | 798 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 969 | - | - | - | 387 | 576 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 387 | - |  |
| Stage 1 | - | - | - | - | 614 | - |  |
| Stage 2 | - | - | - | - | 798 | - |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\boldsymbol{F}$ |  |  | 4 | I | $\mathbf{T}$ |
| Traffic Vol, veh/h | 226 | 121 | 4 | 386 | 124 | 2 |
| Future Vol, veh/h | 226 | 121 | 4 | 386 | 124 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 246 | 132 | 4 | 420 | 135 | 2 |


| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 0 | 0 | 378 | 0 | 740 | 312 |  |
| Stage 1 | - | - | - | - | 312 | - |  |
| Stage 2 | - | - | - | - | 428 | - |  |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | - | - | 1180 | - | 384 | 728 |  |
| Stage 1 | - | - | - | - | 742 | - |  |
| Stage 2 | - | - | - | - | 657 | - |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1180 | - | 383 | 728 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 383 | - |  |
| Stage 1 | - | - | - | - | 742 | - |  |
| Stage 2 | - | - | - | - | 655 | - |  |


| Approach | EB |  | WB | NB |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0 |  | 0.1 | 19.3 |  |  |  |  |
| HCM LOS |  |  |  | C |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | NBLn2 | EBT | EBR | WBL | WBT |  |
| Capacity (veh/h) |  | 383 | 728 | - | - | 1180 | - |  |
| HCM Lane V/C Ratio |  | 0.352 | 0.003 | - | - | 0.004 | - |  |
| HCM Control Delay (s) |  | 19.4 | 10 | - | - | 8.1 | - |  |
| HCM Lane LOS |  | C | B | - | - | A | - |  |
| HCM 95th \%tile Q(veh) |  | 1.6 | 0 | - | - | 0 | - |  |


|  | $\rangle$ | $\rightarrow$ |  | 7 | － |  | 4 | 4 | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ |  | \％ | $\uparrow$ |  | \％ | 个个 | F | ${ }^{7}$ | 个4 | F |
| Traffic Volume（veh／h） | 52 | 341 | 2 | 76 | 740 | 49 | ， | 314 | 46 | 31 | 253 | 38 |
| Future Volume（veh／h） | 52 | 341 | 2 | 76 | 740 | 49 | 3 | 314 | 46 | 31 | 253 | 38 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 57 | 371 | 2 | 83 | 804 | 53 | 3 | 341 | 50 | 34 | 275 | 41 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 80 | 951 | 5 | 108 | 915 | 60 | 113 | 486 | 217 | 113 | 485 | 217 |
| Arrive On Green | 0.05 | 0.51 | 0.51 | 0.06 | 0.53 | 0.53 | 0.06 | 0.14 | 0.14 | 0.06 | 0.14 | 0.14 |
| Sat Flow，veh／h | 1781 | 1859 | 10 | 1781 | 1735 | 114 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 57 | 0 | 373 | 83 | 0 | 857 | 3 | 341 | 50 | 34 | 275 | 41 |
| Grp Sat Flow（s），veh／h／n | 1781 | 0 | 1869 | 1781 | 0 | 1850 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 2.5 | 0.0 | 9.6 | 3.6 | 0.0 | 32.2 | 0.1 | 7.2 | 2.2 | 1.4 | 5.7 | 1.8 |
| Cycle Q Clear（g＿c），s | 2.5 | 0.0 | 9.6 | 3.6 | 0.0 | 32.2 | 0.1 | 7.2 | 2.2 | 1.4 | 5.7 | 1.8 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.06 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 80 | 0 | 956 | 108 | 0 | 975 | 113 | 486 | 217 | 113 | 485 | 217 |
| V／C Ratio（X） | 0.71 | 0.00 | 0.39 | 0.77 | 0.00 | 0.88 | 0.03 | 0.70 | 0.23 | 0.30 | 0.57 | 0.19 |
| Avail Cap（c＿a），veh／h | 124 | 0 | 1261 | 277 | 0 | 1408 | 406 | 823 | 367 | 408 | 828 | 369 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 37.2 | 0.0 | 11.8 | 36.6 | 0.0 | 16.5 | 34.7 | 32.6 | 30.4 | 35.3 | 31.9 | 30.2 |
| Incr Delay（d2），s／veh | 10.8 | 0.0 | 0.3 | 10.9 | 0.0 | 4.8 | 0.1 | 1.9 | 0.5 | 1.5 | 1.0 | 0.4 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.3 | 0.0 | 3.7 | 1.9 | 0.0 | 13.3 | 0.1 | 3.2 | 0.9 | 0.7 | 2.5 | 0.7 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 48.0 | 0.0 | 12.0 | 47.4 | 0.0 | 21.2 | 34.8 | 34.4 | 30.9 | 36.8 | 32.9 | 30.6 |
| LnGrp LOS | D | A | B | D | A | C | C | C | C | D | C | C |
| Approach Vol，veh／h |  | 430 |  |  | 940 |  |  | 394 |  |  | 350 |  |
| Approach Delay，s／veh |  | 16.8 |  |  | 23.5 |  |  | 34.0 |  |  | 33.1 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 9.3 | 44.9 | 9.5 | 15.3 | 8.1 | 46.1 | 9.5 | 15.3 |  |  |  |  |
| Change Period（ $Y+R \mathrm{Rc}$ ），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 12.3 | 53.3 | 18.0 | 18.4 | 5.5 | 60.1 | 18.1 | 18.3 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 5.6 | 11.6 | 2.1 | 7.7 | 4.5 | 34.2 | 3.4 | 9.2 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.1 | 2.5 | 0.0 | 1.3 | 0.0 | 7.4 | 0.0 | 1.6 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 25.7 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | 4 | b |  |
| Traffic Vol, veh/h | 2 | 26 | 66 | 145 | 177 | 8 |
| Future Vol, veh/h | 2 | 26 | 66 | 145 | 177 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 2 | 28 | 72 | 158 | 192 | 9 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 6.2 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 124 | 285 | 480 | 219 |
| Demand Flow Rate, veh/h | 126 | 291 | 490 | 223 |
| Vehicles Circulating, veh/h | 409 | 255 | 91 | 309 |
| Vehicles Exiting, veh/h | 123 | 326 | 444 | 237 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.4 | 6.1 | 6.7 | 5.8 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR |  |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 4.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 223 |
| Entry Flow, veh/h | 126 | 291 | 490 | 1007 |
| Cap Entry Lane, veh/h | 909 | 1064 | 1258 | 0.983 |
| Entry HV Adj Factor | 0.983 | 0.979 | 0.980 | 219 |
| Flow Entry, veh/h | 124 | 285 | 480 | 990 |
| Cap Entry, veh/h | 893 | 1041 | 1232 | 0.221 |
| V/C Ratio | 0.139 | 0.274 | 0.390 | A |
| Control Delay, s/veh | 5.4 | A | 6.7 | A |
| LOS | A | 1 | 2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | \＄ |  |
| Traffic Volume（veh／h） | 16 | 355 | 402 | 239 | 275 | 8 | 287 | 13 | 268 | 6 |  | 8 |
| Future Volume（veh／h） | 16 | 355 | 402 | 239 | 275 | 8 | 287 | 13 | 268 | 6 | 9 | 8 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 17 | 366 | 0 | 246 | 284 | 9 | 296 | 14 | 0 | 7 | 10 | 9 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 37 | 473 |  | 309 | 760 | 649 | 385 | 18 |  | 14 | 20 | 18 |
| Arrive On Green | 0.02 | 0.26 | 0.00 | 0.18 | 0.41 | 0.41 | 0.23 | 0.23 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1705 | 81 | 1572 | 468 | 669 | 602 |
| Grp Volume（v），veh／h | 17 | 366 | 0 | 246 | 284 | 9 | 310 | 0 | 0 | 26 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1785 | 0 | 1572 | 1739 | 0 | 0 |
| Q Serve（g＿s），s | 0.5 | 10.5 | 0.0 | 7.6 | 6.1 | 0.2 | 9.3 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.5 | 10.5 | 0.0 | 7.6 | 6.1 | 0.2 | 9.3 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.95 |  | 1.00 | 0.27 |  | 0.35 |
| Lane Grp Cap（c），veh／h | 37 | 473 |  | 309 | 760 | 649 | 403 | 0 |  | 51 | 0 | 0 |
| V／C Ratio（X） | 0.46 | 0.77 |  | 0.80 | 0.37 | 0.01 | 0.77 | 0.00 |  | 0.51 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 168 | 1037 |  | 725 | 1624 | 1387 | 889 | 0 |  | 547 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 27.7 | 19.8 | 0.0 | 22.6 | 11.8 | 10.0 | 20.8 | 0.0 | 0.0 | 27.4 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 8.7 | 2.7 | 0.0 | 4.6 | 0.3 | 0.0 | 3.1 | 0.0 | 0.0 | 7.5 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.3 | 4.4 | 0.0 | 3.3 | 2.2 | 0.1 | 3.9 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 36.4 | 22.5 | 0.0 | 27.3 | 12.1 | 10.0 | 23.9 | 0.0 | 0.0 | 34.8 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | C | A |  | C | A | A |
| Approach Vol，veh／h |  | 383 |  |  | 539 |  |  | 310 |  |  | 26 |  |
| Approach Delay，s／veh |  | 23.1 |  |  | 19.0 |  |  | 23.9 |  |  | 34.8 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 14.5 | 19.1 | 6.2 | 5.7 | 27.9 | 17.4 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 9.6 | 12.5 | 2.8 | 2.5 | 8.1 | 11.3 |
| Green Ext Time（p＿c），s | 0.6 | 2.1 | 0.1 | 0.0 | 1.9 | 1.7 |

## Intersection Summary

| HCM 6th Ctrl Delay | 21.8 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{7}$ |  |  | A | 1 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 604 | 36 | 125 | 446 | 24 | 165 |
| Future Vol, veh/h | 604 | 36 | 125 | 446 | 24 | 165 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 657 | 39 | 136 | 485 | 26 | 179 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | A | a | $\mathbf{7}$ |
| Traffic Vol, veh/h | 418 | 177 | 1 | 289 | 138 | 1 |
| Future Vol, veh/h | 418 | 177 | 1 | 289 | 138 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 454 | 192 | 1 | 314 | 150 | 1 |



|  | $\rangle$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ |  | ＊ | $\hat{\square}$ |  | ${ }_{1}$ | 个个 | 「 | ${ }_{1}$ | 个个 | 「 |
| Traffic Volume（veh／h） | 38 | 725 | 6 | 78 | 488 | 42 | 6 | 328 | 112 | 52 | 317 | 50 |
| Future Volume（veh／h） | 38 | 725 | 6 | 78 | 488 | 42 | 6 | 328 | 112 | 52 | 317 | 50 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 41 | 788 | 7 | 85 | 530 | 46 | 7 | 357 | 122 | 57 | 345 | 54 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 68 | 907 | 8 | 110 | 872 | 76 | 117 | 518 | 231 | 117 | 518 | 231 |
| Arrive On Green | 0.04 | 0.49 | 0.49 | 0.06 | 0.51 | 0.51 | 0.07 | 0.15 | 0.15 | 0.07 | 0.15 | 0.15 |
| Sat Flow，veh／h | 1781 | 1851 | 16 | 1781 | 1697 | 147 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 41 | 0 | 795 | 85 | 0 | 576 | 7 | 357 | 122 | 57 | 345 | 54 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1867 | 1781 | 0 | 1844 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.7 | 0.0 | 28.7 | 3.6 | 0.0 | 16.8 | 0.3 | 7.3 | 5.4 | 2.3 | 7.0 | 2.3 |
| Cycle Q Clear（g＿c），s | 1.7 | 0.0 | 28.7 | 3.6 | 0.0 | 16.8 | 0.3 | 7.3 | 5.4 | 2.3 | 7.0 | 2.3 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 68 | 0 | 916 | 110 | 0 | 947 | 117 | 518 | 231 | 117 | 518 | 231 |
| V／C Ratio（X） | 0.60 | 0.00 | 0.87 | 0.77 | 0.00 | 0.61 | 0.06 | 0.69 | 0.53 | 0.49 | 0.67 | 0.23 |
| Avail Cap（c＿a），veh／h | 166 | 0 | 1402 | 199 | 0 | 1418 | 422 | 855 | 381 | 424 | 860 | 383 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 36.0 | 0.0 | 17.2 | 35.2 | 0.0 | 13.1 | 33.3 | 30.9 | 30.1 | 34.3 | 30.7 | 28.7 |
| Incr Delay（d2），s／veh | 8.4 | 0.0 | 3.9 | 11.0 | 0.0 | 0.6 | 0.2 | 1.6 | 1.9 | 3.1 | 1.5 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.9 | 0.0 | 11.9 | 1.8 | 0.0 | 6.3 | 0.1 | 3.1 | 2.1 | 1.1 | 3.0 | 0.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 44.4 | 0.0 | 21.1 | 46.2 | 0.0 | 13.7 | 33.5 | 32.5 | 31.9 | 37.4 | 32.2 | 29.2 |
| LnGrp LOS | D | A | C | D | A | B | C | C | C | D | C | C |
| Approach Vol，veh／h |  | 836 |  |  | 661 |  |  | 486 |  |  | 456 |  |
| Approach Delay，s／veh |  | 22.3 |  |  | 17.9 |  |  | 32.4 |  |  | 32.5 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 9.2 | 41.8 | 9.5 | 15.6 | 7.4 | 43.6 | 9.5 | 15.6 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 8.5 | 57.1 | 18.0 | 18.4 | 7.1 | 58.5 | 18.1 | 18.3 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 5.6 | 30.7 | 2.3 | 9.0 | 3.7 | 18.8 | 4.3 | 9.3 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 6.5 | 0.0 | 1.6 | 0.0 | 4.4 | 0.1 | 1.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 25.0 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | 4 | F |  |
| Traffic Vol, veh/h | 3 | 24 | 67 | 151 | 179 | 7 |
| Future Vol, veh/h | 3 | 24 | 67 | 151 | 179 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 26 | 73 | 164 | 195 | 8 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 6.7 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 148 | 327 | 493 | 221 |
| Demand Flow Rate, veh/h | 150 | 334 | 503 | 225 |
| Vehicles Circulating, veh/h | 444 | 283 | 110 | 378 |
| Vehicles Exiting, veh/h | 159 | 330 | 484 | 239 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 5.9 | 6.9 | 7.1 | 6.3 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR |  | LTR | LTR |
| RT Channelized | 1.000 | 1.000 | 1.000 | 1.000 |
| Lane Util | 2.609 | 2.609 | 2.609 |  |
| Follow-Up Headway, s | 2.609 | 4.976 | 4.976 | 4.976 |
| Critical Headway, s | 4.976 | 334 | 503 | 225 |
| Entry Flow, veh/h | 150 | 1034 | 1233 | 938 |
| Cap Entry Lane, veh/h | 877 | 0.980 | 0.980 | 0.983 |
| Entry HV Adj Factor | 0.984 | 327 | 493 | 221 |
| Flow Entry, veh/h | 148 | 1013 | 1209 | 923 |
| Cap Entry, veh/h | 863 | 0.323 | 0.408 | 0.240 |
| V/C Ratio | 0.171 | 6.9 | 7.1 | 6.3 |
| Control Delay, s/veh | 5.9 | A | A | A |
| LOS | 1 | 2 | 1 |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | $\uparrow$ | b |  |
| Traffic Vol, veh/h | 1 | 29 | 32 | 457 | 447 | 2 |
| Future Vol, veh/h | 1 | 29 | 32 | 457 | 447 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 32 | 35 | 497 | 486 | 2 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | 「 | \% | $\uparrow$ | 「 |  | $\uparrow$ | F |  | ¢ |  |
| Traffic Volume (veh/h) | 15 | 315 | 402 | 227 | 275 | 7 | 326 | 12 | 300 | 6 | 8 | 7 |
| Future Volume (veh/h) | 15 | 315 | 402 | 227 | 275 | 7 | 326 | 12 | 300 | 6 | 8 | 7 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 16 | 325 | 0 | 234 | 284 | 8 | 336 | 13 | 0 | 7 | , | 8 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap, veh/h | 35 | 431 |  | 297 | 706 | 603 | 431 | 17 |  | 14 | 18 | 16 |
| Arrive On Green | 0.02 | 0.23 | 0.00 | 0.17 | 0.38 | 0.38 | 0.25 | 0.25 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow, veh/h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1718 | 66 | 1572 | 508 | 653 | 580 |
| Grp Volume(v), veh/h | 16 | 325 | 0 | 234 | 284 | 8 | 349 | 0 | 0 | 24 | 0 | 0 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1784 | 0 | 1572 | 1741 | 0 | 0 |
| Q Serve(g_s), s | 0.5 | 9.1 | 0.0 | 7.1 | 6.3 | 0.2 | 10.2 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.5 | 9.1 | 0.0 | 7.1 | 6.3 | 0.2 | 10.2 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.96 |  | 1.00 | 0.29 |  | 0.33 |
| Lane Grp Cap(c), veh/h | 35 | 431 |  | 297 | 706 | 603 | 448 | 0 |  | 48 | 0 | 0 |
| V/C Ratio(X) | 0.46 | 0.75 |  | 0.79 | 0.40 | 0.01 | 0.78 | 0.00 |  | 0.50 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 171 | 1058 |  | 740 | 1657 | 1415 | 906 | 0 |  | 558 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 27.2 | 20.1 | 0.0 | 22.4 | 12.7 | 10.8 | 19.6 | 0.0 | 0.0 | 26.9 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 9.0 | 2.7 | 0.0 | 4.6 | 0.4 | 0.0 | 3.0 | 0.0 | 0.0 | 7.6 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.3 | 3.9 | 0.0 | 3.1 | 2.3 | 0.1 | 4.2 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 36.2 | 22.8 | 0.0 | 27.0 | 13.1 | 10.8 | 22.5 | 0.0 | 0.0 | 34.5 | 0.0 | 0.0 |


| LnGrp LOS | D | C | C | B | B | C | A | C |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Vol, veh/h | 341 | 526 |  | 349 | A |  |  |  |
| Approach Delay, s/veh | 23.4 | 19.2 |  | 22.5 | 34.5 |  |  |  |
| Approach LOS | C | B |  | C | C |  |  |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 13.9 | 17.5 | 6.1 | 5.6 | 25.9 | 18.6 |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time (g_c+11), s | 9.1 | 11.1 | 2.8 | 2.5 | 8.3 | 12.2 |
| Green Ext Time (p_c), s | 0.6 | 1.9 | 0.0 | 0.0 | 1.9 | 1.9 |

## Intersection Summary

| HCM 6th Ctrl Delay | 21.6 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for [NBR, EBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\boldsymbol{\beta}$ |  |  | 个 | a | $\mathbf{7}$ |
| Traffic Vol, veh/h | 574 | 38 | 131 | 478 | 30 | 157 |
| Future Vol, veh/h | 574 | 38 | 131 | 478 | 30 | 157 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 624 | 41 | 142 | 520 | 33 | 171 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 12.3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | i | 4 | $\boldsymbol{F}$ |  | 7 | $\mathbf{T}$ |
| Traffic Vol, veh/h | 5 | 356 | 283 | 196 | 266 | 3 |
| Future Vol, veh/h | 5 | 356 | 283 | 196 | 266 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 200 | - | - | - | 100 | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 5 | 387 | 308 | 213 | 289 | 3 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor2 |  |  |  |  |  |  |
| Conflicting Flow All | 521 | 0 | - | 0 | 812 | 415 |
| Stage 1 | - | - | - | - | 415 | - |
| Stage 2 | - | - | - | - | 397 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1045 | - | - | - | 348 | 637 |
| $\quad$ Stage 1 | - | - | - | - | 666 | - |
| Stage 2 | - | - | - | - | 679 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1045 | - | - | - | 346 | 637 |
| Mov Cap-2 Maneuver | - | - | - | - | 346 | - |
| Stage 1 | - | - | - | - | 663 | - |
| Stage 2 | - | - | - | - | 679 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0 | 50.6 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1045 | - | - | - | 346 | 637 |
| HCM Lane V/C Ratio | 0.005 | - | - | -0.836 | 0.005 |  |
| HCM Control Delay (s) | 8.5 | - | - | - | 51.1 | 10.7 |
| HCM Lane LOS | A | - | - | - | F | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 7.4 | 0 |




|  | $\rangle$ |  |  | 7 |  |  |  | $\dagger$ |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | \% | $\uparrow$ |  |  | $\dagger$ |  |  | $\dagger$ |  |
| Traffic Volume (veh/h) | 36 | 678 | 0 | 72 | 419 | 48 | 3 | 288 | 101 | 41 | 292 | 60 |
| Future Volume (veh/h) | 36 | 678 | 0 | 72 | 419 | 48 | 3 | 288 | 101 | 41 | 292 | 60 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 39 | 737 | 0 | 78 | 455 | 52 | 3 | 313 | 110 | 45 | 317 | 65 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 54 | 709 | 0 | 82 | 650 | 74 | 3 | 290 | 102 | 39 | 275 | 56 |
| Arrive On Green | 0.03 | 0.38 | 0.00 | 0.05 | 0.39 | 0.39 | 0.22 | 0.22 | 0.22 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1870 | 0 | 1781 | 1648 | 188 | 13 | 1313 | 461 | 191 | 1345 | 276 |
| Grp Volume(v), veh/h | 39 | 737 | 0 | 78 | 0 | 507 | 426 | 0 | 0 | 427 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1870 | 0 | 1781 | 0 | 1836 | 1787 | 0 | 0 | 1811 | 0 | 0 |
| Q Serve(g_s), s | 2.6 | 45.5 | 0.0 | 5.2 | 0.0 | 27.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.6 | 45.5 | 0.0 | 5.2 | 0.0 | 27.7 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.10 | 0.01 |  | 0.26 | 0.11 |  | 0.15 |
| Lane Grp Cap(c), veh/h | 54 | 709 | 0 | 82 | 0 | 725 | 395 | 0 | 0 | 370 | 0 | 0 |
| VIC Ratio(X) | 0.72 | 1.04 | 0.00 | 0.96 | 0.00 | 0.70 | 1.08 | 0.00 | 0.00 | 1.15 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 709 | 0 | 82 | 0 | 725 | 395 | 0 | 0 | 370 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.7 | 37.3 | 0.0 | 57.1 | 0.0 | 30.4 | 46.8 | 0.0 | 0.0 | 47.8 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 18.2 | 44.4 | 0.0 | 84.4 | 0.0 | 3.0 | 68.3 | 0.0 | 0.0 | 96.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 29.1 | 0.0 | 4.3 | 0.0 | 12.7 | 19.2 | 0.0 | 0.0 | 20.8 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 75.8 | 81.6 | 0.0 | 141.5 | 0.0 | 33.4 | 115.1 | 0.0 | 0.0 | 143.7 | 0.0 | 0.0 |
| LnGrp LOS | E | F | A | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 776 |  |  | 585 |  |  | 426 |  |  | 427 |  |
| Approach Delay, s/veh |  | 81.4 |  |  | 47.8 |  |  | 115.1 |  |  | 143.7 |  |
| Approach LOS |  | F |  |  | D |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 10.0 | 50.0 |  | 29.0 | 8.1 | 51.9 |  | 31.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.5 | 45.5 |  | 24.5 | 5.1 | 45.9 |  | 26.5 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.2 | 47.5 |  | 26.5 | 4.6 | 29.7 |  | 28.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 |  | 0.0 | 0.0 | 3.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 91.0 |  |  |  |  |  |  |  |  |  |
|  |  |  | F |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | 4 | b |  |
| Traffic Vol, veh/h | 3 | 24 | 67 | 170 | 195 | 7 |
| Future Vol, veh/h | 3 | 24 | 67 | 170 | 195 | 7 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 26 | 73 | 185 | 212 | 8 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 7.0 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 149 | 329 | 517 | 238 |
| Demand Flow Rate, veh/h | 151 | 336 | 527 | 242 |
| Vehicles Circulating, veh/h | 463 | 305 | 110 | 381 |
| Vehicles Exiting, veh/h | 160 | 332 | 504 | 260 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 6.0 | 7.1 | 7.3 | 6.6 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 151 | 336 | 527 | 242 |
| Cap Entry Lane, veh/h | 861 | 1011 | 1233 | 936 |
| Entry HV Adj Factor | 0.984 | 0.980 | 0.980 | 0.983 |
| Flow Entry, veh/h | 149 | 329 | 517 | 238 |
| Cap Entry, veh/h | 847 | 991 | 1209 | 920 |
| VIC Ratio | 0.175 | 0.332 | 0.427 | 0.259 |
| Control Delay, s/veh | 6.0 | 7.1 | 7.3 | 6.6 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 1 | 1 | 2 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y' |  |  | -1 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 1 | 29 | 32 | 479 | 465 | 2 |
| Future Vol, veh/h | 1 | 29 | 32 | 479 | 465 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 32 | 35 | 521 | 505 | 2 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | $\uparrow$ |  |
| Traffic Volume（veh／h） | 15 | 360 | 402 | 235 | 329 | 7 | 326 | 12 | 306 | 6 | 8 | 7 |
| Future Volume（veh／h） | 15 | 360 | 402 | 235 | 329 | 7 | 326 | 12 | 306 | 6 | 8 | 7 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 16 | 371 | 0 | 242 | 339 | 8 | 336 | 13 | 0 | 7 | 9 | 8 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 35 | 473 |  | 303 | 755 | 645 | 424 | 16 |  | 14 | 18 | 16 |
| Arrive On Green | 0.02 | 0.25 | 0.00 | 0.17 | 0.41 | 0.41 | 0.25 | 0.25 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1718 | 66 | 1572 | 508 | 653 | 580 |
| Grp Volume（v），veh／h | 16 | 371 | 0 | 242 | 339 | 8 | 349 | 0 | 0 | 24 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1784 | 0 | 1572 | 1741 | 0 | 0 |
| Q Serve（g＿s），s | 0.5 | 11.2 | 0.0 | 7.9 | 8.0 | 0.2 | 11.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.5 | 11.2 | 0.0 | 7.9 | 8.0 | 0.2 | 11.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.96 |  | 1.00 | 0.29 |  | 0.33 |
| Lane Grp Cap（c），veh／h | 35 | 473 |  | 303 | 755 | 645 | 441 | 0 |  | 48 | 0 | 0 |
| V／C Ratio（X） | 0.46 | 0.78 |  | 0.80 | 0.45 | 0.01 | 0.79 | 0.00 |  | 0.50 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 160 | 987 |  | 691 | 1546 | 1321 | 846 | 0 |  | 521 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 29.2 | 20.9 | 0.0 | 23.9 | 13.0 | 10.6 | 21.2 | 0.0 | 0.0 | 28.8 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 9.2 | 2.9 | 0.0 | 4.9 | 0.4 | 0.0 | 3.2 | 0.0 | 0.0 | 7.9 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.3 | 4.8 | 0.0 | 3.5 | 3.0 | 0.1 | 4.6 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 38.4 | 23.8 | 0.0 | 28.8 | 13.4 | 10.6 | 24.4 | 0.0 | 0.0 | 36.8 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | C | A |  | D | A | A |
| Approach Vol，veh／h |  | 387 |  |  | 589 |  |  | 349 |  |  | 24 |  |
| Approach Delay，s／veh |  | 24.4 |  |  | 19.7 |  |  | 24.4 |  |  | 36.8 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 14.8 | 19.8 | 6.2 | 5.7 | 29.0 | 19.4 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 9.9 | 13.2 | 2.8 | 2.5 | 10.0 | 13.0 |
| Green Ext Time（p＿c），s | 0.6 | 2.1 | 0.0 | 0.0 | 2.3 | 1.9 |

Intersection Summary

| HCM 6th Ctrl Delay | 22.6 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{7}$ |  |  | A | l | $\mathbf{7}$ |
| Traffic Vol, veh/h | 601 | 38 | 153 | 510 | 30 | 175 |
| Future Vol, veh/h | 601 | 38 | 153 | 510 | 30 | 175 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 653 | 41 | 166 | 554 | 33 | 190 |




| Major/Minor | Major1 | Major2 |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Minor2 |  |  |  |  |  |  |
| Conflicting Flow All | 556 | 0 | - | 0 | 863 | 445 |
| Stage 1 | - | - | - | - | 445 | - |
| Stage 2 | - | - | - | - | 418 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1015 | - | - | - | 325 | 613 |
| $\quad$ Stage 1 | - | - | - | - | 646 | - |
| Stage 2 | - | - | - | - | 664 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1015 | - | - | - | 323 | 613 |
| Mov Cap-2 Maneuver | - | - | - | - | 323 | - |
| Stage 1 | - | - | - | - | 643 | - |
| Stage 2 | - | - | - | - | 664 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0 | 68.2 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1015 | - | - | - | 323 | 613 |
| HCM Lane V/C Ratio | 0.005 | - | - | -0.922 | 0.005 |  |
| HCM Control Delay (s) | 8.6 | - | - | - | 68.8 | 10.9 |
| HCM Lane LOS | A | - | - | - | F | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 9.1 | 0 |




|  | $\rangle$ |  |  |  |  |  |  | $\uparrow$ |  |  | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | ¢ |  | \% | $\uparrow$ |  |  | $\dagger$ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 36 | 693 | 0 | 75 | 437 | 50 | 3 | 288 | 104 | 42 | 292 | 60 |
| Future Volume (veh/h) | 36 | 693 | 0 | 75 | 437 | 50 | 3 | 288 | 104 | 42 | 292 | 60 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 39 | 753 | 0 | 82 | 475 | 54 | 3 | 313 | 113 | 46 | 317 | 65 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | , | 2 | 2 | 2 |
| Cap, veh/h | 54 | 709 | 0 | 82 | 651 | 74 | 3 | 288 | 104 | 40 | 274 | 56 |
| Arrive On Green | 0.03 | 0.38 | 0.00 | 0.05 | 0.39 | 0.39 | 0.22 | 0.22 | 0.22 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 1870 | 0 | 1781 | 1649 | 187 | 12 | 1302 | 470 | 195 | 1341 | 275 |
| Grp Volume(v), veh/h | 39 | 753 | 0 | 82 | 0 | 529 | 429 | 0 | 0 | 428 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1870 | 0 | 1781 | 0 | 1837 | 1785 | 0 | 0 | 1811 | 0 | 0 |
| Q Serve(g_s), s | 2.6 | 45.5 | 0.0 | 5.5 | 0.0 | 29.4 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 2.6 | 45.5 | 0.0 | 5.5 | 0.0 | 29.4 | 26.5 | 0.0 | 0.0 | 24.5 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.10 | 0.01 |  | 0.26 | 0.11 |  | 0.15 |
| Lane Grp Cap(c), veh/h | 54 | 709 | 0 | 82 | 0 | 725 | 394 | 0 | 0 | 370 | 0 | 0 |
| V/C Ratio(X) | 0.72 | 1.06 | 0.00 | 1.00 | 0.00 | 0.73 | 1.09 | 0.00 | 0.00 | 1.16 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 76 | 709 | 0 | 82 | 0 | 725 | 394 | 0 | 0 | 370 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 57.7 | 37.3 | 0.0 | 57.2 | 0.0 | 30.9 | 46.8 | 0.0 | 0.0 | 47.8 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 18.2 | 51.4 | 0.0 | 100.8 | 0.0 | 3.7 | 71.1 | 0.0 | 0.0 | 97.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 30.5 | 0.0 | 4.8 | 0.0 | 13.6 | 19.5 | 0.0 | 0.0 | 20.9 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 75.8 | 88.7 | 0.0 | 158.1 | 0.0 | 34.6 | 117.9 | 0.0 | 0.0 | 144.8 | 0.0 | 0.0 |
| LnGrp LOS | E | F | A | F | A | C | F | A | A | F | A | A |
| Approach Vol, veh/h |  | 792 |  |  | 611 |  |  | 429 |  |  | 428 |  |
| Approach Delay, s/veh |  | 88.0 |  |  | 51.2 |  |  | 117.9 |  |  | 144.8 |  |
| Approach LOS |  | F |  |  | D |  |  | F |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $s$ | 10.0 | 50.0 |  | 29.0 | 8.1 | 51.9 |  | 31.0 |  |  |  |  |
| Change Period ( $Y+R \mathrm{R}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.5 | 45.5 |  | 24.5 | 5.1 | 45.9 |  | 26.5 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 7.5 | 47.5 |  | 26.5 | 4.6 | 31.4 |  | 28.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 |  | 0.0 | 0.0 | 3.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 94.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | F |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | r |  | 1 | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 3 | 26 | 72 | 163 | 193 | 8 |
| Future Vol, veh/h | 3 | 26 | 72 | 163 | 193 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 28 | 78 | 177 | 210 | 9 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 7.2 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 159 | 352 | 532 | 238 |
| Demand Flow Rate, veh/h | 162 | 359 | 542 | 242 |
| Vehicles Circulating, veh/h | 478 | 306 | 120 | 406 |
| Vehicles Exiting, veh/h | 170 | 356 | 520 | 259 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 6.3 | 7.4 | 7.6 | 6.8 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR |  | LTR | LTR |
| RT Channelized | 1.000 | 1.000 | 1.000 | 1.000 |
| Lane Util | 2.609 | 2.609 | 2.609 |  |
| Follow-Up Headway, s | 2.609 | 4.976 | 4.976 | 246 |
| Critical Headway, s | 4.976 | 359 | 542 | 242 |
| Entry Flow, veh/h | 162 | 1010 | 1221 | 912 |
| Cap Entry Lane, veh/h | 847 | 0.981 | 0.981 | 0.983 |
| Entry HV Adj Factor | 0.984 | 352 | 532 | 238 |
| Flow Entry, veh/h | 159 | 991 | 1197 | 897 |
| Cap Entry, veh/h | 834 | 0.355 | 0.444 | 6.8 |
| V/C Ratio | 0.191 | 7.4 | 7.6 | A |
| Control Delay, s/veh | 6.3 | A | 2 | 2 |










| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\uparrow$ | 「 | 7 | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | \＄ |  |
| Traffic Volume（veh／h） | 16 | 339 | 433 | 245 | 296 | 8 | 351 | 13 | 323 | 6 | 9 | 8 |
| Future Volume（veh／h） | 16 | 339 | 433 | 245 | 296 | 8 | 351 | 13 | 323 | 6 | 9 | 8 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 17 | 349 | 0 | 253 | 305 | 9 | 362 | 14 | 0 | 7 | 10 | 9 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 36 | 446 |  | 313 | 737 | 630 | 449 | 17 |  | 14 | 19 | 18 |
| Arrive On Green | 0.02 | 0.24 | 0.00 | 0.18 | 0.40 | 0.40 | 0.26 | 0.26 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1718 | 66 | 1572 | 468 | 669 | 602 |
| Grp Volume（v），veh／h | 17 | 349 | 0 | 253 | 305 | 9 | 376 | 0 | 0 | 26 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1784 | 0 | 1572 | 1739 | 0 | 0 |
| Q Serve（g＿s），s | 0.6 | 10.9 | 0.0 | 8.5 | 7.3 | 0.2 | 12.2 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.6 | 10.9 | 0.0 | 8.5 | 7.3 | 0.2 | 12.2 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.96 |  | 1.00 | 0.27 |  | 0.35 |
| Lane Grp Cap（c），veh／h | 36 | 446 |  | 313 | 737 | 630 | 467 | 0 |  | 51 | 0 | 0 |
| V／C Ratio（X） | 0.47 | 0.78 |  | 0.81 | 0.41 | 0.01 | 0.81 | 0.00 |  | 0.51 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 156 | 962 |  | 673 | 1506 | 1286 | 824 | 0 |  | 507 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 29.9 | 21.9 | 0.0 | 24.4 | 13.4 | 11.3 | 21.3 | 0.0 | 0.0 | 29.5 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 9.0 | 3.0 | 0.0 | 4.9 | 0.4 | 0.0 | 3.3 | 0.0 | 0.0 | 7.8 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％oile BackOfQ（50\％），veh／ln | 0.3 | 4.7 | 0.0 | 3.7 | 2.8 | 0.1 | 5.1 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 38.9 | 25.0 | 0.0 | 29.3 | 13.8 | 11.3 | 24.7 | 0.0 | 0.0 | 37.4 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | C | A |  | D | A | A |
| Approach Vol，veh／h |  | 366 |  |  | 567 |  |  | 376 |  |  | 26 |  |
| Approach Delay，s／veh |  | 25.6 |  |  | 20.7 |  |  | 24.7 |  |  | 37.4 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 15.4 | 19.4 | 6.3 | 5.8 | 29.0 | 20.6 |
| Change Period（Y＋Rc），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 10.5 | 12.9 | 2.9 | 2.6 | 9.3 | 14.2 |
| Green Ext Time（p＿c），s | 0.6 | 2.0 | 0.1 | 0.0 | 2.0 | 2.0 |

## Intersection Summary

HCM 6th Ctrl Delay 23.5

HCM 6th LOS C
Notes
Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\boldsymbol{F}$ |  |  | 个 | a | $\mathbf{7}$ |
| Traffic Vol, veh/h | 619 | 41 | 141 | 515 | 32 | 169 |
| Future Vol, veh/h | 619 | 41 | 141 | 515 | 32 | 169 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 1 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 673 | 45 | 153 | 560 | 35 | 184 |




| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 561 | 0 | - | 0 | 874 | 447 |  |
| $\quad$ Stage 1 | - | - | - | - | 447 | - |  |
| $\quad$ Stage 2 | - | - | - | - | 427 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | 1010 | - | - | - | 320 | 612 |  |
| $\quad$ Stage 1 | - | - | - | - | 644 | - |  |
| Stage 2 | - | - | - | - | 658 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1010 | - | - | - | 318 | 612 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 318 | - |  |
| Stage 1 | - | - | - | - | 641 | - |  |
| Stage 2 | - | - | - | - | 658 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0 | 82.2 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1010 | - | - | - | 318 | 612 |
| HCM Lane V/C Ratio | 0.005 | - | - | -0.981 | 0.005 |  |
| HCM Control Delay (s) | 8.6 | - | - | - | 82.9 | 10.9 |
| HCM Lane LOS | A | - | - | - | F | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 10.4 | 0 |



| Major/Minor | Major1 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Major2 |  | Minor1 |  |  |  |  |
| Conflicting Flow All | 0 | 0 | 605 | 0 | 891 | 524 |
| Stage 1 | - | - | - | - | 524 | - |
| $\quad$ Stage 2 | - | - | - | - | 367 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | -2.218 | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | - | - | 973 | - | 313 | 553 |
| $\quad$ Stage 1 | - | - | - | - | 594 | - |
| Stage 2 | - | - | - | - | 701 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 973 | - | 312 | 553 |
| Mov Cap-2 Maneuver | - | - | - | - | 312 | - |
| Stage 1 | - | - | - | - | 594 | - |
| Stage 2 | - | - | - | - | 700 | - |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | ---: |
| HCM Control Delay, s | 0 | 0.1 | 23.6 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 312 | 553 | - | - | 973 | - |
| HCM Lane V/C Ratio | 0.39 | 0.002 | - | -0.002 | - |  |
| HCM Control Delay (s) | 23.7 | 11.5 | - | - | 8.7 | - |
| HCM Lane LOS | C | B | - | - | A | - |
| HCM 95th \%tile Q(veh) | 1.8 | 0 | - | - | 0 | - |


|  | $\rangle$ | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{+}$ |  | \％ | $\hat{\dagger}$ |  | ${ }_{7}$ | ¢个 | 「 | ${ }_{1}$ | 个个 | 「 |
| Traffic Volume（veh／h） | 39 | 731 | 0 | 78 | 452 | 52 | 3 | 310 | 109 | 44 | 315 | 65 |
| Future Volume（veh／h） | 39 | 731 | 0 | 78 | 452 | 52 | 3 | 310 | 109 | 44 | 315 | 65 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 42 | 795 | 0 | 85 | 491 | 57 | 3 | 337 | 118 | 48 | 342 | 71 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 69 | 918 | 0 | 110 | 845 | 98 | 119 | 499 | 223 | 119 | 499 | 223 |
| Arrive On Green | 0.04 | 0.49 | 0.00 | 0.06 | 0.51 | 0.51 | 0.07 | 0.14 | 0.14 | 0.07 | 0.14 | 0.14 |
| Sat Flow，veh／h | 1781 | 1870 | 0 | 1781 | 1645 | 191 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 42 | 795 | 0 | 85 | 0 | 548 | 3 | 337 | 118 | 48 | 342 | 71 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1870 | 0 | 1781 | 0 | 1836 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.7 | 28.2 | 0.0 | 3.5 | 0.0 | 15.5 | 0.1 | 6.7 | 5.2 | 1.9 | 6.9 | 3.0 |
| Cycle Q Clear（g＿c），s | 1.7 | 28.2 | 0.0 | 3.5 | 0.0 | 15.5 | 0.1 | 6.7 | 5.2 | 1.9 | 6.9 | 3.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.10 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 69 | 918 | 0 | 110 | 0 | 943 | 119 | 499 | 223 | 119 | 499 | 223 |
| V／C Ratio（X） | 0.61 | 0.87 | 0.00 | 0.77 | 0.00 | 0.58 | 0.03 | 0.67 | 0.53 | 0.40 | 0.68 | 0.32 |
| Avail Cap（c＿a），veh／h | 169 | 1411 | 0 | 216 | 0 | 1434 | 428 | 869 | 387 | 431 | 873 | 390 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 35.4 | 16.9 | 0.0 | 34.6 | 0.0 | 12.6 | 32.7 | 30.6 | 29.9 | 33.5 | 30.6 | 29.0 |
| Incr Delay（d2），s／veh | 8.3 | 3.8 | 0.0 | 10.9 | 0.0 | 0.6 | 0.1 | 1.6 | 1.9 | 2.2 | 1.7 | 0.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.9 | 11.6 | 0.0 | 1.8 | 0.0 | 5.8 | 0.1 | 2.9 | 2.0 | 0.9 | 3.0 | 1.2 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 43.7 | 20.7 | 0.0 | 45.5 | 0.0 | 13.2 | 32.7 | 32.1 | 31.8 | 35.7 | 32.3 | 29.8 |
| LnGrp LOS | D | C | A | D | A | B | C | C | C | D | C | C |
| Approach Vol，veh／h |  | 837 |  |  | 633 |  |  | 458 |  |  | 461 |  |
| Approach Delay，s／veh |  | 21.8 |  |  | 17.5 |  |  | 32.1 |  |  | 32.2 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 9.1 | 41.2 | 9.5 | 15.0 | 7.4 | 42.9 | 9.5 | 15.0 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 9.1 | 56.5 | 18.0 | 18.4 | 7.1 | 58.5 | 18.1 | 18.3 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 5.5 | 30.2 | 2.1 | 8.9 | 3.7 | 17.5 | 3.9 | 8.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 6.5 | 0.0 | 1.7 | 0.0 | 4.2 | 0.1 | 1.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 24.7 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | 4 | F |  |
| Traffic Vol, veh/h | 3 | 26 | 72 | 182 | 209 | 8 |
| Future Vol, veh/h | 3 | 26 | 72 | 182 | 209 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 85 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 3 | 28 | 78 | 198 | 227 | 9 |



| Intersection |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 7.5 |  |  |  |
| Intersection LOS | A |  |  |  |
| Approach | EB | WB | NB | SB |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 1 | 1 | 1 |
| Adj Approach Flow, veh/h | 160 | 353 | 555 | 255 |
| Demand Flow Rate, veh/h | 163 | 360 | 566 | 259 |
| Vehicles Circulating, veh/h | 496 | 328 | 120 | 408 |
| Vehicles Exiting, veh/h | 171 | 358 | 539 | 280 |
| Ped Vol Crossing Leg, \#/h | 0 | 0 | 0 | 0 |
| Ped Cap Adj | 1.000 | 1.000 | 1.000 | 1.000 |
| Approach Delay, s/veh | 6.4 | 7.7 | 7.9 | 7.0 |
| Approach LOS | A | A | A | A |


| Lane | Left | Left | Left | Left |
| :---: | :---: | :---: | :---: | :---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR | LTR |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 2.609 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 4.976 |
| Entry Flow, veh/h | 163 | 360 | 566 | 259 |
| Cap Entry Lane, veh/h | 832 | 988 | 1221 | 910 |
| Entry HV Adj Factor | 0.984 | 0.981 | 0.981 | 0.983 |
| Flow Entry, veh/h | 160 | 353 | 555 | 255 |
| Cap Entry, veh/h | 819 | 969 | 1198 | 895 |
| VIC Ratio | 0.196 | 0.365 | 0.464 | 0.285 |
| Control Delay, s/veh | 6.4 | 7.7 | 7.9 | 7.0 |
| LOS | A | A | A | A |
| 95th \%tile Queue, veh | 1 | 2 | 3 | 1 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Yr |  |  | -1 | $\mathbf{F}$ |  |
| Traffic Vol, veh/h | 1 | 31 | 34 | 515 | 500 | 2 |
| Future Vol, veh/h | 1 | 31 | 34 | 515 | 500 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 34 | 37 | 560 | 543 | 2 |









| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | 「 | \％ | 个 | 「 |  | $\uparrow$ | 「 |  | $\dagger$ |  |
| Traffic Volume（veh／h） | 16 | 384 | 433 | 253 | 350 | 8 | 351 | 13 | 329 | 6 | 9 | 8 |
| Future Volume（veh／h） | 16 | 384 | 433 | 253 | 350 | 8 | 351 | 13 | 329 | 6 | 9 | 8 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1856 | 1856 | 1856 | 1856 | 1870 | 1856 | 1870 | 1856 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 17 | 396 | 0 | 261 | 361 | 9 | 362 | 14 | 0 | 7 | 10 | 9 |
| Peak Hour Factor | 0.92 | 0.97 | 0.97 | 0.97 | 0.97 | 0.92 | 0.97 | 0.92 | 0.97 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 2 | 3 | 2 | 2 | 2 |
| Cap，veh／h | 36 | 489 |  | 318 | 785 | 670 | 442 | 17 |  | 13 | 19 | 17 |
| Arrive On Green | 0.02 | 0.26 | 0.00 | 0.18 | 0.42 | 0.42 | 0.26 | 0.26 | 0.00 | 0.03 | 0.03 | 0.03 |
| Sat Flow，veh／h | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1718 | 66 | 1572 | 468 | 669 | 602 |
| Grp Volume（v），veh／h | 17 | 396 | 0 | 261 | 361 | 9 | 376 | 0 | 0 | 26 | 0 | 0 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 1856 | 1572 | 1767 | 1856 | 1585 | 1784 | 0 | 1572 | 1739 | 0 | 0 |
| Q Serve（g＿s），s | 0.6 | 13.3 | 0.0 | 9.4 | 9.3 | 0.2 | 13.2 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 0.6 | 13.3 | 0.0 | 9.4 | 9.3 | 0.2 | 13.2 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.96 |  | 1.00 | 0.27 |  | 0.35 |
| Lane Grp Cap（c），veh／h | 36 | 489 |  | 318 | 785 | 670 | 459 | 0 |  | 50 | 0 | 0 |
| V／C Ratio（X） | 0.47 | 0.81 |  | 0.82 | 0.46 | 0.01 | 0.82 | 0.00 |  | 0.52 | 0.00 | 0.00 |
| Avail Cap（c＿a），veh／h | 145 | 894 |  | 625 | 1400 | 1196 | 766 | 0 |  | 471 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay（d），s／veh | 32.2 | 22.9 | 0.0 | 26.2 | 13.7 | 11.1 | 23.2 | 0.0 | 0.0 | 31.8 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 9.2 | 3.3 | 0.0 | 5.3 | 0.4 | 0.0 | 3.7 | 0.0 | 0.0 | 8.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.4 | 5.8 | 0.0 | 4.2 | 3.6 | 0.1 | 5.6 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 41.4 | 26.2 | 0.0 | 31.5 | 14.2 | 11.1 | 26.9 | 0.0 | 0.0 | 40.0 | 0.0 | 0.0 |
| LnGrp LOS | D | C |  | C | B | B | C | A |  | D | A | A |
| Approach Vol，veh／h |  | 413 |  |  | 631 |  |  | 376 |  |  | 26 |  |
| Approach Delay，s／veh |  | 26.8 |  |  | 21.3 |  |  | 26.9 |  |  | 40.0 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 16.4 | 22.0 | 6.4 | 5.8 | 32.6 | 21.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 23.5 | 32.0 | 18.0 | 5.4 | 50.1 | 28.5 |
| Max Q Clear Time（g＿c＋11），s | 11.4 | 15.3 | 3.0 | 2.6 | 11.3 | 15.2 |
| Green Ext Time（p＿c），s | 0.6 | 2.2 | 0.1 | 0.0 | 2.4 | 1.9 |

## Intersection Summary

HCM 6th Ctrl Delay 24.7
HCM 6th LOS
C
Notes
Unsignalized Delay for［NBR，EBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{F}$ |  | i | 个 | t | $\mathbf{7}$ |
| Traffic Vol, veh/h | 646 | 41 | 163 | 547 | 32 | 187 |
| Future Vol, veh/h | 646 | 41 | 163 | 547 | 32 | 187 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Yield | - | None | - | Yield |
| Storage Length | - | - | 275 | - | 0 | 250 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 1 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 702 | 45 | 177 | 595 | 35 | 203 |




| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 596 | 0 | - | 0 | 925 | 477 |  |
| Stage 1 | - | - | - | - | 477 | - |  |
| Stage 2 | - | - | - | - | 448 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | 980 | - | - | $-\sim 299$ | 588 |  |  |
| $\quad$ Stage 1 | - | - | - | - | 624 | - |  |
| Stage 2 | - | - | - | - | 644 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 980 | - | - | - | $\sim 298$ | 588 |  |
| Mov Cap-2 Maneuver | - | - | - | - | $\sim 298$ | - |  |
| Stage 1 | - | - | - | - | 621 | - |  |
| Stage 2 | - | - | - | - | 644 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0 | 111.6 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 980 | - | - | - | 298 | 588 |
| HCM Lane V/C Ratio | 0.006 | - | - | -1.076 | 0.006 |  |
| HCM Control Delay (s) | 8.7 | - | - | -112.6 | 11.2 |  |
| HCM Lane LOS | A | - | - | - | F | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 12.5 | 0 |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 6 |  | 1 | 个 | I | $\mathbf{7}$ |
| Traffic Vol, veh/h | 426 | 150 | 2 | 357 | 112 | 1 |
| Future Vol, veh/h | 426 | 150 | 2 | 357 | 112 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 500 | - | 0 | 50 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 463 | 163 | 2 | 388 | 122 | 1 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F |  | ${ }^{7}$ | F |  | ${ }^{7}$ | 个 $\uparrow$ | F | ${ }^{7}$ | 个 $\uparrow$ | $\overline{7}$ |
| Traffic Volume (veh/h) | 39 | 746 | 0 | 81 | 470 | 54 | 3 | 310 | 112 | 45 | 315 | 65 |
| Future Volume (veh/h) | 39 | 746 | 0 | 81 | 470 | 54 | 3 | 310 | 112 | 45 | 315 | 65 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 42 | 811 | 0 | 88 | 511 | 59 | 3 | 337 | 122 | 49 | 342 | 71 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 69 | 931 | 0 | 114 | 861 | 99 | 116 | 495 | 221 | 116 | 495 | 221 |
| Arrive On Green | 0.04 | 0.50 | 0.00 | 0.06 | 0.52 | 0.52 | 0.07 | 0.14 | 0.14 | 0.07 | 0.14 | 0.14 |
| Sat Flow, veh/h | 1781 | 1870 | 0 | 1781 | 1646 | 190 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 42 | 811 | 0 | 88 | 0 | 570 | 3 | 337 | 122 | 49 | 342 | 71 |
| Grp Sat Flow(s),veh/h/n | 1781 | 1870 | 0 | 1781 | 0 | 1836 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 1.8 | 29.5 | 0.0 | 3.7 | 0.0 | 16.5 | 0.1 | 6.9 | 5.5 | 2.0 | 7.0 | 3.1 |
| Cycle Q Clear(g_c), s | 1.8 | 29.5 | 0.0 | 3.7 | 0.0 | 16.5 | 0.1 | 6.9 | 5.5 | 2.0 | 7.0 | 3.1 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.10 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 69 | 931 | 0 | 114 | 0 | 960 | 116 | 495 | 221 | 116 | 495 | 221 |
| V/C Ratio(X) | 0.61 | 0.87 | 0.00 | 0.78 | 0.00 | 0.59 | 0.03 | 0.68 | 0.55 | 0.42 | 0.69 | 0.32 |
| Avail Cap(c_a), veh/h | 165 | 1390 | 0 | 197 | 0 | 1398 | 417 | 847 | 378 | 420 | 851 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.4 | 17.1 | 0.0 | 35.4 | 0.0 | 12.7 | 33.6 | 31.4 | 30.8 | 34.5 | 31.5 | 29.8 |
| Incr Delay (d2), s/veh | 8.5 | 4.2 | 0.0 | 10.7 | 0.0 | 0.6 | 0.1 | 1.7 | 2.2 | 2.4 | 1.7 | 0.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.9 | 12.3 | 0.0 | 1.9 | 0.0 | 6.2 | 0.1 | 3.0 | 2.2 | 0.9 | 3.1 | 1.2 |
| Unsig. Movement Delay, s/ve |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d).s/veh | 44.9 | 21.4 | 0.0 | 46.1 | 0.0 | 13.3 | 33.7 | 33.1 | 33.0 | 37.0 | 33.2 | 30.6 |


| LnGrp Delay(d),s/veh | 44.9 | 21.4 | 0.0 | 46.1 | 0.0 | 13.3 | 33.7 | 33.1 | 33.0 | 37.0 | 33.2 | 30.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | D | C | A | D | A | B | C | C | C | D | C | C |
| Approach Vol, veh/h |  | 853 |  |  | 658 |  |  | 462 |  | 46 |  |  |
| Approach Delay, s/veh |  | 22.5 |  |  | 17.7 |  |  | 33.1 |  | 43 |  |  |
| Approach LOS |  | C |  |  | B |  |  | C |  | 33.2 |  |  |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 9.4 | 42.7 | 9.5 | 15.2 | 7.5 | 44.7 | 9.5 | 15.2 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$, s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Max Green Setting (Gmax), s | 8.5 | 57.1 | 18.0 | 18.4 | 7.1 | 58.5 | 18.1 | 18.3 |
| Max Q Clear Time (g_c+11), s | 5.7 | 31.5 | 2.1 | 9.0 | 3.8 | 18.5 | 4.0 | 8.9 |
| Green Ext Time (p_c), s | 0.0 | 6.7 | 0.0 | 1.6 | 0.0 | 4.4 | 0.1 | 1.8 |

## Intersection Summary

| HCM 6th Ctrl Delay | 25.2 |
| :--- | ---: |
| HCM 6th LOS | C |


[^0]:    Source: Appendix E, Table 8.

[^1]:    ${ }^{1}$ Final Traffic Study for the Ione Band of Miwok Indians Casino/Hotel Proposal, Dowling Asssociates, Sacramento, CA, November 7, 2008.

[^2]:    ${ }^{2}$ 6th Edition of Highway Capacity Manual, Transportation Research Board, Washington D.C., 2016

[^3]:    FIGURE 4B | EXISTING WEEKDAY AM(PM) PEAK HOUR TRAFFIC VOLUMES TRANSPORTATION IMPACT STUDY

    Ione Casino Project
    Amador County

[^4]:    ${ }^{3}$ Transportation Impact Analysis of the Tejon Casino, Linscott, Law, \& Greenspan Engineers, San Diego, CA, October 30, 2019.

[^5]:    ${ }^{4}$ Putnam Ranch Development Project, Draft Transportation Analysis Report, Fehr \& Peers Associates, Roseville, CA, May 11, 2023.

[^6]:    FIGURE 9B CUMULATIVE WEEKDAY AM(PM) PEAK HOUR TRAFFIC VOLUMES TRANSPORTATION IMPACT STUDY

    Ione Casino Project
    Amador County

[^7]:    ${ }^{5}$ Technical Advisory on Evaluating Transportation Impacts in CEQA, Governor's Office of Planning and Research, Sacramento, CA, December, 2018.

